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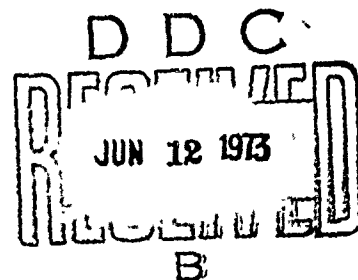
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RDTE PROJECT NO.  
AVSCOM PROJECT NO. 70-15-3  
USAASTA PROJECT NO. 70-15-3

# **VIBRATION AND TEMPERATURE SURVEY CH-54B HELICOPTER**

FINAL REPORT



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MARCH 1973

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UNITED STATES ARMY AVIATION SYSTEMS TEST ACTIVITY  
EDWARDS AIR FORCE BASE, CALIFORNIA 93523



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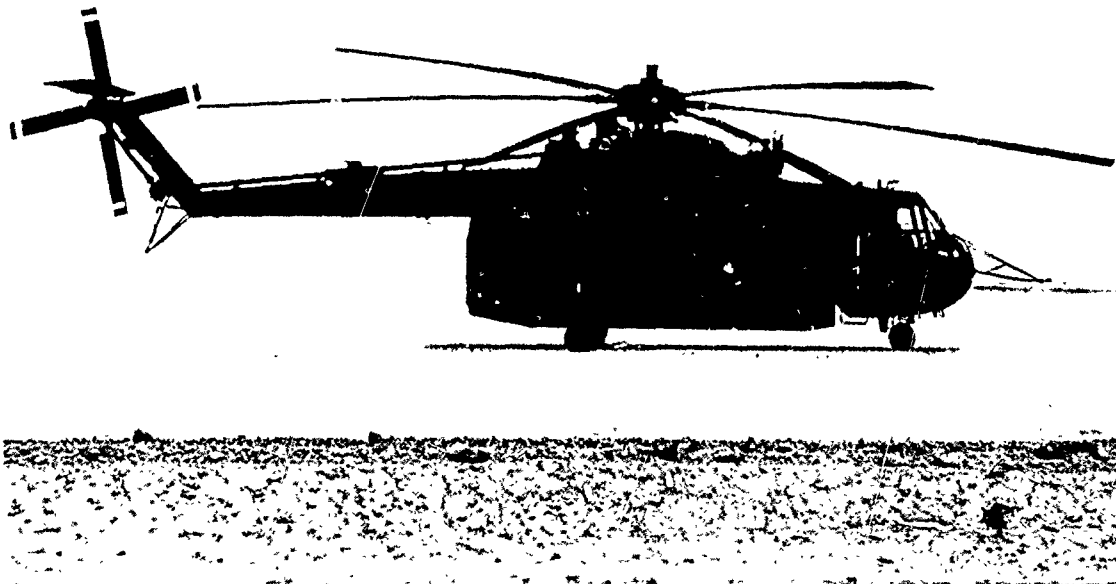
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## FOREWORD

The United States Army Air Mobility Research and Development Laboratory (USAAMRDL), Eustis Directorate, Fort Eustis, Virginia, provided data reduction technical support through a contract with Northrop Corporation, Electronics Division, Palos Verdes Peninsula, California. USAAMRDL also provided instrumentation installation, calibration, and maintenance support. The dental work required to construct the pilot's bite block was provided by the Air Force Flight Test Center Dental Laboratory, Edwards Air Force Base, California. Wet Bulb Globe Temperature measurement equipment was obtained from the United States Army Medical Equipment Research and Development Laboratory, Fort Totten, New York. Technical advice on the measurement of pilot vibrations was obtained from the United States Army Aeromedical Research Laboratory, Fort Rucker, Alabama.

## ABSTRACT

Vibration and temperature measurement tests were conducted on a CH-54B helicopter to define the vibration and temperature environment for the instruments, avionics, pilot station, and other component parts for representative flight conditions. Testing was performed by the United States Army Aviation Systems Test Activity, Edwards Air Force Base, California, between 22 August and 29 September 1972. The testing consisted of 16 flights totaling 18.5 productive test hours. Vibration data were recorded from 70 accelerometer locations for 55 flight conditions, and narrow band spectral analyses were performed on the vibration data. The results of the spectral analyses were summarized by use of statistical methods. Forward fuselage vibrations were primarily low frequency and were caused by the main rotor. Aft fuselage vibrations were primarily high frequency and were caused by gearbox and other rotating component vibration sources. The highest vibration levels were recorded at the auxiliary power plant at main transmission gear mesh frequencies. There were two shortcomings: amplification of main rotor-induced vibrations by avionics vibration isolation mounts, and excessively high Wet Bulb Globe Temperature index at the pilot station under certain environmental conditions.



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DISTRIBUTION

# **INTRODUCTION**

## **BACKGROUND**

1. The failure rates of helicopter components such as instruments, avionics, gearboxes, bearings, pumps, etc., have reduced mission accomplishment and have increased the logistic support effort required to keep Army helicopters at the necessary level of operational capability. It is suspected that many component failures result from an excessive vibration and temperature environment and that the helicopter vibration and temperature environment may degrade pilot performance. However, there are insufficient data available to verify these suspicions. To obtain the data necessary to define the vibration and temperature environment of helicopter components and the pilot station, the United States Army Aviation Systems Test Activity (USAASTA) was directed (ref 1, app A) by the United States Army Aviation Systems Command (AVSCOM) to conduct a vibration and temperature survey on present-day Army helicopters.

2. This report on the CH-54B helicopter is the third of a planned series of six reports which will define the vibration and temperature environment of the OH-58A (ref 2, app A), UH-1H (ref 3), CH-54B, OH-6A, CH-47C, and AH-1G helicopters.

## **TEST OBJECTIVE**

3. The objective of the entire environmental test project is to determine a representative vibration and temperature environment for all present-day Army helicopters. The objective of the CH-54B environmental survey was to determine the vibration and temperature environment of the CH-54B instruments, avionics, selected components, and the pilot station under all normal operating conditions.

## **DESCRIPTION**

4. The CH-54B helicopter is an improved version of the CH-54A. Power for the CH-54B is furnished by two Pratt and Whitney model T73-P-700 gas turbine engines rated at 4800 shaft horsepower (shp) each for 30 minutes and 4430 shp for continuous operations (sea level, standard day). The helicopter is transmission-limited to 7900 shp for dual-engine operation and to 30 minutes single-engine operation at 4800 shp. A Solar model T-62T-16A1 or T-62T-16A2 gas turbine auxiliary power plant is provided for ground engine starting and operation of aircraft accessories during periods when the rotor system is not operating. The CH-54B design incorporates a single main lifting rotor and a tail rotor for antitorque and directional control. The main rotor is a six-bladed fully articulated system, and the tail rotor is a four-bladed semiarticulated system. Externally attached cargo or a detachable pod can be carried. The pod can be used to carry cargo and/or personnel internally or be equipped as a portable hospital

unit, a command post, etc. A capability for towing surface-type vehicles is also provided. The cockpit compartment has seats and controls for the pilot and copilot, and also for a pilot seated behind the copilot facing aft. Seating for two additional personnel is also provided. The helicopter has a fixed-tricycle landing gear with a full-swiveling nose wheel and dual main wheels. Brakes are provided for the main wheels only and can be activated by either the pilot or the copilot. There are no provisions for arming the helicopter. The instruments are rigidly mounted. Selected avionics items are mounted on vibration isolators. The avionics equipment on the test aircraft was as specified in the operator's manual (ref 4, app A) except for the AN/ARC-102 radio set, which was not installed. Detailed aircraft and flight instruments information may be found in appendix B and in the operator's manual.

### SCOPE OF TEST

5. Vibration data were recorded during steady flight and maneuvering flight from 51 triaxial accelerometer locations, 10 biaxial accelerometer locations, and 9 uniaxial locations for 55 flight and ground conditions. Three configurations were tested: clean, 28,400 pounds; pod, 41,900 pounds; sling load, 41,900 pounds. The flight conditions and configurations tested are listed in table 1 and appendix C, respectively. Temperature data were recorded at 20 locations in flight and during static hot soaks in the sun. The accelerometer and thermocouple locations are described in appendix D and photographs of these locations are presented in appendix E. A total of 16 flights were conducted, consisting of 18.5 productive test hours, at Edwards Air Force Base, California. A comparison with selected previously gathered vibration data was made. The flight restrictions and operating limitations observed during this evaluation were as specified in the operator's manual (ref 4, app A). The flight conditions and configurations which will be used for future helicopter environmental testing are contained in the test plan (ref 5).

### METHODS OF TEST

6. The test CH-54B helicopter (S/N 69-18463) was instrumented to record vibration data on a frequency multiplexed-frequency modulated (FM-FM) magnetic tape system. One hundred eighty-two channels of acceleration vibration data were recorded from accelerometers mounted on the instrument panel, avionics, pilot station, and other selected components. The instrumentation was limited to recording data from 12 accelerometer axes simultaneously with 8 manual switching groups. This switching enabled a total of 96 channels of vibration data to be recorded for each flight condition. To record the total of 182 channels, the accelerometers were relocated and all flight conditions were repeated. Twenty channels of temperature data were hand-recorded from a single temperature display by manually switching to the desired temperature pickup. The nose of the helicopter was pointed toward the sun for all temperature measurements. The parameters required to define the flight condition were hand-recorded from calibrated ship's standard instruments.



Table 1. CH-54B Vibration Test Conditions.

Test	Conditions <sup>1</sup>	Average Density Altitude (ft)	Average Temperature (°C)
Hover	In ground effect (IGE), clean, pod; out of ground effect (OGE), clean, pod, sling load.	4200	23
Level flight (LF)	$V_H^2$ (104 KCAS <sup>3</sup> ), $0.9V_H$ , $0.8V_H$ , $0.7V_H$ , $V_{loiter}$ (55 KCAS); clean. $V_H$ (100 KCAS), $0.9V_H$ , $0.8V_H$ , $0.7V_H$ , $V_{loiter}$ (55 KCAS); pod. $V_H$ (90 KCAS), $0.9V_H$ , $0.8V_H$ , $0.7V_H$ , $V_{loiter}$ (55 KCAS); sling load.	5300	21
Climb	$V_{best R/C}^4$ (60 KCAS, $V_{cruise R/C}$ (80 KCAS); power for 2000 ft/min R/C, clean; maximum continuous power, pod, sling load.	5300	21.5
Descent	$V_{min R/D}^5$ (60 KCAS, minimum governing power; $V_{cruise R/D}$ (80 KCAS), 500 ft/min; clean, pod, sling load.	5300	21.5
Takeoff (T/O A)	From 10-foot hover, clean, pod; from 50-foot hover, sling load.	4100	22
Landing (LDG)	Landing A, to 10-foot hover, clean, pod; to 50-foot hover, sling load. Landing B, to touchdown, clean, pod.	4100	22
Maneuvering	90° turns at constant altitude, 100-KCAS entry airspeed, 15° and 30° bank angles, right and left, clean, pod; 90-KCAS entry airspeed, 10° and 20° bank angles, right and left, sling load.	5300	23
Ground run	Flight idle (185 rpm), ground idle (70 rpm), APP <sup>6</sup> only	4500	29

<sup>1</sup>Coordinated flight maintained at level flight, climb, descent, and maneuvering test conditions.

Average gross weights tested: 28,400 pounds, clean; 41,900 pounds, pod and sling load.

Main rotor speed: 100 percent (185 rpm).

<sup>2</sup> $V_H$ : Maximum level flight airspeed.

<sup>3</sup>KCAS: Knots calibrated airspeed.

<sup>4</sup>R/C: Rate of climb.

<sup>5</sup>R/D: Rate of descent.

<sup>6</sup>APP: Auxiliary power plant.

7. A total of 10,019 vibration data records were recorded and narrow-band spectral analyses were performed on 9810 of these data records. To present the results of the spectral analysis in a form which could be more easily comprehended than the 9810 spectral analysis plots, a statistical method of summarizing the data on a digital computer (referred to as data compression) was developed. The data were compressed by selecting groups of the 9810 spectral analysis plots and summarizing each of these groups in two compressed data plots. These two compressed data plots show the maximum acceleration and the mean plus 3-standard-deviation (3-sigma) acceleration with the mean acceleration in the form of a frequency spectrum similar to the individual spectral analysis plots. The mean plus 3-sigma acceleration value is that acceleration below which 99.87 percent of all data recorded fell. Data compression was accomplished by taking the acceleration value at each of the 500 frequencies which were output by the spectral analyzer for all spectral analysis plots in a compression group and finding the maximum and minimum acceleration, the mean acceleration, and the mean plus 3-sigma acceleration. With the data compression plots which present the maximum acceleration values, a table is provided which lists the flight condition, accelerometer location, and axis at which each maximum acceleration occurred. The equations used to calculate the mean and standard deviation and a block diagram of the spectral analysis and data compression systems are presented in appendix F.

8. The flight conditions selected for the vibration testing were intended to cover all normal flight conditions encountered in operational use of the CH-54B helicopter. The first pass of the data compression grouped the data according to flight condition. The second and third data compression passes combined all of the flight conditions in proportion to the number of columns each flight condition occupies in the data array (figs. 1 through 3, app G). For example, landings comprise 5 out of 55 columns or 9 percent of the data which, in the compressions that combine flight conditions, represents a flight during which 9 percent of the flight time is spent in landings. The first-pass data compressions may be used to combine flight conditions in any proportion desired.

### CHRONOLOGY

9. The chronology of testing was as follows:

Test request received	14	September	1970
Test aircraft available	18	July	1972
Test flying initiated	22	August	1972
Test flying completed	29	September	1972

## RESULTS AND DISCUSSION

### GENERAL

10. The CH-54B instrument and avionics vibrations were found to be primarily sinusoidal with a random variation of amplitude with time at each discrete frequency. The primary forward fuselage instrument and avionics vibration source was the main rotor with a maximum mean plus 3-sigma acceleration of 0.41g at the main rotor 6-per-rotor-revolution (6/rev) frequency of 18.5 hertz (Hz). The primary aft fuselage avionics vibration sources were gearboxes, shafts, and other rotating components with a maximum mean plus 3-sigma acceleration of 4.0g at 55.5 Hz. All instrument and avionics mean plus 3-sigma vibration levels were below the laboratory qualification vibration levels of MIL-STD-810B (ref 6, app A). The pilot seat pad did not attenuate main rotor-induced vibrations; however, vibrations above 10 Hz were attenuated by the pilot's body. The maximum mean plus 3-sigma vibration level for all locations tested was 117g at 1915 Hz at the auxiliary power plant. Main rotor-induced vibration harmonic content and amplitudes for the CH-54B were lower than those of the OH-58A and UH-1H helicopters. The CH-54B aft fuselage vibration levels from 50 Hz to 2000 Hz were higher than the aft fuselage vibration levels of the OH-58A and UH-1H helicopters. The highest instrument and avionics temperatures were recorded in the cabin area under static conditions and decreased in forward flight. Under certain environmental conditions the Wet Bulb Globe Temperature index is excessively high at the pilot station. The results of this test indicate the data in this and previous environmental test reports should be applied to revising the appropriate military environmental specifications and improved vibration isolation methods should be developed.

### VIBRATION DATA

#### Data Relevancy

11. Experience shows that there is a wide variation in the vibration level of different helicopters of the same model due to differences in the mechanical condition of each helicopter. Thus, if vibration levels are to be measured which are representative of those encountered in a particular model of helicopter, then a sample of several units of this model of helicopter must be tested. All of the data in this report are from one CH-54B helicopter, S/N 69-18463, which was obtained from Sikorsky Aircraft by USAASTA with 317 flight hours and accumulated 70 additional flight hours at USAASTA before this vibration test was conducted.

## Data Presentation

12. The data were summarized in three data compression passes and in 10 special-purpose compressions. Each data compression is presented as two plots: maximum acceleration recorded versus frequency and mean with mean plus 3-sigma acceleration versus frequency. The mean plus 3-sigma acceleration values are felt to best represent the test data, since accelerations in excess of the mean plus 3-sigma limit were recorded less than 0.13 percent of the time. This result indicates that accelerations in excess of the mean plus 3-sigma limit would be only rarely encountered in operational use of the helicopter. The data grouping used in each compression pass are summarized in table 2, with details of the data compression shown in the data arrays (figs. 1, 2, and 3, app G). In the data array, each square represents a spectral analysis data point. The numbers assigned to each group of squares in the data array represent a compression group, with squares with like numbers belonging to the same compression group. This compression group number is written on each compressed data plot for identification. The special-purpose compressions combine all axes and flight conditions for the accelerometer locations of interest. The special-purpose compressions were used to determine transmissibility and pilot station vibrations. The specific locations compressed are indicated on transmissibility and pilot station vibration plots.

13. The instrument and avionics third-pass compression results are presented in table 3 and in figures A and B in the body of this report. The second-pass compression results are presented in appendix G for all accelerometer locations. Only the instruments, avionics, and pilot station compressions are presented in appendix G for the first pass compressions. The first pass compressions for the other locations are available from USAASTA. For the second and third compression passes a table is presented with the plot of the maximum accelerations which lists the accelerometer location, axis, and flight condition at which each significant peak occurred. For the third pass compression this table is expanded to include the source of the significant accelerations. The acceleration values which are presented in this report are one-half of the peak-to-peak value. The individual spectral analysis data, on digital magnetic tape, are available from USAASTA.

## Instrument and Avionics Vibration

14. Instrument and avionics vibration data were gathered from 16 triaxial accelerometer locations at the test conditions shown in table 1. Accelerometer locations are described in detail in table 2, appendix D, and shown in photographs in appendix E. The third pass forward fuselage data compressions are presented in figures A and B in the body of this report. Second pass data compressions are presented in figures 4 through 9, appendix G, and first pass data compressions are presented in figures 53 through 94, appendix G. The data were found to be primarily sinusoidal with a random variation of acceleration amplitude with time at each discrete frequency. The random amplitude variation was usually less than 30 percent of the acceleration amplitude mean value and was apparently due to small changes in variables such as light turbulence or small control inputs. There was a significant difference in vibration frequency content between the forward

Table 2. Data Compression Grouping.

Compression Pass	Group <sup>1</sup>	Group Elements (location number)	Number of Group Elements	Number of Compressions
1st	Equipment	Instruments (1, 2, 3, 4, 5, 6, 7) Avionics, forward fuselage (8, 9, 10, 11, 12, 13) Avionics, aft fuselage (14, 48, 56) Pilot input (15, 16, 17, 18, 19) Pilot output (20, 21) Tach generators (22, 23, 24) Transmission mounts (25, 26, 27, 28) Upper main transmission (29) 45° and 90° gearboxes (30, 31) Hanger bearings (32, 33, 34, 35, 36) Hydraulic system (37, 38, 39, 40, 41, 55) Oil cooler (42, 43) Fuel pressure switches (44, 45) Brake cylinder (46) Rotor brake support (47) Cockpit blower (49) Horizontal stabilizer tip (50) Anticollision light (51) Primary servo actuators (52, 53) AFCS servo (54) Auxiliary power plant (57, 58) Engine mounts (60, 61, 62, 63, 64) Engine (65, 66, 67, 68, 69, 70)	24	<sup>3</sup> 168
	Flight conditions <sup>2</sup>	Hover Level flight Climb Descent Takeoff and landing Turns Ground run	7	
2nd	Equipment	Same as 1st pass	24	24
	Flight conditions	All	1	
3rd	Equipment	Instruments and avionics (1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13)	1	1
	Flight conditions	All		

<sup>1</sup>All axes combined for all compressions.<sup>2</sup>Flight conditions described in detail in table 1.<sup>3</sup>Two additional compressions consisting of locations 57 and 58 combined, and location 44, were calculated for the APP-only ground test condition.

Table 3. Instruments and Avionics Maximum Accelerations for Figure A.<sup>1</sup>

Frequency (~ Hz)	Flight Condition <sup>2</sup>	Configuration	Axis	Location Number	Amplitude (~ g)	Source
5	OGE	Sling load	Longitudinal	7	0.54	--
12	LDG A	Pod	Longitudinal	7	0.22	--
18	LDG A	Pod	Longitudinal	7	0.70	Main rotor 6/rev
37	LDG A	Pod	Longitudinal	2	0.73	Main rotor 12/rev
50	Left, 25°	Pod	Longitudinal	1	0.16	Tail rotor drive shaft
56	LDG B	Clean	Longitudinal	1	0.17	Main rotor 18/rev
74	V cruise R/C	Clean	Longitudinal	1	0.15	Main rotor 24/rev
256	LDG A	Pod	Longitudinal	12	0.24	Gas producer
368	LF (V <sub>H</sub> )	Clean	Lateral	13	0.35	--

<sup>1</sup>All instruments and forward fuselage avionics.

<sup>2</sup>Flight condition abbreviations defined in table 1.

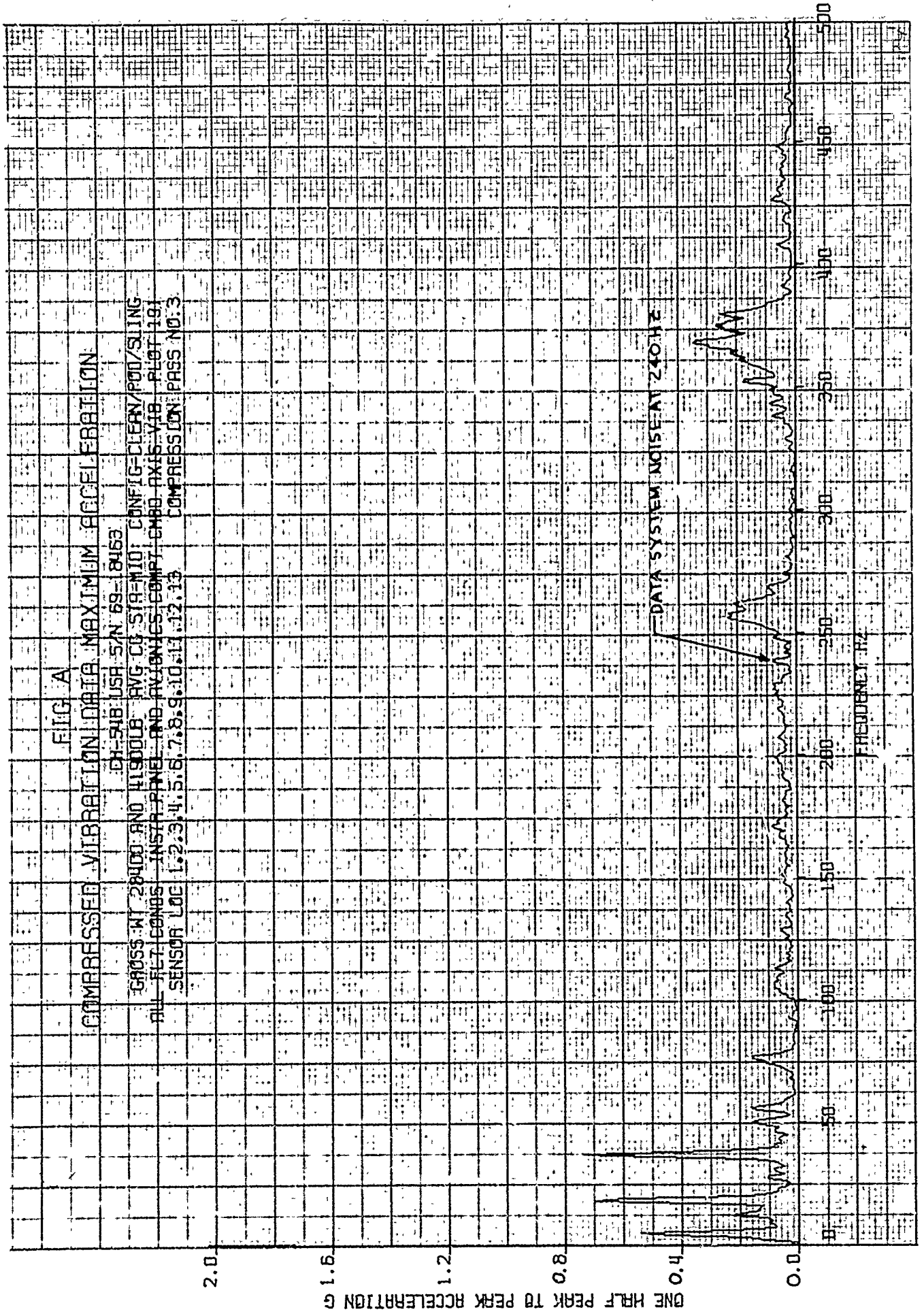
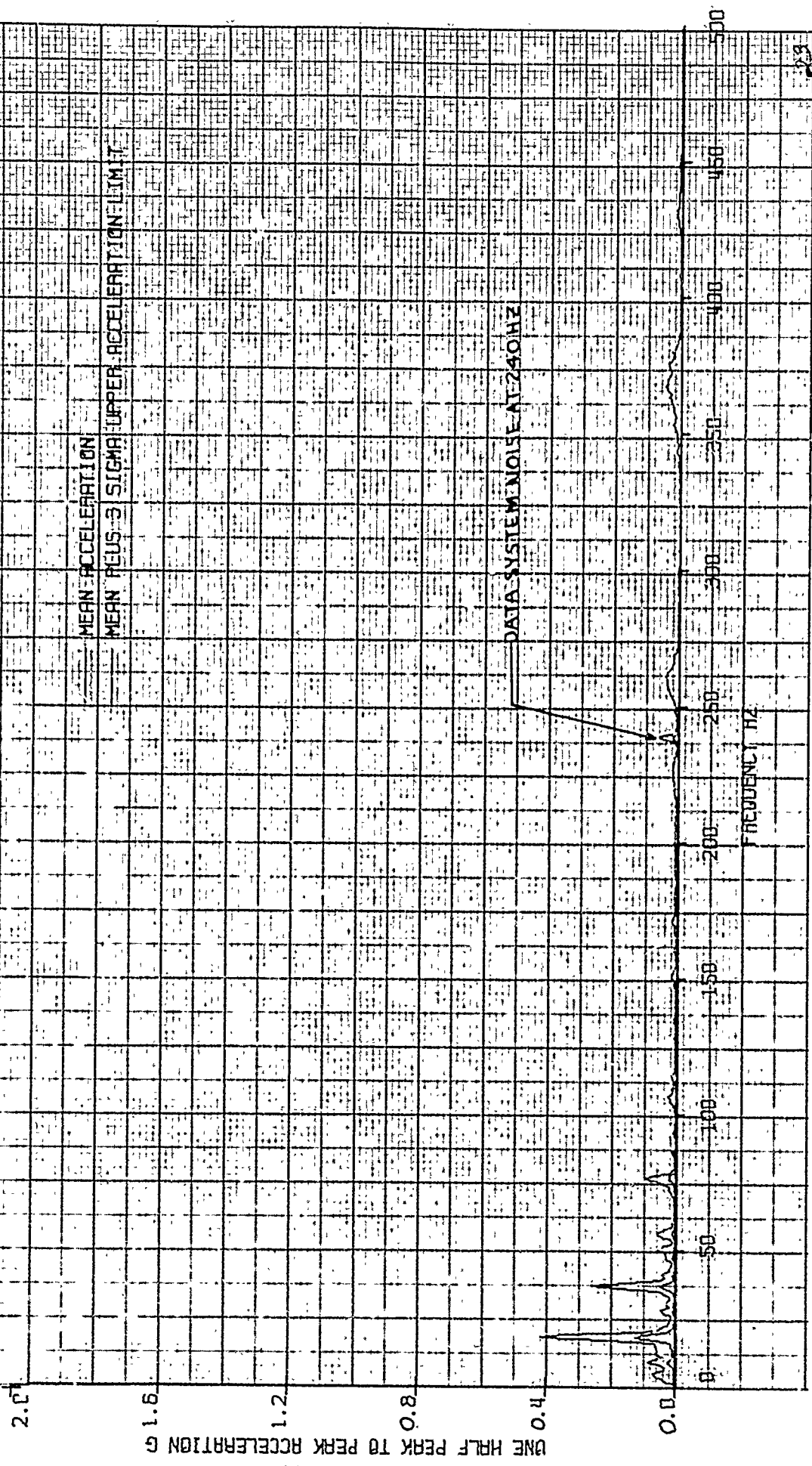


FIG. B  
COMPRESSED VIBRATION DATA

GROSS WT. 28400 LBS. USA 371-83-10483  
 ALL FLT. COND'S INSTR. PANEL AND AVIONICS COMPT CMAD AXIS VIB. PLOT 191  
 SENSOR LOC. 1.2, 3.14, 3.6, 7.8, 9, 10, 11, 12, 13 COMPRESSION PASS NO. 3





and aft fuselage areas. In the forward fuselage area the main rotor was the primary vibration source, with the tail rotor drive shaft and engine also causing significant vibrations. In the aft fuselage area the primary vibration sources were the tail rotor, tail rotor drive train, main transmission, and numerous other rotating components located in the main transmission area. Table 4 lists the primary CH-54B vibration sources and their frequency at 100 percent main rotor speed. Main rotor speed was set at 100 percent  $\pm 1$  percent during this testing. In the forward fuselage area a maximum mean plus 3-sigma acceleration value of 0.42g at the main rotor 6/rev frequency of 18.5 Hz was recorded (fig. B). A peak acceleration value of 0.74g at the main rotor 12/rev frequency of 37 Hz (fig. A) was recorded along the longitudinal axis on the lower right portion of the instrument panel (location 7) during a landing. Low-level vibrations at main rotor noninteger harmonics of 3/rev (9.2 Hz) and 9/rev (27.7 Hz) frequencies were consistently observed with a maximum mean plus 3-sigma acceleration of 0.08g at 9.2 Hz. Vibrations at frequencies of 5 Hz and 12 Hz were also occasionally observed. In the aft fuselage area (figs. 8 and 9, app G) vibrations were of higher amplitude and frequency than in the forward fuselage area. A maximum mean plus 3-sigma acceleration of 4.0g was recorded at the tail rotor 4/rev and main rotor 18/rev frequency of 55.5 Hz. A peak acceleration of 5.03g was recorded at the main transmission first stage planetary gear mesh frequency of 1400 Hz along the lateral axis at the automatic flight control system transducer package (location 14) during a 25-degree bank left turn.

#### Comparison with the Military Standard

15. Figure C shows a laboratory vibration test curve for equipment installed in helicopters taken from figure 514.1-3 of the military standard, MIL-STD-810B (ref 6, app A). The ordinate is changed from units of vibration amplitude as the curve is presented in MIL-STD-810B to units of vibration acceleration to be compatible with the data presented in this report. The significant mean plus 3-sigma acceleration and limits from figure B and figure 9, appendix G, are plotted on this specification curve with previously acquired OH-58A vibration data (ref 2, app A) and UH-1H vibration data (ref 3). This specification curve does not limit helicopter instrument and avionics vibration levels but gives vibration levels to be used for laboratory qualification of instruments and avionics for helicopter use. A data compression composed of only equipment mounted on isolators was not calculated, since the lower curve of figure C assumes that the vibration isolators will reduce vibrations above a frequency of 33 Hz, which was not the case for the vibration isolators tested. All instrument and avionics mean plus 3-sigma vibration levels are below the test curve of MIL-STD-810B. The forward fuselage-mounted equipment vibration levels are well below the test curve of MIL-STD-810B, while the aft fuselage-mounted equipment vibration levels are higher and approach the test curve of MIL-STD-810B in the 50-Hz area.

Table 4. CH-54B Vibration Sources.

Main rotor speed: 185 rpm

Source		Frequency (~ Hz)
Main rotor	Fundamental	3.1
	6/rev	18.5
	12/rev	37.0
	18/rev	55.5
	24/rev	74.0
	30/rev	92.5
Tail rotor	Fundamental	14.1
	4/rev	56.4
	8/rev	113.0
	12/rev	169.2
	16/rev	225.6
	20/rev	282.0
Tail rotor drive shaft (engine to 45° gearbox)	Fundamental	50.3
Tail rotor drive shaft (45° gearbox to 90° gearbox)	Fundamental	41.1
Gas producer (100 percent)	Fundamental	267
Power turbine (100 percent)	Fundamental	150
90° gearbox gear mesh	Fundamental	864
45° gearbox gear mesh	Fundamental	1352
Main transmission input bevel gear mesh	Fundamental	1910
Main transmission first stage planetary gear mesh	Fundamental	1386
Main transmission second stage planetary gear mesh	Fundamental	711

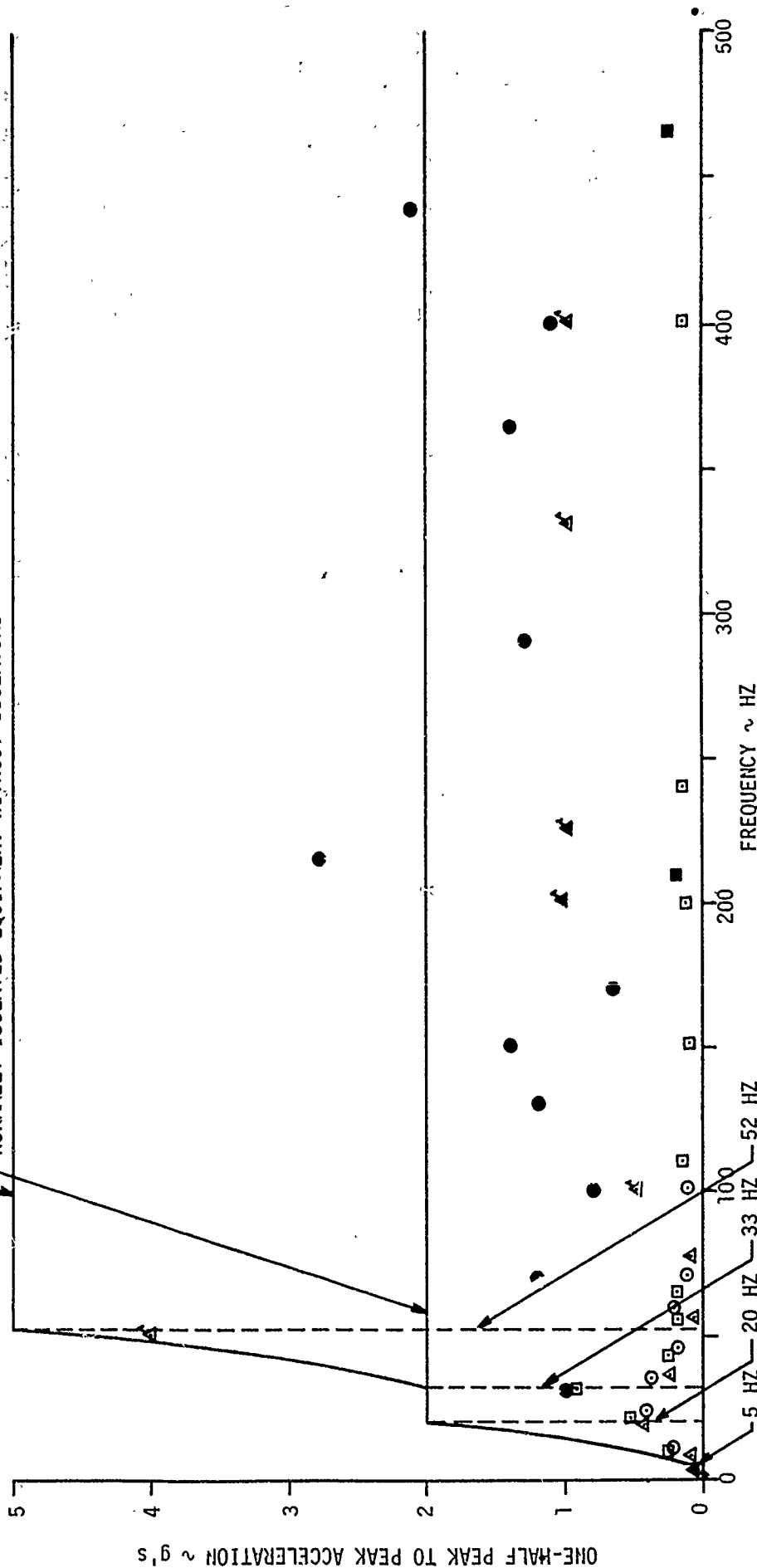
FIGURE C  
COMPARISON WITH LABORATORY VIBRATION TEST CURVES FOR EQUIPMENT INSTALLED IN HELICOPTERS  
CURVES FROM MIL-STD-810B, FIG 514.1-3  
MEAN PLUS 3 SIGMA ACCELERATION, ALL INSTRUMENTS  
AND AVIONICS, ALL AXES, ALL CONDITIONS

NOTE: SHADED SYMBOLS DENOTE  
WEAPONS FIRING.  
OPEN SYMBOLS DENOTE NON  
WEAPONS FIRING.  
FLAGS DENOTE EQUIPMENT  
IN AFT FUSELAGE

HELICOPTER  
OH-58A  
UH-1H  
CH-54B

SYMBOL  
○ □ △

ALL EQUIPMENT WITH MOUNTS  
NORMALLY ISOLATED EQUIPMENT WITHOUT ISOLATORS



### Isolation Mount Characteristics

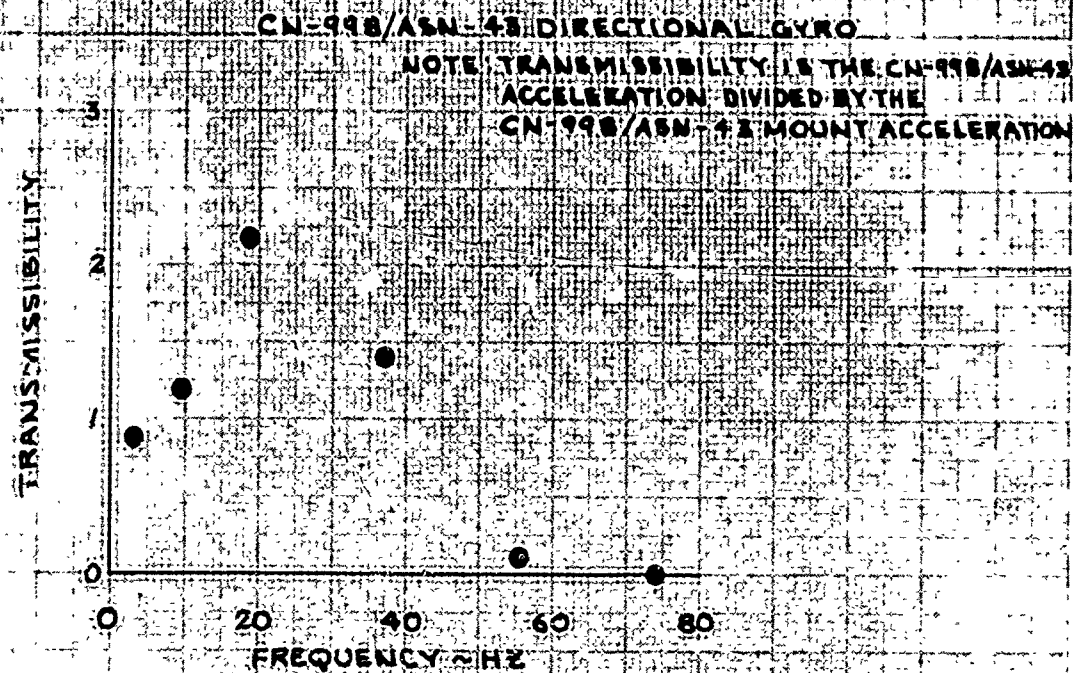
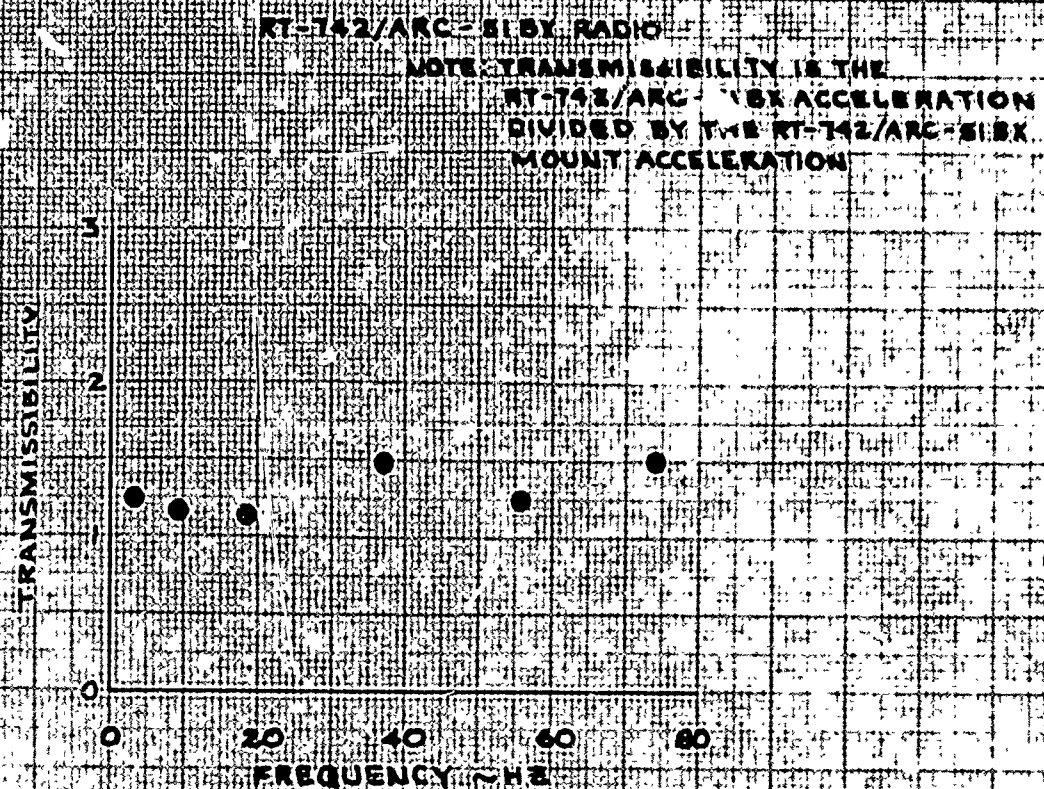
16. The transmissibility of the isolation mounts on the RT-742/ARC-51BX radio and CN-998/ASN-43 directional gyro was evaluated at the CH-54B driving frequencies. Transmissibility was determined by measuring the input and output accelerations across the isolation mounts and calculating the ratio of output to input acceleration. The input and output accelerations used were those determined from the mean plus 3-sigma compressions of all axes and all flight conditions. This ratio is plotted as a data point at each driving frequency in figure D. The results indicate that the isolation mounts significantly amplify CH-54B driving frequencies below 74 Hz for the RT-742/ARC-51BX radio and between 5 Hz and 40 Hz for the CN-998/ASN-43 directional gyro. This amplification is apparently due to isolator resonant frequencies which are near the helicopter driving frequencies. Above 40 Hz, the directional gyro isolation mounts were effective; however, the ARC-54BX radio isolation mounts were not effective at any measured driving frequencies. The amplification of vibrations in this low-frequency range is highly undesirable, since severe CH-54B instrument and avionics vibrations occur at these low frequencies. Amplification by the vibration isolators is a shortcoming, correction of which is desirable. Improved vibration isolation for instrument and avionics components should be provided.

### Pilot Station Vibrations

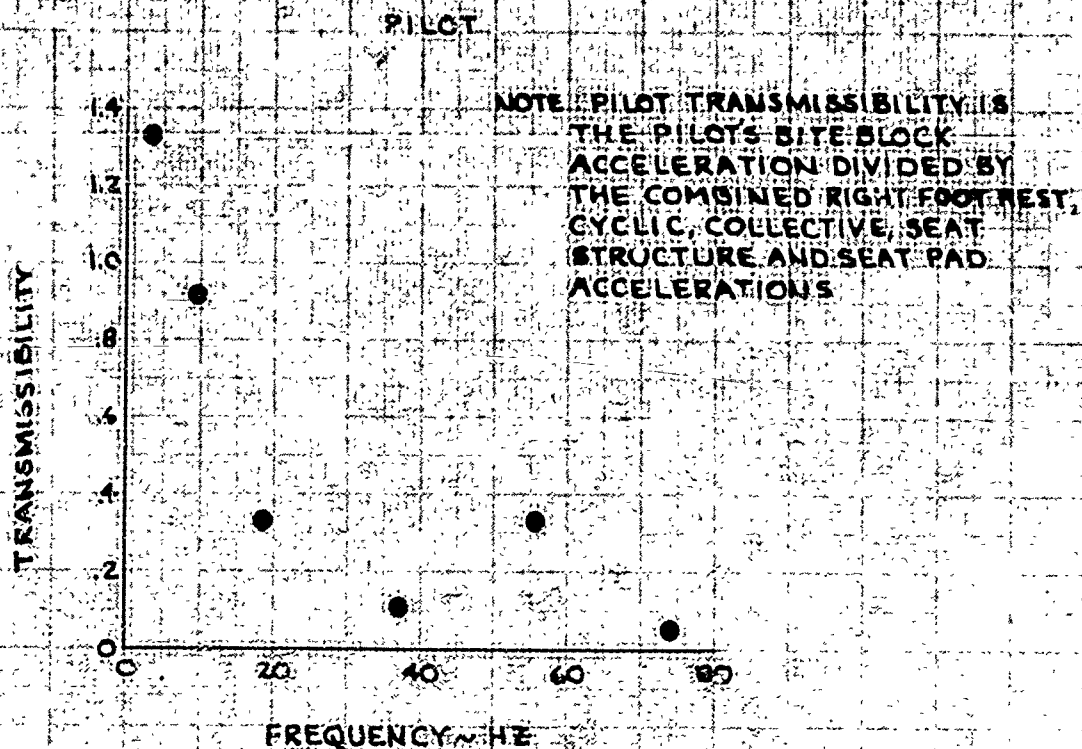
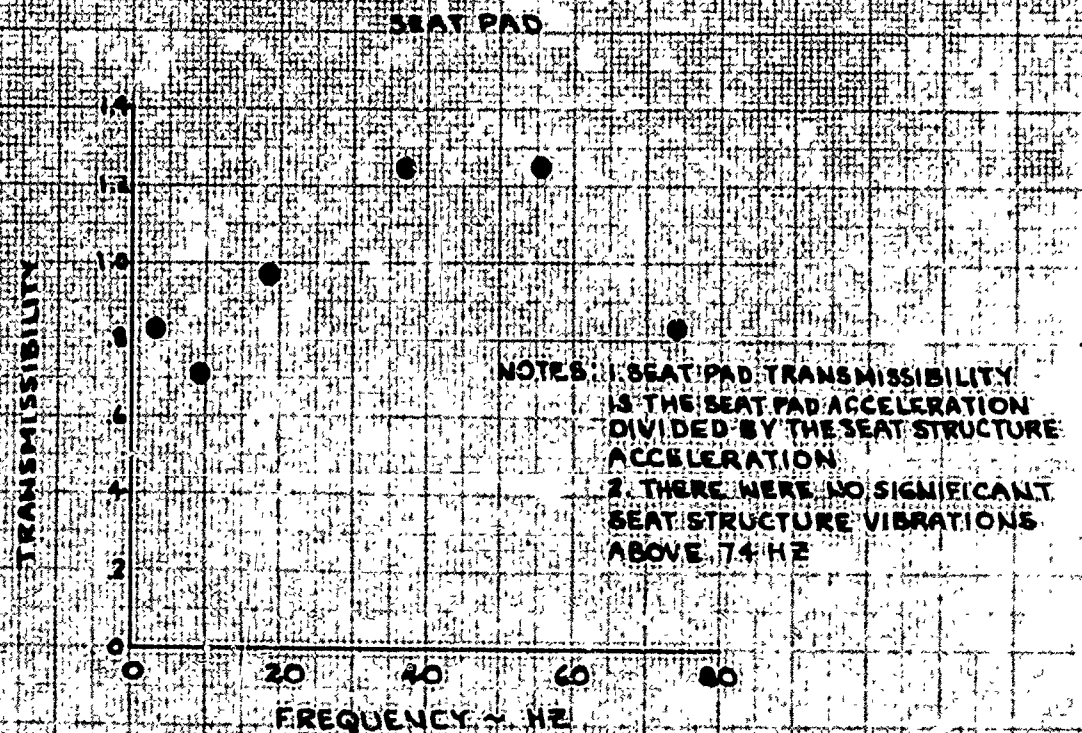
17. Pilot station vibrations were measured at the pilot collective grip, cyclic grip, right pedal foot rest, seat structure, seat pad, bite block, and helmet at the conditions shown in table 1. Accelerometer locations are described in detail in table 2, appendix D, and are shown in photographs in appendix E. The second-pass data compressions are presented in figures 10 through 13, appendix G, and the first-pass data compressions are presented in figures 95 through 122. The pilot for which this data were recorded weighed 175 pounds and was 68 inches tall. Fifty pounds of ballast was placed on the floor beneath the pilot seat to simulate the fuselage response due to a 225-pound pilot station loading.

18. The transmissibility of the seat pad was evaluated by calculating the ratio of the seat pad acceleration to the seat structure accelerations at CH-54B driving frequencies. These ratios are plotted in figure E. Seat pad acceleration was measured by attaching an accelerometer to the bottom of a 10-inch by 6-inch by 0.020-inch aluminum plate on which the pilot sat. The accelerations used were those determined from the mean plus 3-sigma compressions of all axes for the seat pad and seat structure. Results indicate that there is little attenuation of seat structure vibrations by the seat pad in the frequency range of main rotor-induced vibrations. Since vibrations are induced by the main rotor, consideration should be given to use of a seat cushion which would attenuate vibrations in the frequency range of the main rotor.

FIGURE D  
VIBRATION ISOLATOR TRANSMISSIBILITY  
CH-54B USAF/AF-10442  
ALL AXES COMBINED  
ALL FLIGHT CONDITIONS



**FIGURE E**  
**SEAT PAD AND PILOT TRANSMISSIBILITY**  
 CH-53E USAF 69-18463  
 ALL AXES COMBINED  
 ALL FLIGHT CONDITIONS



19. The pilot's head vibrations were measured with an accelerometer attached to a bite block. The bite block was a plastic and aluminum form shaped to fit the pilot's teeth which the pilot held securely in his mouth when vibrations were recorded from this location. The ratio of the bite block acceleration to the combined collective grip, cyclic grip, right pedal foot rest, seat structure, and seat pad accelerations was calculated and is presented as pilot transmissibility in figure E. The results show that the pilot's body attenuates vibrations above 10 Hz. The pilot station vibration limits of paragraph 3.7.1b of MIL-H-8501-A (ref 7, app A) are compared to the seat structure mean plus 3-sigma accelerations for all axes in figure F. The data are divided into two groups: hover, level flight, climb, and descent compose one group while takeoff, landing, and turns compose the other group. There is no specification limit on vibration levels during maneuvering flight, so these data were combined with the takeoff and landing transition data, since most maneuvers are transient conditions. There is a specification vibration limit for flight from  $V_{cruise}$  to  $V_{limit}$  airspeeds but no data were grouped for this condition, since the  $V_{cruise}$  and  $V_{limit}$  airspeeds are identical for the CH-54B helicopter. The results show that specification requirements were not exceeded. The highest vibration levels were at the main rotor 6/rev frequency with the magnitude of vibrations at all other frequencies well below those at the 6/rev frequency.

#### Selected Component Vibration Characteristics

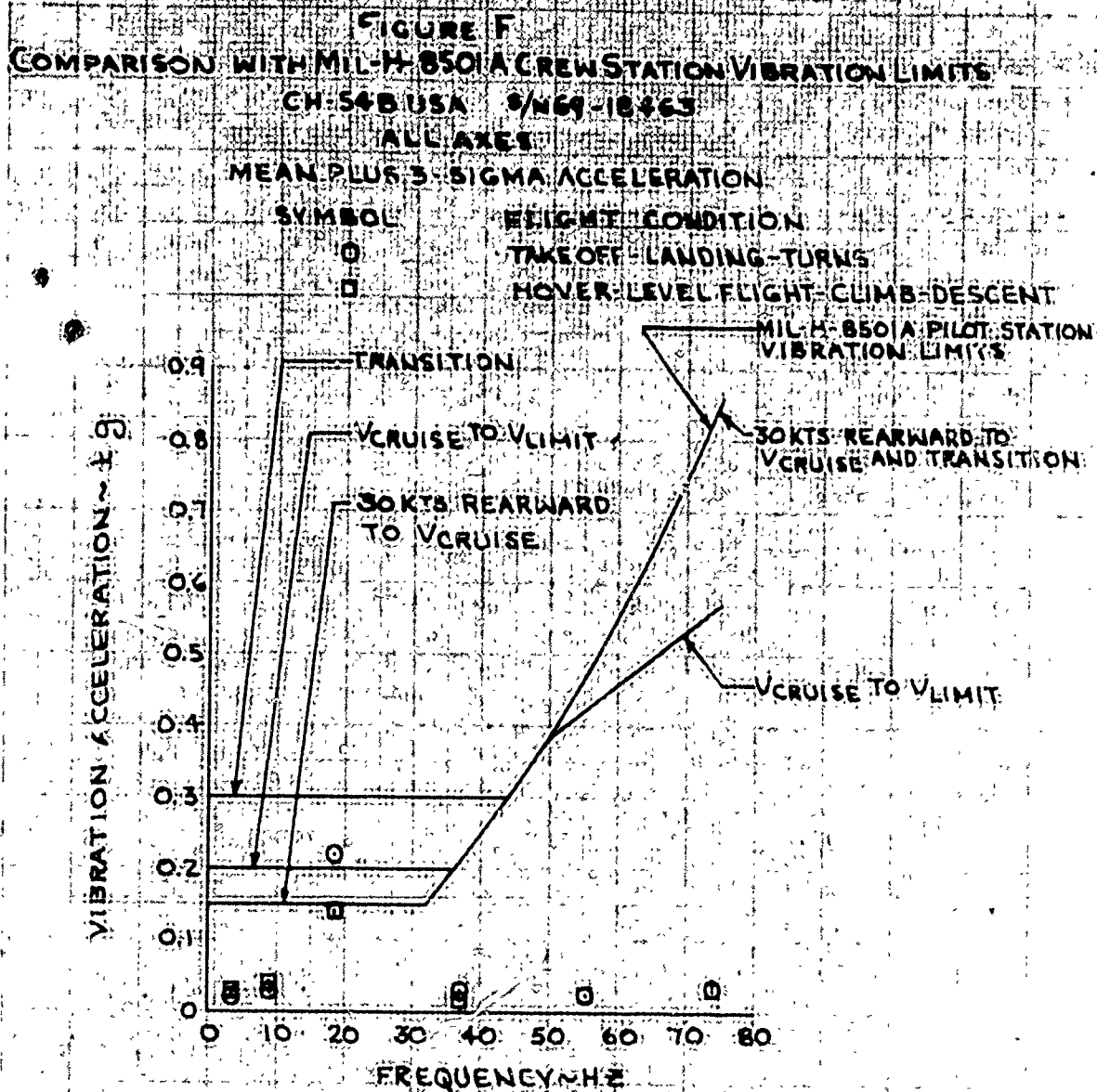
20. Vibration data were recorded at 47 locations throughout the helicopter other than instruments, avionics, and the pilot station. These locations are described in table 2 and appendix D and are shown in photographs in appendix E. Data were recorded at the test conditions listed in table 1. These vibration data were recorded at the request of the United States Army Air Mobility Research and Development Laboratory (USAAMRDL), Eustis Directorate, and were transmitted to USAAMRDL in the Northrop Corporation data report (ref 8, app A). The selected component second-pass data are presented in this report in figures 14 through 52, appendix G. The selected component first-pass data are not presented in this report but are available from USAASTA.

21. The vibration characteristics at these 47 locations will not be discussed in detail but, in general, show the presence of high-level, high-frequency vibration near rotating equipment, particularly gearboxes. The maximum mean plus 3-sigma vibration acceleration level recorded for all locations was 117g at 1915 Hz at the APP (fig. 45, app G). The source of this APP vibration was identified as the main transmission input bevel gear mesh frequency.

#### Comparison with Previous Environmental Test Data

22. Vibration data gathered from the OH-58A helicopter (ref 2, app A) and the UH-1H helicopter (ref 3) are compared with the CH-54B vibration data in figure C. The primary CH-54B main rotor-induced vibrations were at the main rotor first (6/rev) harmonic frequency with some significant vibrations at the main rotor second (12/rev) harmonic frequency. The primary OH-58A and







UH-1H main rotor-induced vibrations were at the main rotor first (2/rev), second (4/rev), and third (6/rev) main rotor harmonic frequencies, with significant vibrations up to the main rotor ninth or tenth harmonic frequencies. The CH-54B main rotor-induced vibrations showed less main rotor harmonic frequency content and their levels were lower than those of the OH-58A and UH-1H helicopters. However, the aft fuselage vibration levels from 50 Hz to 2000 Hz were higher in the CH-54B than in the OH-58A and UH-1H helicopters.

## TEMPERATURE DATA

### Component Air Temperatures

23. Component-part surrounding air temperatures were recorded at 20 locations described in table 3, appendix D, and are shown in photographs in appendix E. Temperatures were recorded for static hot soaks in the sun, level flight between 60 and 100 KCAS, and IGE and OGE hover. The helicopter was headed toward the sun for all temperature measurements. All vents and the pilot and copilot doors and windows were open and the cabin cooling fans were on for in-flight temperature measurements. Static temperatures were recorded with the vents, windows, and doors open and closed. Temperature data for all conditions are presented in table 5. Detailed static temperature data are presented in figures 123 through 126, appendix G, for locations with a temperature rise of 9°C or greater. Temperature rise was determined by subtracting the outside air temperature from the component temperature of interest.

24. It was found that solar radiation had a significant effect on static temperatures but only a small effect on in-flight temperatures. In-flight data were obtained over a range of solar radiation values by recording data at different times of day from morning until afternoon. Less than 10 minutes were required for in-flight temperatures to stabilize at steady-state values. The in-flight temperature data presented in table 5 were obtained by averaging the temperature data over the range of solar radiation values tested. Static temperatures required about 2 hours to stabilize. This long stabilization time required that temperatures be recorded around noon, when solar radiation was nearly constant, for a 2-hour period. To determine static temperatures for values of solar radiation and ambient air temperature different than those tested an analytical method was developed which is described in appendix F. Figures 123 through 126, appendix G, are the results of this analytical method with representative solar radiation values (refs 9 and 10, app A) also shown.

25. Static temperature data for the cabin and avionics locations are tabulated at a solar radiation value of 350 BTU/hr-ft<sup>2</sup> and outside air temperature of 45°C in table 5. These results show that high temperatures in the forward cabin area occur under static conditions and decrease in flight due to increased air circulation. Temperatures in the engine and transmission areas were low under static conditions but increased in flight due to engine and transmission heat. The high forward cabin static temperatures are due to large amounts of transparent area in the forward

Table 5. Average Temperature Rise.

CH-54B USA S/N 69-18463

Location Number	Location Name	Average Temperature Rise ( $\sim$ $^{\circ}$ C) <sup>1</sup>			
		In-Ground-Effect Hover <sup>2</sup>	Out-of-Ground Effect Hover <sup>2</sup>	Level Flight <sup>2</sup>	Static <sup>3</sup>
1	Forward avionics	3.6	3.7	2.6	9.0
2	Instrument panel back	8.2	6.1	6.7	23.0
3	Forward cabin	5.2	5.0	3.7	25.0
4	Aft cabin	4.3	4.0	3.8	11.0
5	Transmission avionics	9.2	8.5	1.9	No data
6	Main rotor tach generator	18.0	6.1	16.5	Zero
7	Gas producer tach generator	17.1	16.5	17.8	Zero
8	Power turbine tach generator	16.7	2.6	1.4	5.0
9	No. 1 hanger bearing	20.0	9.2	16.2	3.0
10	No. 2 hanger bearing	4.9	Zero	17.7	1.0
11	No. 3 hanger bearing	Zero	Zero	15.4	1.0
12	No. 4 hanger bearing	Zero	Zero	13.8	1.0
13	No. 5 hanger bearing	Zero	Zero	11.4	1.0
14	90-degree gearbox	2.8	2.4	Zero	2.0
15	45-degree gearbox	2.6	2.6	9.0	2.0
16	Hydraulic sled	19.2	9.0	16.5	2.0
17	Hoist bay	20.8	27.4	21.9	2.0
18, 19	Main transmission	25.7	17.4	16.4	Zero
20	APP area	17.4	12.2	15.8	Zero

<sup>1</sup>Average temperature rise calculated by subtracting outside air temperature from each location temperature.

<sup>2</sup>Average solar radiation of 193 BTU/hr-ft<sup>2</sup>, windows and vents open.

<sup>3</sup>Data standardized to a solar radiation of 350 BTU/hr-ft<sup>2</sup>. Outside air temperature of 45 $^{\circ}$ C. Windows and vents closed.

<sup>4</sup>Average of both locations.

section of the fuselage, which allow solar radiation to enter. The highest average temperature rise recorded was 27.4°C at the hoist bay area during an OGE hover.

#### Wet Bulb Globe Temperature Index

26. The Wet Bulb Globe Temperature (WBGT) index, as described in reference 11, appendix A, was recorded in flight with all vents and the pilot and copilot doors and windows open and the cockpit cooling fans on. A sensing unit consisting of a dry bulb thermometer, wet bulb thermometer, and black globe thermometer was located near the pilot in the sun. The sensing unit was obtained from the United States Army Medical Equipment Research and Development Laboratory, Fort Totten New York, and is shown in photograph 61, appendix E. Dry bulb and black globe temperatures versus solar radiation and airspeed are presented in figure G.

27. The WBGT index is used to describe the effect of the temperature environment on the human body. It is determined by adding 70 percent of the naturally convected wet bulb temperature, 20 percent of the black globe temperature, and 10 percent of the dry bulb temperature. Temperatures are in degrees Fahrenheit. The following criteria for application of the WBGT index are proposed in Department of the Army Technical Bulletin TB MED 175 (ref 11, app A):

a. When the WBGT Index reaches 82°, discretion should be used in planning heavy exercise for unseasoned personnel.

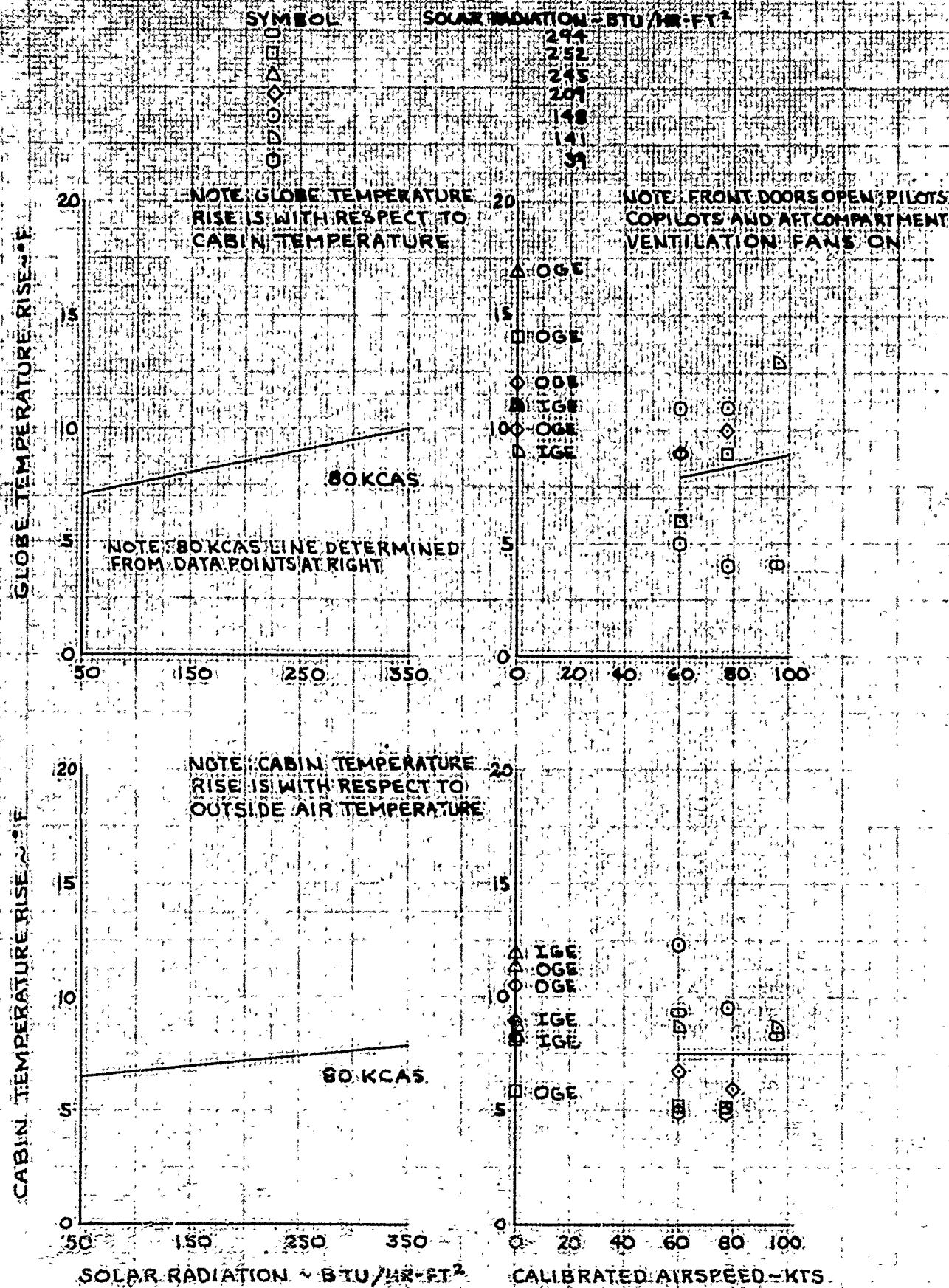
b. When the WBGT reaches 85°, strenuous exercises, such as marching at standard cadence should be suspended in unseasoned personnel during their first three weeks of training. At this temperature training activities may be continued on a reduced scale after the second week of training.

c. Outdoor classes in the sun should be avoided when the WBGT exceeds 85°.

d. When the WBGT reaches 88°, strenuous exercise should be curtailed for all recruits and other trainees with less than 12 weeks training in hot weather. Hardened personnel, after having been acclimatized each season, can carry on limited activity at WBGT of 88° to 90° for periods not exceeding 6 hours a day.

The highest WBGT index value recorded in cruise flight was 74.8°F at an outside air temperature of 88°F, a relative humidity of 41 percent, and a solar radiation value of 245 BTU/hr-ft<sup>2</sup>. Based on the data presented in figure G and a psychrometric chart, the WBGT index can be calculated for any combination of outside air temperatures, relative humidity, and solar radiation. For an outside air temperature of 100°F, a relative humidity of 50 percent, and a solar radiation of 250 BTU/hr-ft<sup>2</sup>, the WBGT index would be 93.1°F at the pilot station. This

**FIGURE G**  
**CABIN AND GLOBE TEMPERATURE AT PILOT STATION**  
**CH-54B USAF 69-18463**



calculation is described in appendix F. A WBGT index of 93.1°F is well in excess of the maximum discussed in the above criteria, and it is likely that a WBGT index higher than 93.1°F would be recorded under certain conditions. Excessively high WBGT index at the pilot station under certain environmental conditions is a shortcoming.

# CONCLUSIONS

## GENERAL

28. Analysis of the test results obtained during this evaluation resulted in the following conclusions:

- a. The CH-54B instrument and avionics vibrations are primarily sinusoidal with a random variation of amplitude with time at each discrete frequency (para 14).
- b. The primary forward fuselage instrument and avionics vibration source is the main rotor with a maximum mean plus 3-sigma acceleration of 0.41g at the main rotor 6/rev frequency of 18.5 Hz (para 14).
- c. The primary aft fuselage avionics vibration sources are gearboxes, shafts, and other rotating components with a maximum mean plus 3-sigma acceleration of 4.0g at 55.5 Hz (para 14).
- d. All instrument and avionics mean plus 3-sigma vibration levels are below the laboratory test curve of MIL-STD-810B (para 15).
- e. The pilot seat pad did not attenuate main rotor-induced vibrations (para 18).
- f. The pilot's body attenuated vibrations above 10 Hz (para 19).
- g. The maximum mean plus 3-sigma vibration level for all locations tested was 117g at 1915 Hz at the auxiliary power plant (para 21).
- h. The CH-54B main rotor-induced vibrations showed less main rotor harmonic frequency content and their levels were lower than those of the OH-58A and UH-1H helicopters (para 22).
- i. The highest instrument and avionics temperatures were recorded in the cabin area under static conditions and decreased in forward flight (para 25).
- j. The highest average temperature rise was 27.4°C above the outside air temperature at the hoist bay in an OGE hover (para 25).
- k. There were no deficiencies and two shortcomings noted during the testing.

### SHORTCOMINGS AFFECTING MISSION ACCOMPLISHMENT

29. Correction of the following shortcomings is desirable for improved operation and mission capabilities:

a. Amplification of vibrations at the main rotor driving frequencies by the vibration isolation mounts on the CN-998/ASN-43 directional gyro and RT-742/ARC-51BX radio (para 16).

b. Excessively high Wet Bulb Globe Temperature index at the pilot station under certain environmental conditions (para 27).

## **RECOMMENDATIONS**

30. The shortcomings should be corrected.
31. The data in this report and subsequent environmental test reports should be applied to revising appropriate military environmental specifications.
32. Improved vibration isolation for instrument and avionics components should be provided (para 16).



## APPENDIX A. REFERENCES

1. Letter, AVSCOM, AMSAV-EF, 31 August 1971, subject: AVSCOM Test Request No. 70-15, Instrument Panel, Avionics Compartment and Crew Station Environmental Study.
2. Final Report, USAASTA, Project No. 70-15-1, *Instrument Panel and Avionics Compartment Environmental Survey, Production OH-58A Helicopter*, September 1972.
3. Final Report, USAASTA, Project No. 70-15-2, *Vibration and Temperature Survey, Production UH-1H Helicopter*, January 1973.
4. Technical Manual, TM 55-1520-217-10/2, *Army Model CH-54B Helicopter*, 13 March 1972.
5. Test Plan, USAASTA, Project No. 70-15, *Helicopter Vibration and Environmental Survey*, July 1971.
6. Military Standard, MIL-STD-810B, *Environmental Test Methods*, 15 June 1967.
7. Military Specification, MIL-H-8501A, *Helicopter Flying and Ground Handling Qualities; General Requirements For*, 7 September 1961, amended 3 April 1962.
8. Test Data Reduction Report, NORT 73-203, Northrop Corporation Electronics Division, *Environmental Vibration Survey, CH-54B Helicopter-Tarhe*, February 1973.
9. Publication, Institut Royale Meteorologique de Belgique, *Donnes du Rayonnement Solair a Leopoldville, Periode 1953-1962*, 1965.
10. Publication, D2-90577-2, R.A. Atlas and B. N. Charles, *Summary of Solar Radiation Characteristics, Tabular Summaries*, December 1964.
11. Department of the Army Technical Bulletin, TB MED 175, *The Etiology, Prevention, Diagnosis, and Treatment of Adverse Effects of Heat*, 25 April 1969.

## APPENDIX B. AIRCRAFT INFORMATION

### DIMENSIONS AND DESIGN DATA

#### Overall Dimensions

Aircraft length (rotor turning)	88 ft, 6 in.
Height (to top of turning tail rotor)	25 ft, 4 in.

#### Main Rotor

Number of blades	6
Diameter	72.236 ft
Blade chord (constant)	26.0 in.
Solidity	0.1146
Blade twist (nonlinear)	-10.65 deg
Airfoil type	NACA 0011 modified

#### Tail Rotor

Number of blades	4
Diameter	16.0 ft
Blade chord (constant)	15.4 in.
Blade twist	Zero
Airfoil type	NACA 0012

#### Gear Ratios

Engine to main rotor	48.5437:1
Engine to tail rotor	10.5932:1

### Operating Limitations

Engine power (30 minutes)	4800 shp
Engine power (continuous)	4430 shp
Rotor speed (power ON)	100 to 104 percent
Rotor speed (power OFF)	90 to 110 percent
Maximum airspeed (sea level)	105 knots
Maximum gross weight	47,000 lb
Maximum fuel	8775 lb

### Transmission Ratings

#### Dual-engine operation:

30 minutes	7900 shp (82.3 percent Q)
Maximum continuous	6600 shp (68.8 percent Q)

#### Single-engine operation:

30 minutes	4800 shp (100 percent Q)
Maximum continuous	3300 shp (68.8 percent Q)

- 38

## APPENDIX C. CONFIGURATIONS

FIGURE 1. HELICOPTER DIAGRAM:

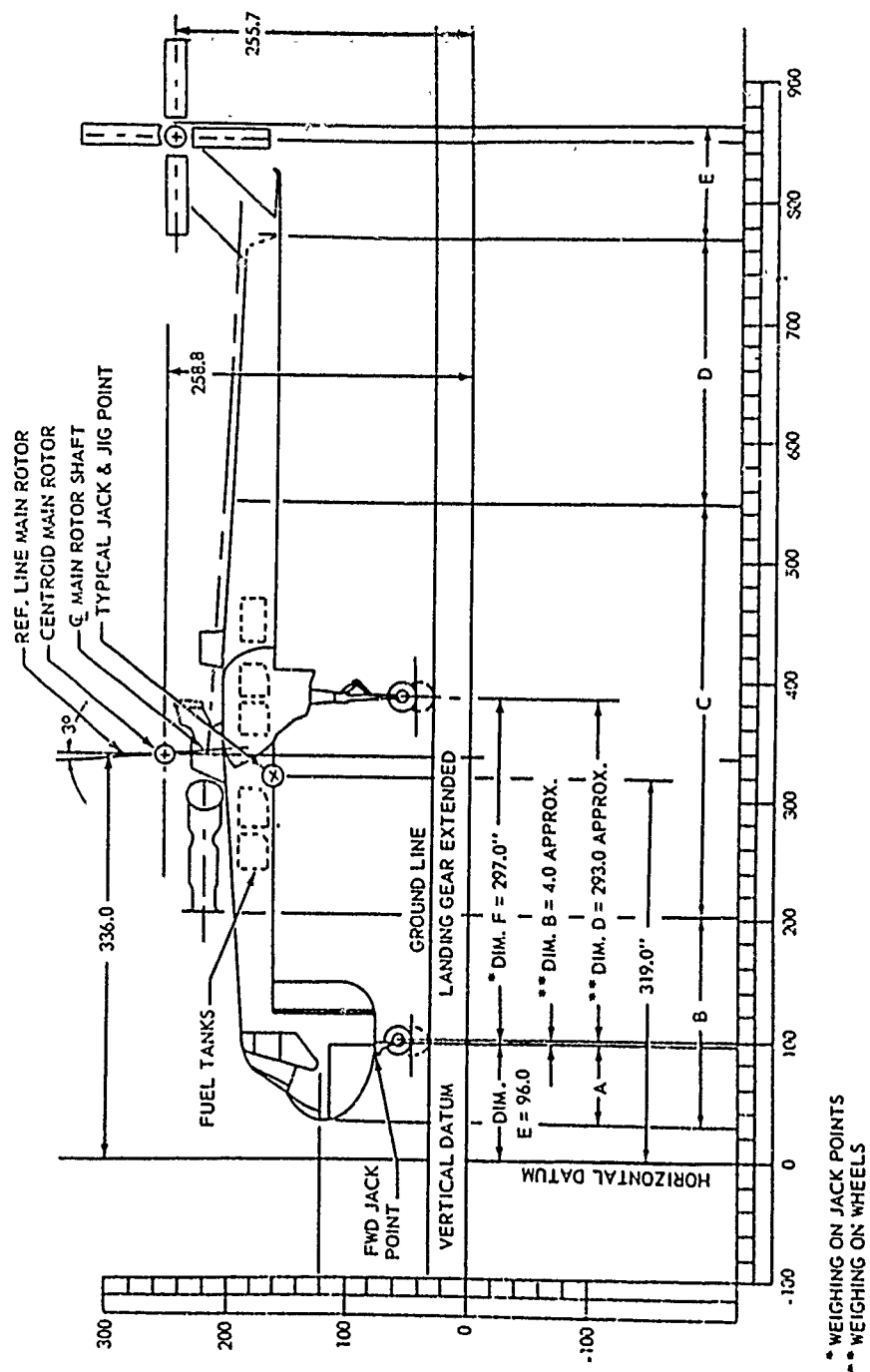


Table 1. Clean Test Configuration.

Item	Weight (lb)	Longitudinal Fuselage Station (in.)	Lateral Fuselage Station (in.)	Longitudinal Moment (in.-lb)	Lateral Moment (in.-lb)
Basic aircraft	21,986	337.0	-1.13	7,409,219	-24,945
Average fuel	5,664	359.86	Zero	2,038,226	Zero
Instrumentation	150	110	-35	16,500	-3,850
Pilot	225	94	+20	21,150	4,500
Copilot	225	94	-20	21,150	-4,500
Engineer	150	108.5	Zero	16,275	Zero
Test conditions	28,400	335.3 (mid)	-1.0, left	9,522,520	-28,795

Table 2. Sling Load Test Configuration.

Item	Weight (lb)	Longitudinal Fuselage Station (in.)	Lateral Fuselage Station (in.)	Longitudinal Moment (in.-lb)	Lateral Moment (in.-lb)
Basic aircraft	21,986	337.0	-1.13	7,409,219	-24,945
Average fuel	5,889	361.69	Zero	2,129,971	Zero
Instrumentation	150	110	-35	16,500	-3,850
Pilot	225	94	+20	21,150	4,500
Copilot	225	94	-20	21,150	-4,500
Engineer	150	108.5	Zero	16,275	Zero
Crew chief	175	127	+30	22,225	5,250
Sling load <sup>1</sup>	13,100	333	Zero	4,362,300	Zero
Test conditions	41,900	334.1 (mid)	-0.6, left	13,998,790	-23,545

<sup>1</sup>The sling load was an engine can, ballasted with concrete, with dimensions as shown:

Table 3. Pod Test Configuration.

Item	Weight (lb)	Longitudinal Fuselage Station (in.)	Lateral Fuselage Station (in.)	Longitudinal Moment (in.-lb)	Lateral Moment (in.-lb)
Basic aircraft	21,986	337.0	-1.13	7,409,226	-24,945
Average fuel	5,883	361.60	Zero	2,127,292	Zero
Instrumentation	150	110	-35	16,500	-3,850
Pilot	225	94	+20	21,150	4,500
Copilot	225	94	-20	21,150	-4,500
Engineer	150	108.5	Zero	16,275	Zero
Pod (empty)	2,881	316.3	Zero	911,260	Zero
Ballast <sup>1</sup>	10,400	330.0	Zero	3,432,000	Zero
Test conditions	41,900	333.1 (mid)	-0.7 (mid)	13,954,853	-28,795

<sup>1</sup>Pod ballast evenly distributed at longitudinal stations 290, 330, and 370.

## APPENDIX D. TEST INSTRUMENTATION

### GENERAL

1. Flight test instrumentation was installed, calibrated, and maintained by the Instrumentation and Calibration Divisions of USAASTA and USAAMRDL. This instrumentation was used to record vibration data, temperature data, and flight condition parameters. A list of the instrumentation components is presented in table 1.

### VIBRATION INSTRUMENTATION

2. An FM-FM magnetic tape system was used to record the vibration data. A block diagram of the instrumentation system is presented in figure 1. Data were recorded over a frequency range of 2 to 2000 Hz for all flight conditions. The transducers were miniature triaxial, biaxial, and uniaxial piezoelectric accelerometers which were mounted at 70 locations throughout the aircraft for a total of 182 channels of vibration data. The instrumentation was limited to recording data from 12 accelerometers simultaneously. To record more than 12 channels of data, an eight-position manual switching network was employed and each flight condition was recorded for each switch position, for a maximum data capacity of 96 channels. To obtain the total of 182 channels of vibration data, the accelerometers were relocated after completion of all test conditions and the test conditions were repeated. The maximum capacity of the instrumentation system is 96 channels without accelerometer relocation and 192 channels with one relocation. Accelerometers were bonded to the component of interest with the accelerometer axis aligned to the component axis. The mounting locations of each accelerometer are shown in the photographs in appendix E. Table 2 lists the accelerometer locations, accelerometer type, and amplitude range.

3. The vibration instrumentation was calibrated to determine the amplitude sensitivity and frequency response of the total data system. A frequency sweep was performed on each accelerometer with an electrodynamic shaker. Each accelerometer was mounted back to back with a calibrated reference accelerometer and the charge sensitivity, picocoulomb/g, and frequency response of the test accelerometer determined by comparison with the reference accelerometer. The airborne data recording system was calibrated by means of a charge source. For each channel, the charge source was set to simulate a given acceleration value by reference to the accelerometer charge sensitivity determined by the shaker calibration, and the airborne data system output was recorded. The ground station was calibrated separately from the airborne system, and the two system scale factors were combined to obtain an overall data system scale factor. It is estimated that the accuracy of the total vibration measurement system, both airborne and ground units, is within  $\pm 10$  percent of the true acceleration amplitude.



Table 1. Instrumentation Component Description.

Nomenclature	Manufacturer	Quantity	Model Number
Piezoelectric accelerometer (triaxial)	Endevco	32	2228C
Piezoelectric accelerometer (uniaxial)	Endevco	8	2226C
Line driver	MB Electronics	81	9402216
Amplifier	MB Electronics	12	N400
Switching relays	Potter and Brumfield	24	JDT27DD1
FM rack	Electro Mechanical Research	2	--
FM rack voltage code oscillator (VCO)	Electro Mechanical Research	12	307A-02
FM rack mixing amplifier	Electro Mechanical Research	2	311A-02-1
FM rack reference oscillator	Electro Mechanical Research	2	313A-01
Tape recorder	Genisco Technology Corp.	1	10-286
Time code generator	Electro Mechanical Research	1	CL24D-27.6A
Thermocouple switch (24 channels)	Thermo Electric	1	33113
Thermocouple indicator	Newport Laboratories	1	2600
Thermocouple wire (iron-constantan)	Series J	--	--
Thermal radiometer	Teledyne Geotech	1	TCH-188-01

**FIGURE 1**

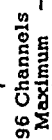


Table 2. Accelerometer Locations.

Location	Location Number	Fuselage Station (in.)	Water Line (in.)	Buttline (in.)	Axis	Full Scale Acceleration Range ( $\pm$ g)	Accelerometer Type <sup>1</sup>
Instrument panel	1	62.0	145.5	20.5L	3	5	2228C
	2	65.0	140.0	17.5L	3	5	2228C
	3	65.0	140.0	6.5L	3	5	2228C
	4	64.0	141.0	Zero	3	5	2228C
	5	65.0	140.0	10.0R	3	5	2228C
	6	62.0	145.5	21.0R	3	5	2228C
	7	67.5	136.0	21.0R	3	5	2228C
Avionics							
CN-998/ASN-43 directional gyro mount	8	56.0	120.0	8.0R	3	5	2228C
CN-998/ASN-43 directional gyro	9	56.0	122.0	8.0R	3	5	2228C
RT-742/ARC-51BX radio mount	10	84.0	101.0	42.5R	3	5	2228C
RT-742/ARC-51BX radio	11	84.0	103.0	42.5R	3	5	2228C
R-1388/ARN-82 radio	12	84.0	88.0	41.5R	3	5	2228C
AFCs amplifier	13	57.5	90.0	Zero	3	5	2228C
AFCs transducer package	14	338.0	182.5	33.0R	3	5	2228C
Pilot							
Seat pad plate	15	90.0	124.0	20.5R	3	5	2228C
Seat structure	16	90.0	129.5	20.5R	3	5	2228C
Right pedal foot rest	17	70.5	121.0	29.0R	Vertical, lateral	5	2228C
Collective grip	18	82.5	140.0	10.0R	Vertical	5	2226C
Cyclic grip	19	77.0	146.0	20.5R	3	5	2228C
Pilot's helmet (SPH-4)	20	--	--	--	3	5	2228C
Bite block	21	--	--	--	3	5	2228C
Main rotor tach generator	22	359.0	202.0	4.5L	3	100	2228C
Power turbine tach generator	23	243.5	214.5	35.5L	3	50	2228C
Gas producer tach generator	24	294.5	230.5	11.0L	3	50	2228C
Transmission mounts							
Forward	25	319.0	166.0	Zero	3	50	2228C
Aft	26	319.0	167.5	Zero	3	50	2228C
Right	27	339.5	167.0	20.5R	3	50	2228C
Left	28	339.5	167.0	20.5L	3	50	2228C
Upper main transmission	29	339.5	235.0	4.0R	3	50	2228C
Tail rotor shaft 90-degree gearbox	30	872.0	256.0	5.0L	3	50	2228C
Tail rotor shaft 45-degree gearbox	31	802.0	187.0	Zero	3	100	2228C
Tail rotor shaft hanger bearing							
No. 1	32	435.5	210.0	4.0R	Vertical, lateral	50	2228C
No. 2	33	511.0	205.0	4.0R	Vertical, lateral	50	2228C
No. 3	34	589.0	200.0	4.0R	Vertical, lateral	50	2228C
No. 4	35	649.0	194.5	4.0R	Vertical, lateral	50	2228C
No. 5	36	729.0	187.5	4.0R	Vertical, lateral	50	2228C

Hydraulic pump, 1st stage	37	357.0	227.0	3.5R	3	50	2228C
Hydraulic line, hoist power	38	327.5	203.1	43.0R	3	50	2228C
Hydraulic manifold, 2nd stage	39	330.0	206.5	43.0R	3	5	2228C
Hydraulic pump, utility	40	362.5	219.0	11.0R	3	300	2228C
Hydraulic sled	41	435.5	203.5	8.0L	3	50	2228C
Oil cooler support	42	368.5	228.0	8.0R	3	167	2228C
Oil cooler idler	43	363.0	232.5	Zero	3	167	2228C
APP fuel pressure switch	44	384.0	219.0	6.0R	3	17	2228C
Engine fuel pressure switch	45	267.0	196.0	13.0L	3	5	2228C
Brake cylinder, rudder pedal	46	67.5	113.0	29.0R	3	5	2228C
Rotor brake support	47	338.0	219.5	40.5L	3	50	2228C
Compass transmitter support	48	619.0	162.0	Zero	3	5	2228C
Pilot cooling fan	49	56.5	123.0	30.0R	3	5	2228C
Horizontal stabilizer tip	50	847.0	267.0	106.0R	3	17	2228C
Anticollision light, nose	51	68.5	77.0	Zero	3	5	2228C
Primary servo actuator No. 1	52	327.5	237.0	8.0R	3	50	2228C
No. 2	53	347.5	237.0	8.0R	3	50	2228C
AFCS servo	54	112.0	141.5	30.0R	3	5	2228C
Hydraulic manifold, 1st stage	55	409.5	217.8	27.0L	3	50	2228C
ADF antenna mount	56	609.5	205.5	Zero	3	5	2228C
APP clutch	57	385.0	209.0	9.5R	3	300	2228C
APP mount	58	381.5	201.0	9.5R	3	50	2228C
Engine							
Torque tube top	60	325.5	221.2	27.0L	Vertical	50	2226C
Torque tube side	60	325.5	213.8	24.0L	Lateral	50	2226C
Outboard absorber	61	295.6	211.0	41.0L	Vertical, lateral	50	2228C
Inboard absorber	62	295.6	211.0	11.0L	Vertical, lateral	50	2228C
Outboard forward mount	63	248.0	215.0	34.5L	Vertical, lateral	50	2228C
Inboard forward mount	64	248.0	215.0	16.5L	Vertical, lateral	50	2228C
Engine							
Power turbine top	65	227.0	226.0	27.0L	Vertical	50	2226C
Power turbine side	66	227.0	213.8	23.5L	Lateral	50	2226C
Rear frame top	67	251.0	228.0	27.0L	Vertical	50	2226C
Rear frame side	68	251.0	213.8	15.0L	Lateral	50	2226C
Front frame top	69	223.5	227.0	27.0L	Vertical	50	2226C
Front frame side	70	223.5	213.8	23.0L	Lateral	50	2226C

<sup>1</sup>2228C accelerometers are triaxial, 2226C accelerometers are uniaxial accelerometers.

#### TEMPERATURE INSTRUMENTATION

4. Temperature data were recorded by mounting thermocouples at 20 locations throughout the helicopter. The temperatures were displayed on one temperature indicator which was switched to the desired thermocouple. Table 3 lists the locations of the thermocouples and the temperature measurement equipment is described in table 1. Photographs of the thermocouple locations are presented in appendix E. Solar radiation was recorded on the ground with a calibrated radiometer. Outside air temperature (OAT) was recorded with a laboratory thermometer for static temperature measurements and with the ship's OAT indicator for in-flight temperature measurement.

#### FLIGHT CONDITION PARAMETERS

5. The parameters listed in table 4 were hand-recorded from the ship's standard instruments to determine the flight condition. An estimate of the readability of each instrument is also given in table 4.

Table 3: Thermocouple Locations.

Location	Location Number	Fuselage Station (in.)	Water Line (in.)	Buttline (in.)
Forward avionics	1	62.5	95.0	4.5R
Instrument panel back	2	62.0	140.5	Zero
Forward cabin	3	103.8	180.5	Zero
Aft cabin	4	138.6	109.0	39.5L
Transmission avionics	5	338.0	185.5	38.0R
Main rotor tach generator	6	359.0	202.0	4.5L
Gas producer tach generator	7	294.5	230.5	11.0L
Power turbine tach generator	8	243.5	214.5	35.5L
Hanger bearing No. 1	9	435.5	210.0	Zero
Hanger bearing No. 2	10	511.0	205.0	Zero
Hanger bearing No. 3	11	589.0	200.0	Zero
Hanger bearing No. 4	12	649.0	194.5	Zero
Hanger bearing No. 5	13	729.0	197.5	Zero
90-degree gearbox	14	872.0	256.0	5.0L
45-degree gearbox	15	802.0	187.0	Zero
Hydraulic sled	16	424.0	212.0	21.5L
Hoist bay	17	324.0	194.5	Zero
Main transmission	18, 19	339.5	167.0	20.5R, L
APP area	20	384.0	219.0	6.0R

Table 4. Flight Condition Parameters.

Parameter	Range of Interest	Readability
Airspeed	20 to 105 knots	$\pm 1$ knot
Altitude	Zero to 10,000 feet	$\pm 4$ feet
Outside air temperature	Zero to 30°C	$\pm 0.4^{\circ}\text{C}$
Main rotor speed	95 to 105 percent	$\pm 1$ percent
Gas producer speed	37 to 104.2 percent	$\pm 0.2$ percent
Fuel quantity	Zero to 8817 pounds	$\pm 20$ pounds

## APPENDIX E. INSTRUMENTATION PHOTOGRAPHS

### Index

<u>Photograph</u>	<u>Photograph Number</u>
Accelerometer Locations 1, 2, and 3	1
Accelerometer Locations 4, 5, 6, and 7	2
Accelerometer Locations 8 and 9	3
Accelerometer Locations 10 and 11	4
Accelerometer Location 12	5
Accelerometer Location 13	6
Accelerometer Location 14	7
Accelerometer Location 15	8
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Thermocouple Location 16	58
Thermocouple Location 17	59
Thermocouple Locations 18 and 19	60
Thermocouple Location 20	27
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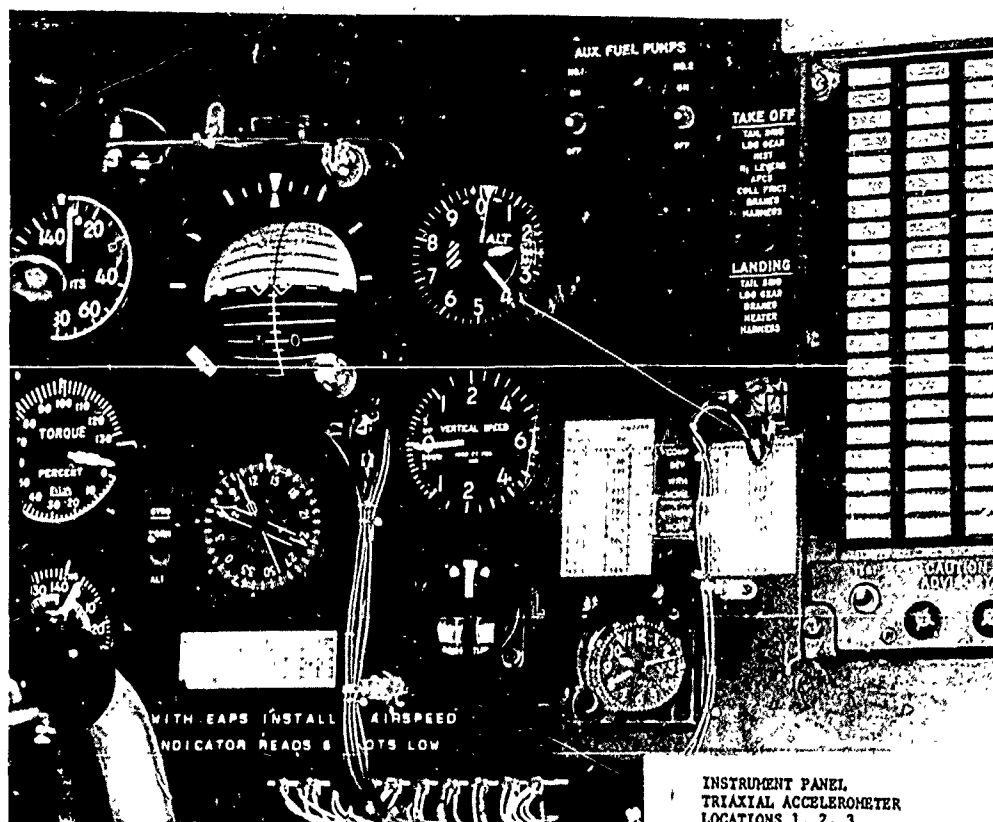


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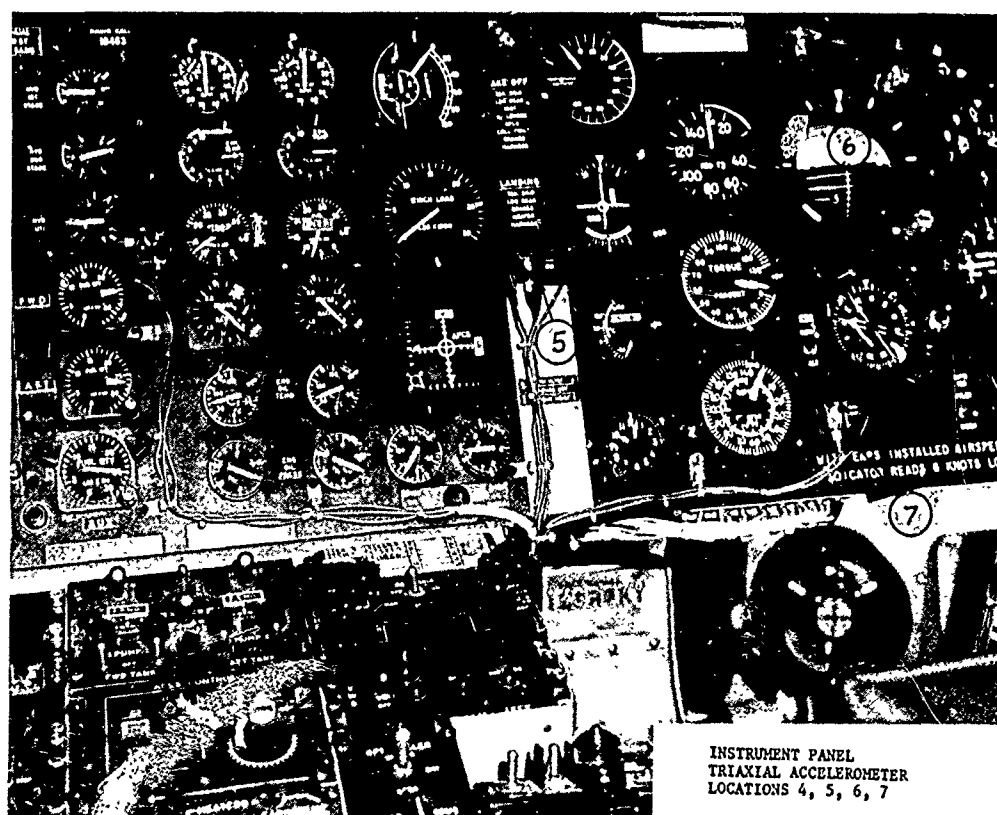
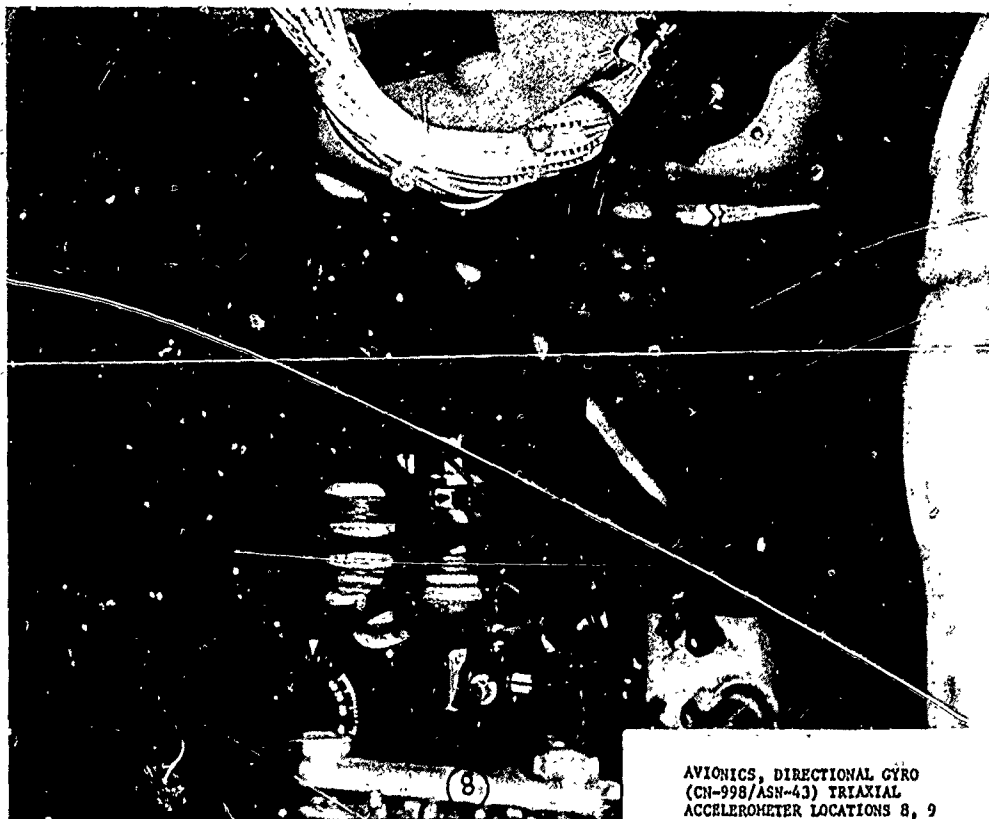
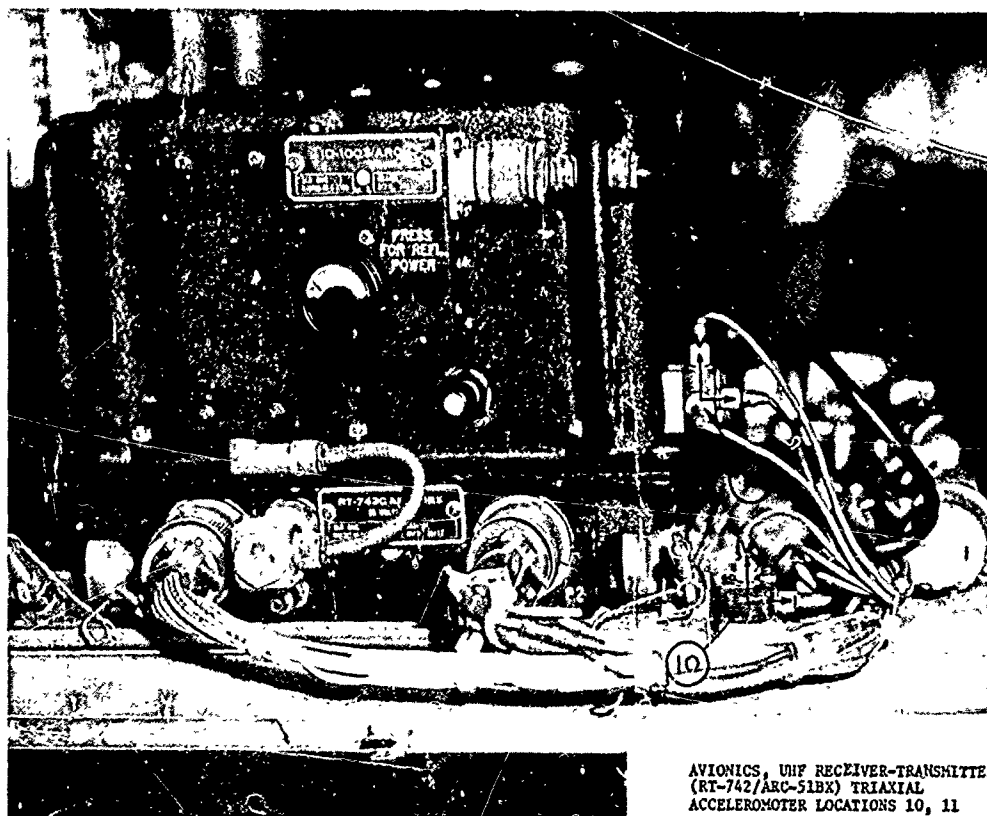


Photo 2.



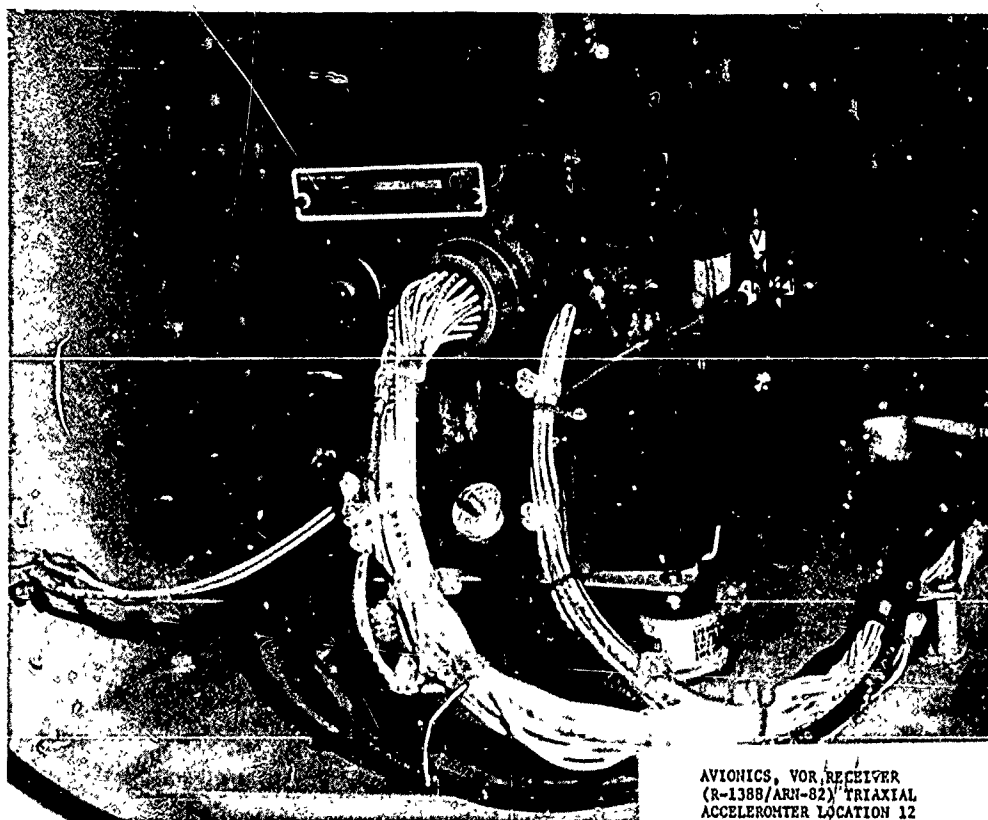
AVIONICS, DIRECTIONAL GYRO  
(CN-998/ASN-43) TRIAXIAL  
ACCELEROMETER LOCATIONS 8, 9

Photo 3.



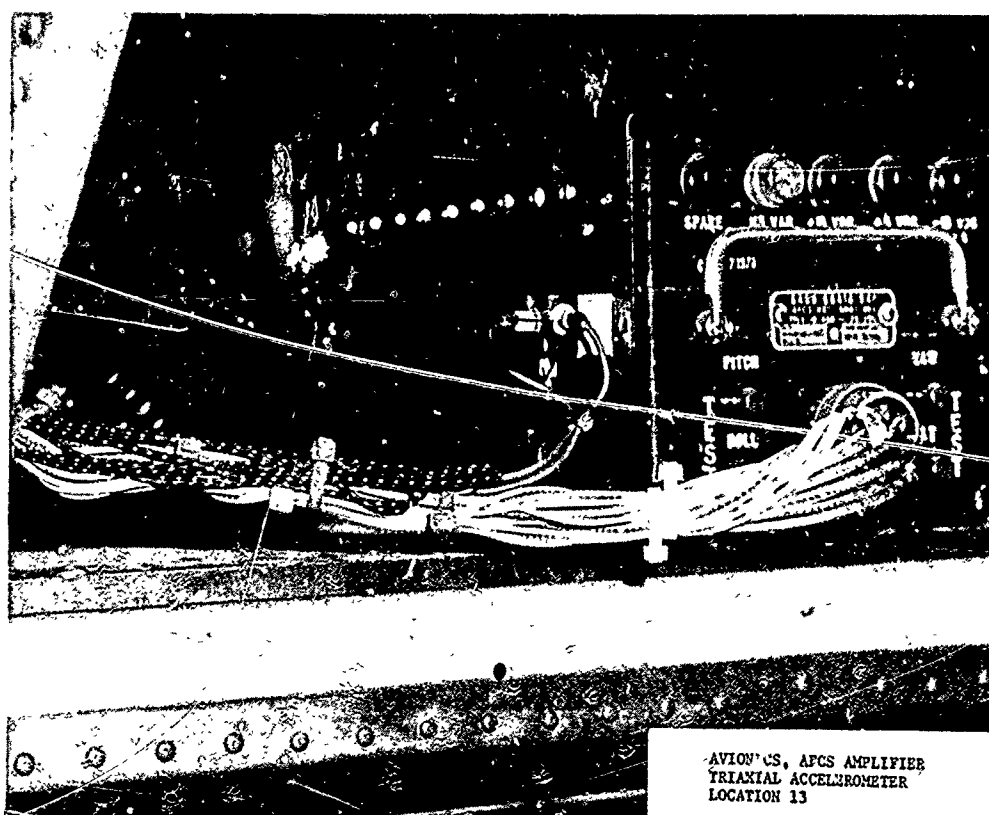
AVIONICS, UHF RECEIVER-TRANSMITTER  
(RT-742/ARC-51BX) TRIAXIAL  
ACCELEROMETER LOCATIONS 10, 11

Photo 4.



AVIONICS, VOR RECEIVER  
(R-1388/ARN-82) TRIAXIAL  
ACCELEROMETER LOCATION 12

Photo 5.



AVIONICS, AFCS AMPLIFIER  
TRIAXIAL ACCELEROMETER  
LOCATION 13

Photo 6.

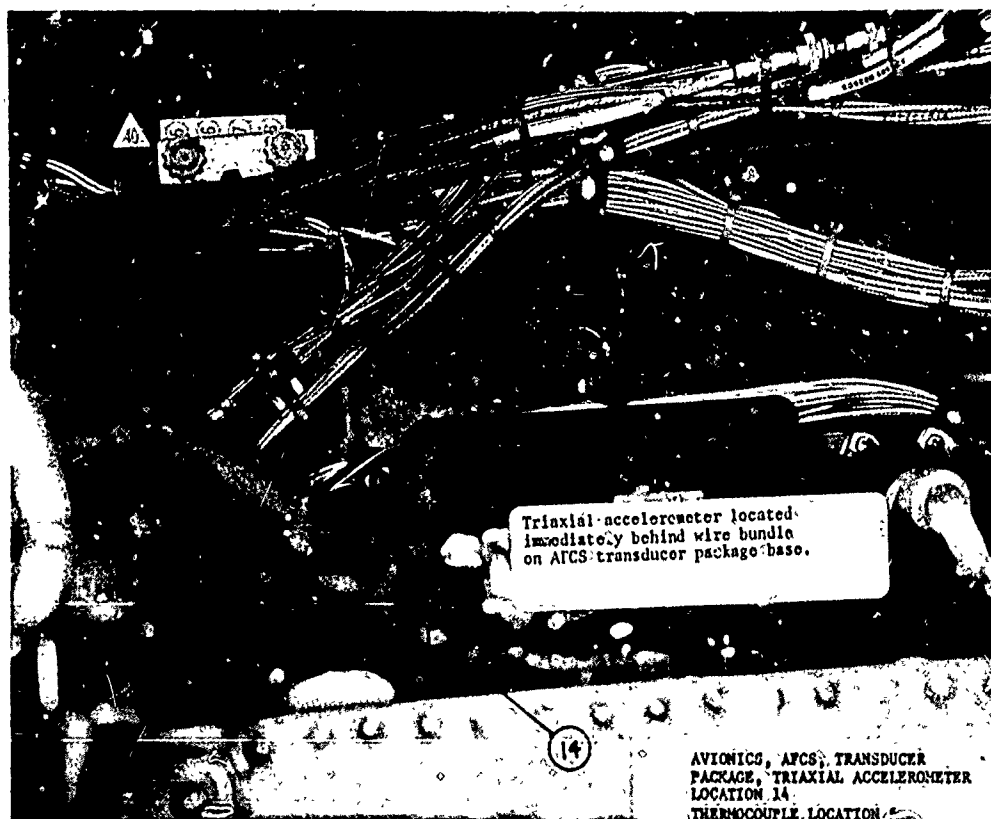


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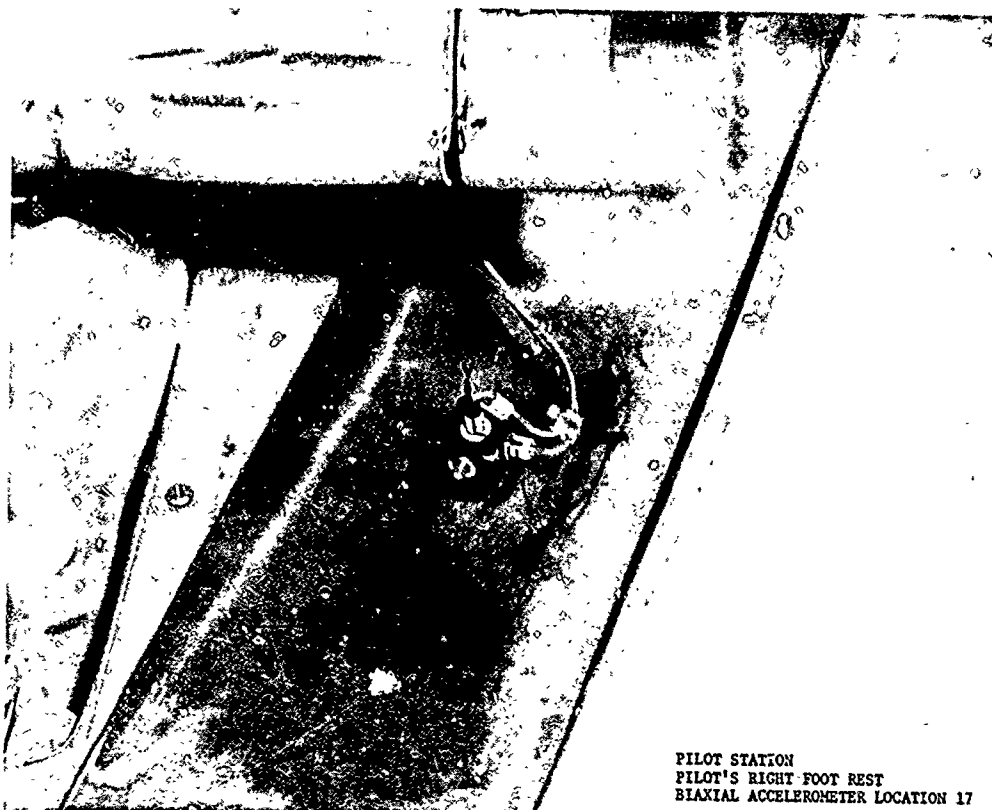


Photo 8.



PILOT STATION  
SEAT STRUCTURE, BOTTOM OF SEAT PAN  
TRIAxIAL ACCELEROMETER  
LOCATION 16

Photo 9.



PILOT STATION  
PILOT'S RIGHT FOOT REST  
BIAXIAL ACCELEROMETER LOCATION 17

Photo 10.

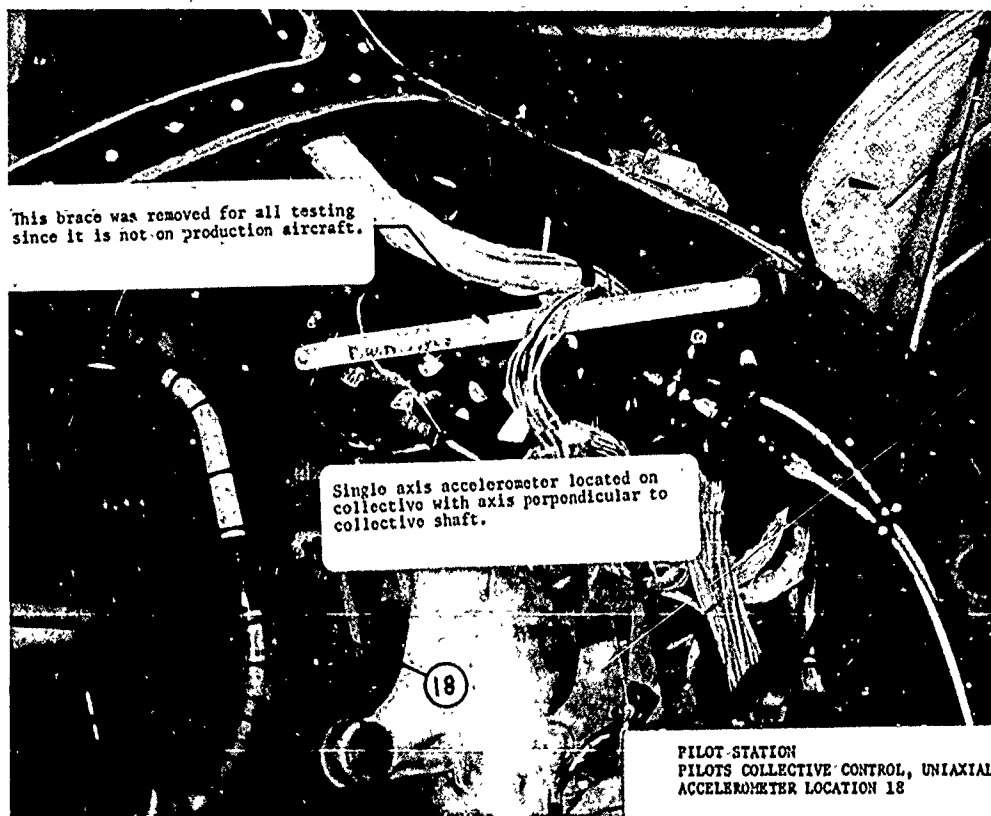


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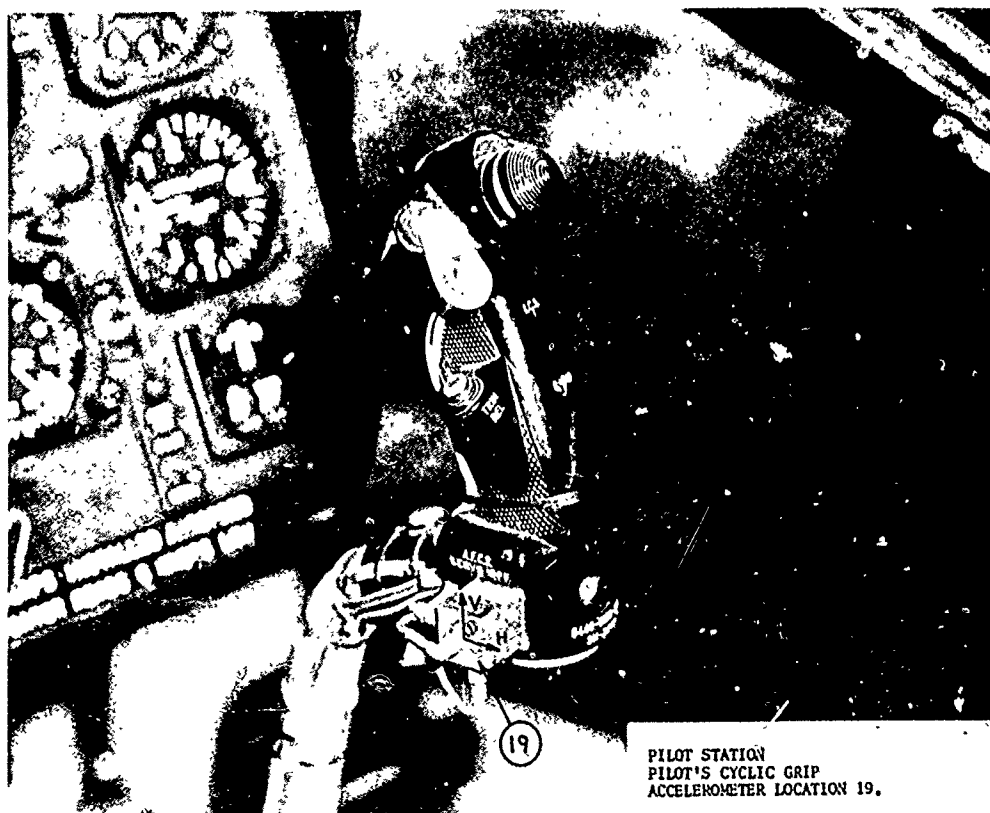


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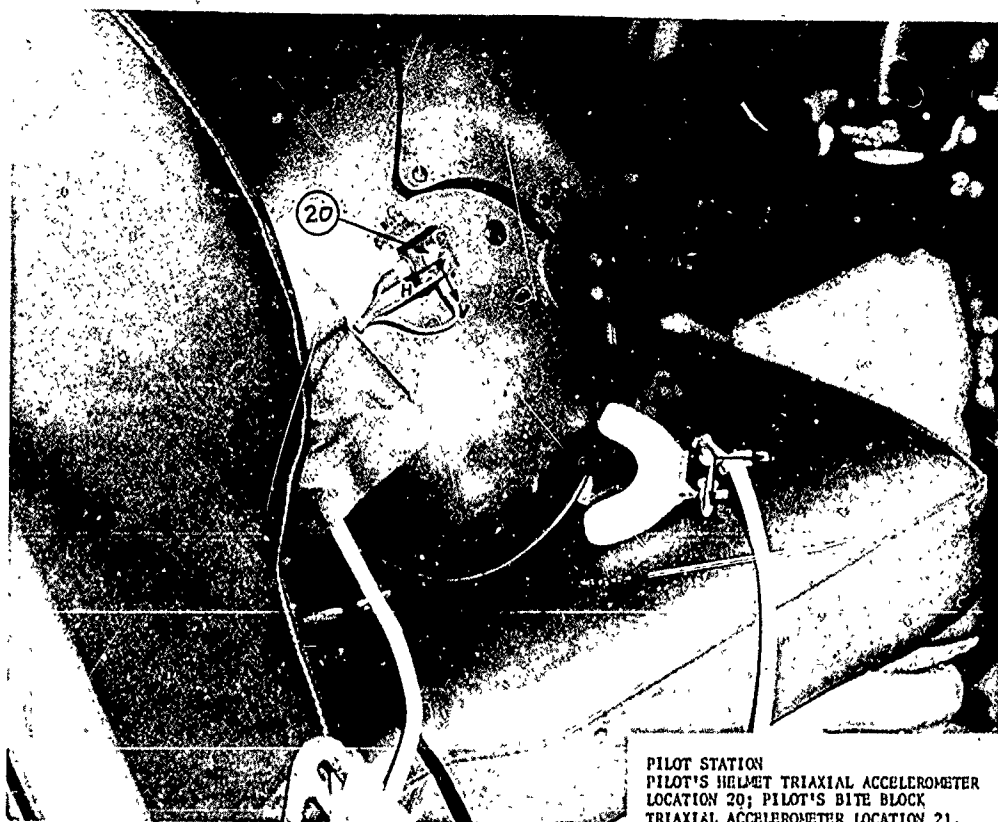
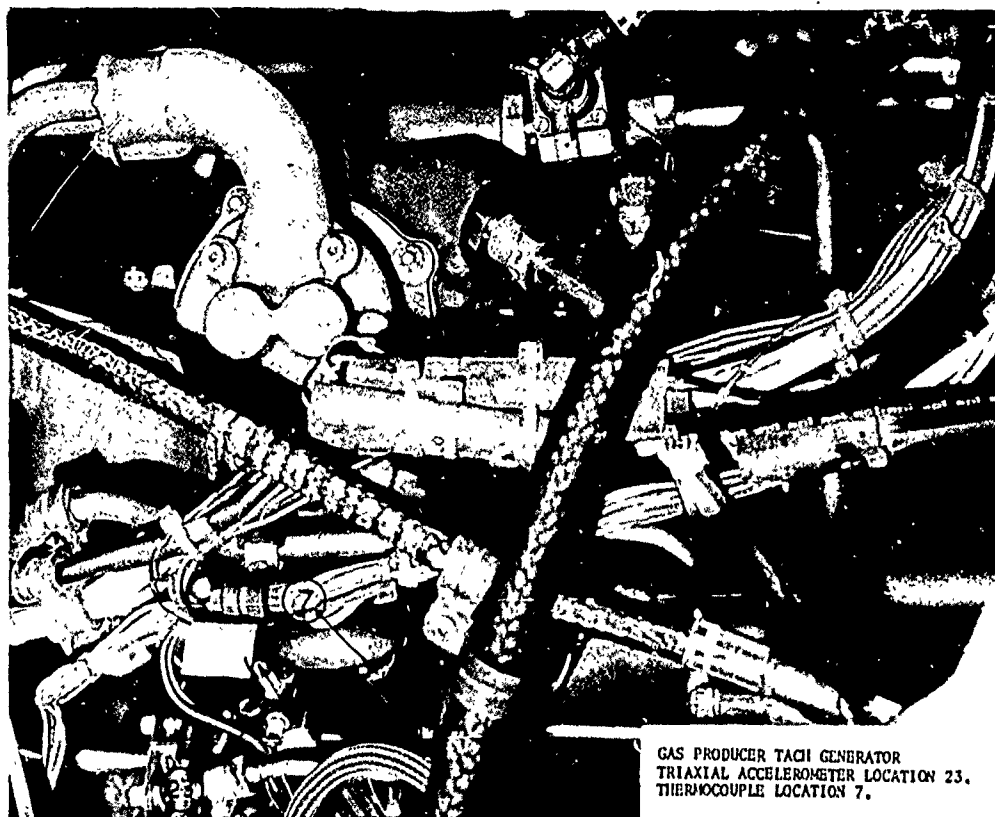


Photo 13



Photo 14.



GAS PRODUCER TACHI GENERATOR  
 TRIAXIAL ACCELEROMETER LOCATION 23.  
 THERMOCOUPLE LOCATION 7.

Photo 15.



POWER TURBINE TACHI GENERATOR  
 TRIAXIAL ACCELEROMETER  
 LOCATION 24.  
 THERMOCOUPLE LOCATION 8.

Photo 16.

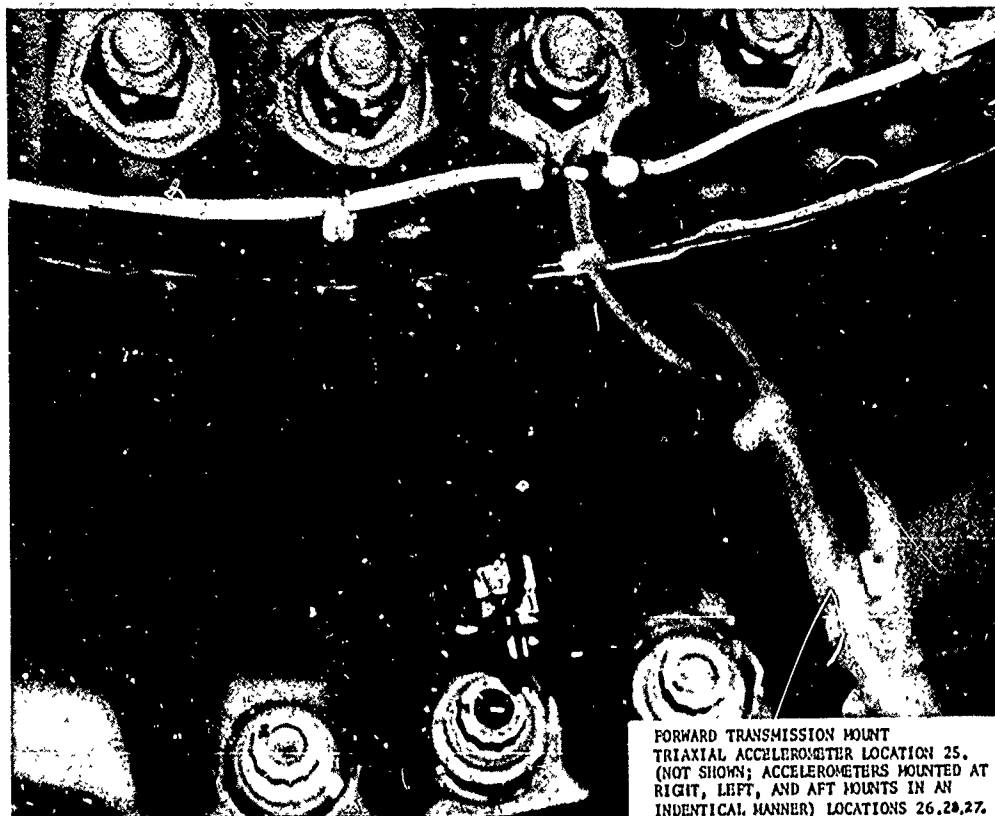


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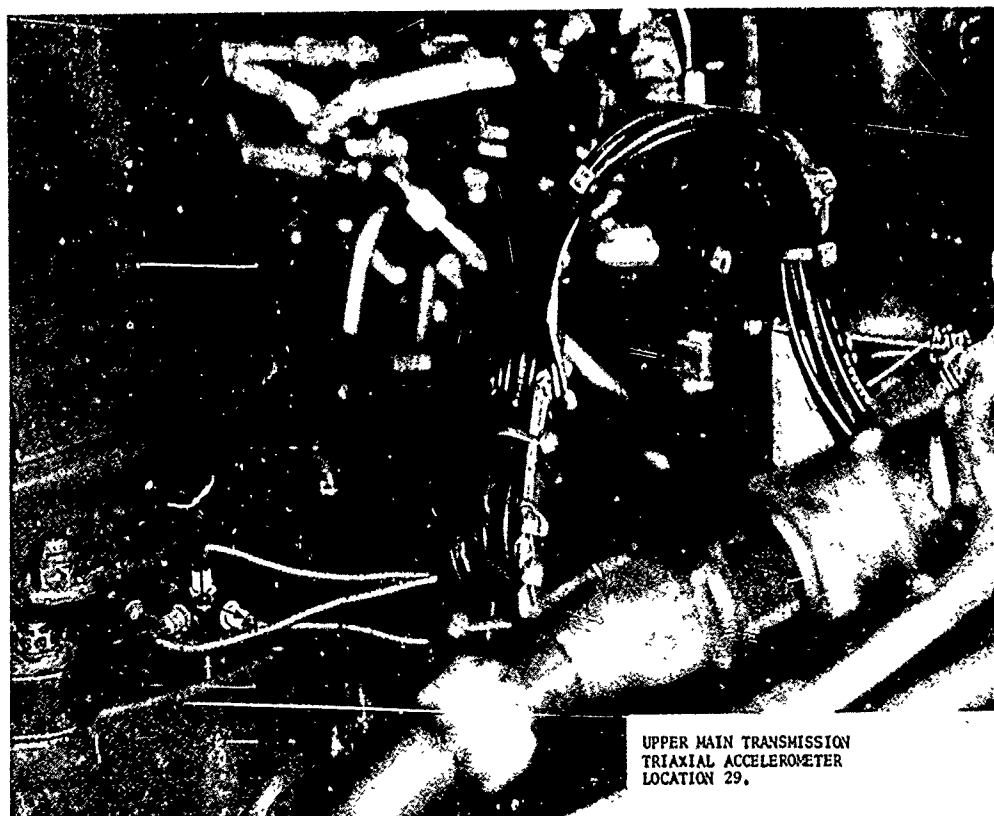
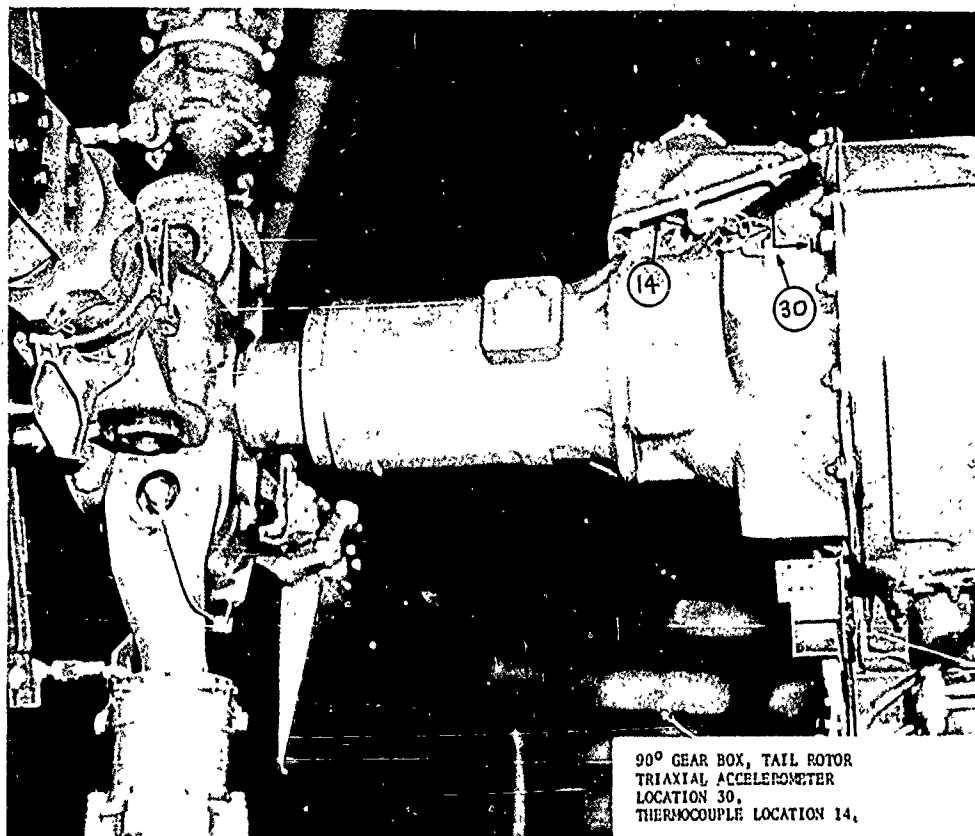
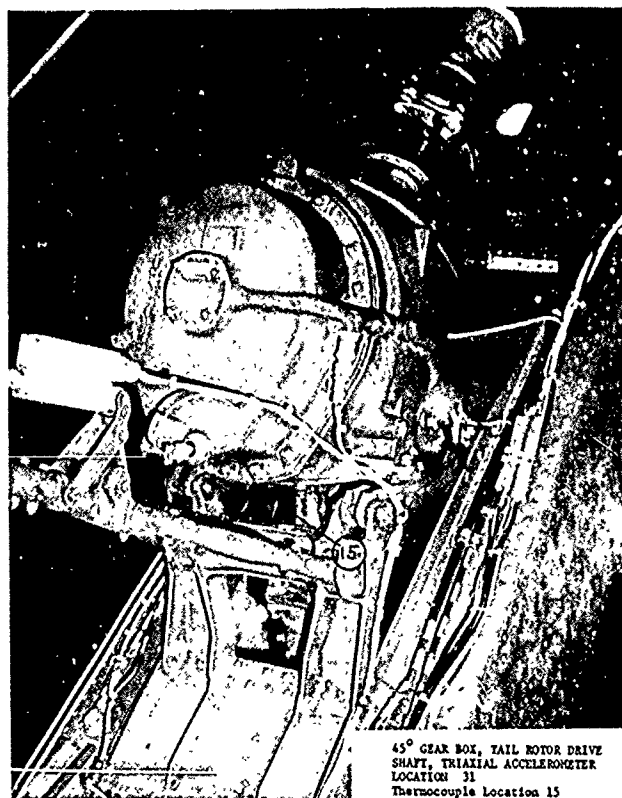


Photo 18.



90° GEAR BOX, TAIL ROTOR  
 TRIAXIAL ACCELEROMETER  
 LOCATION 30,  
 THERMOCOUPLE LOCATION 14,

Photo 19.



45° GEAR BOX, TAIL ROTOR DRIVE  
 SHAFT, TRIAXIAL ACCELEROMETER  
 LOCATION 31  
 Thermocouple Location 15

Photo 20.

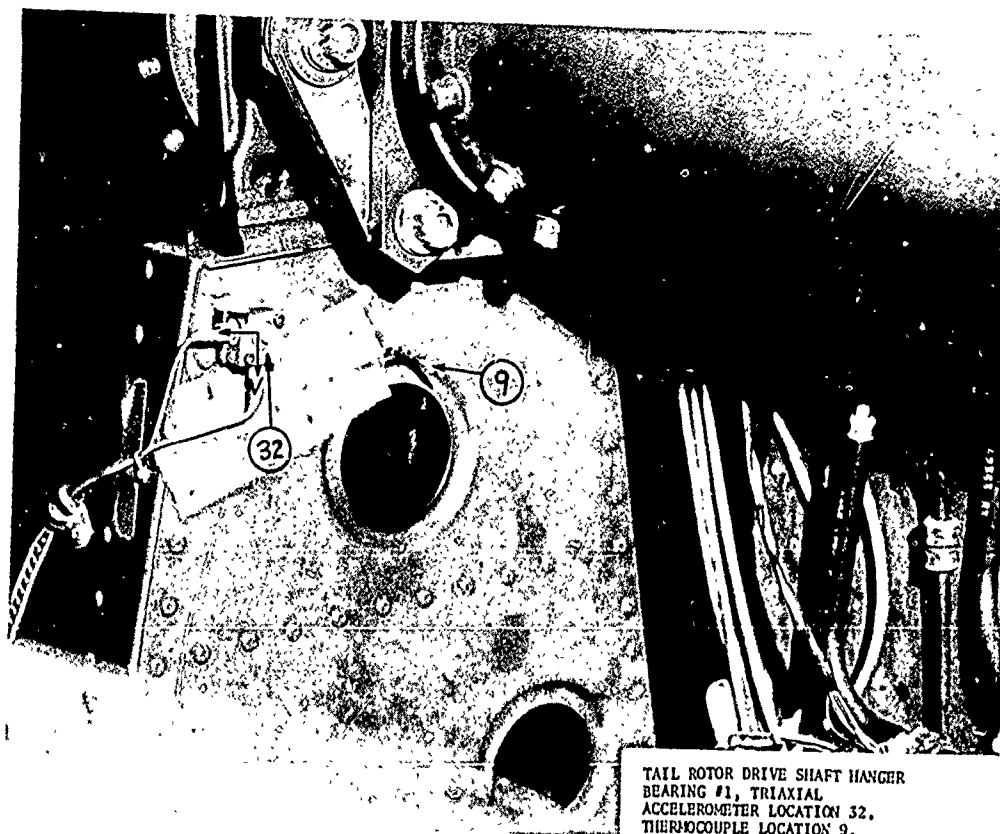


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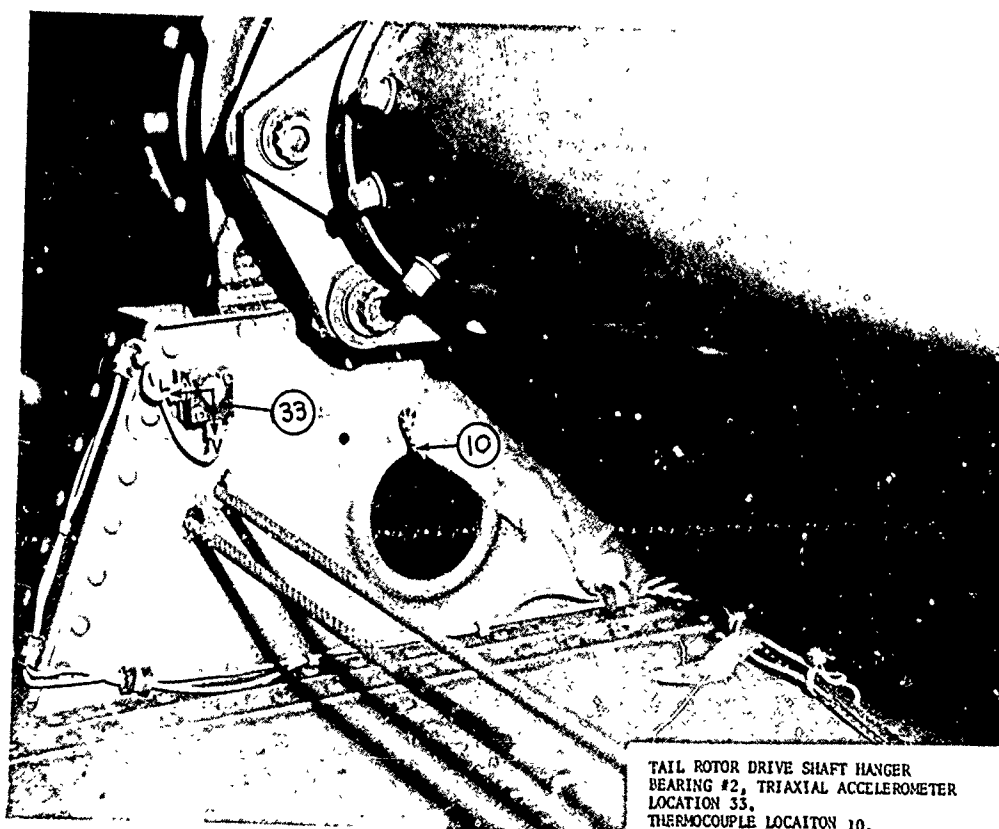


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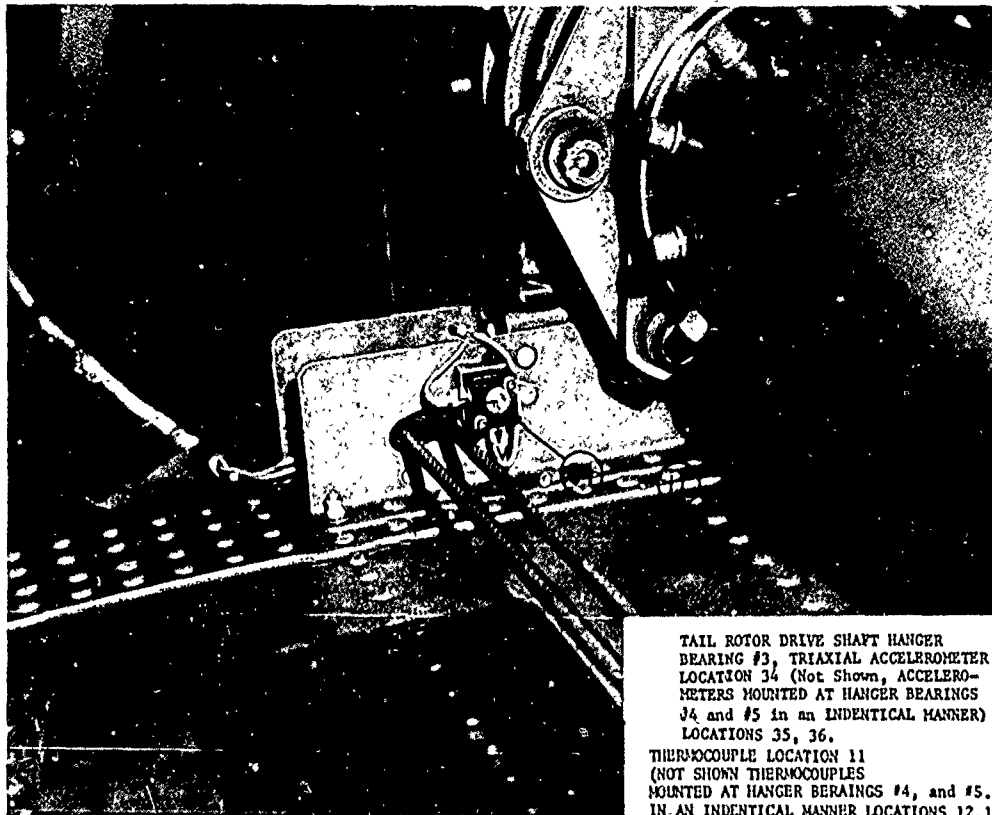


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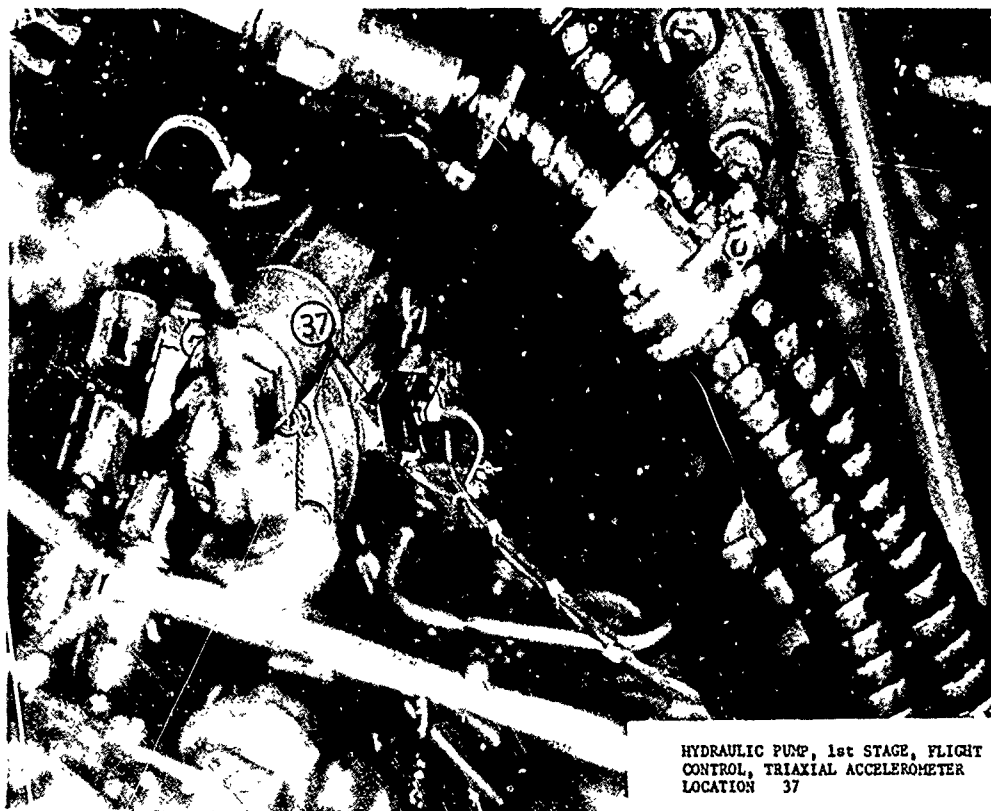
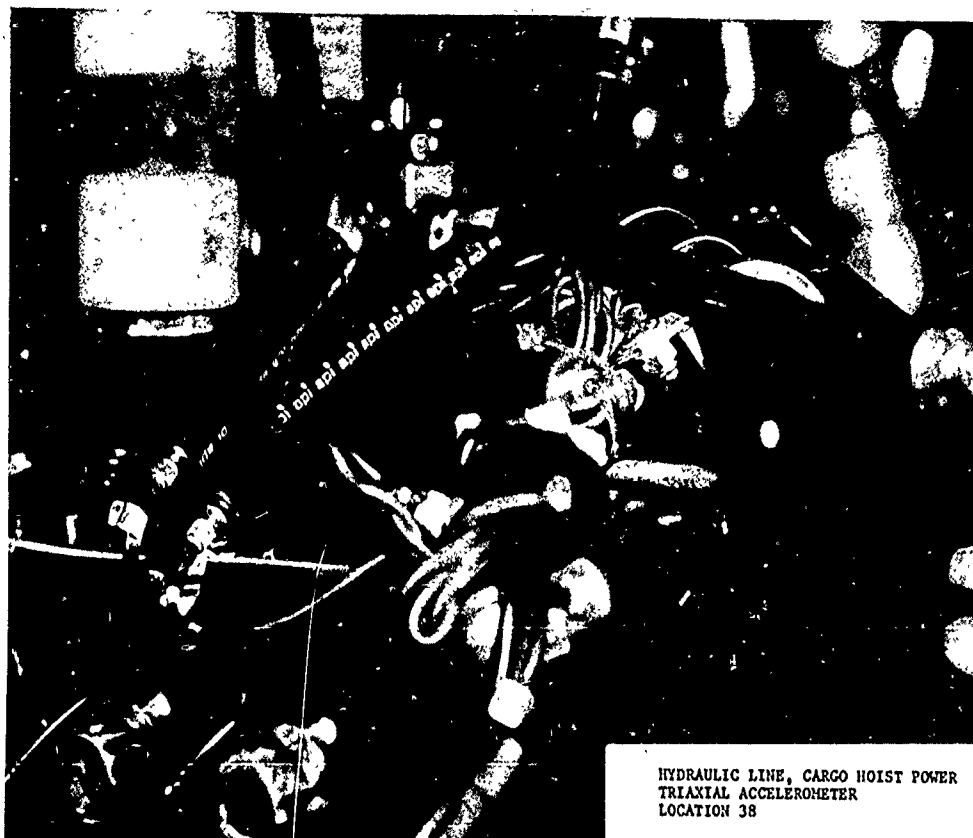
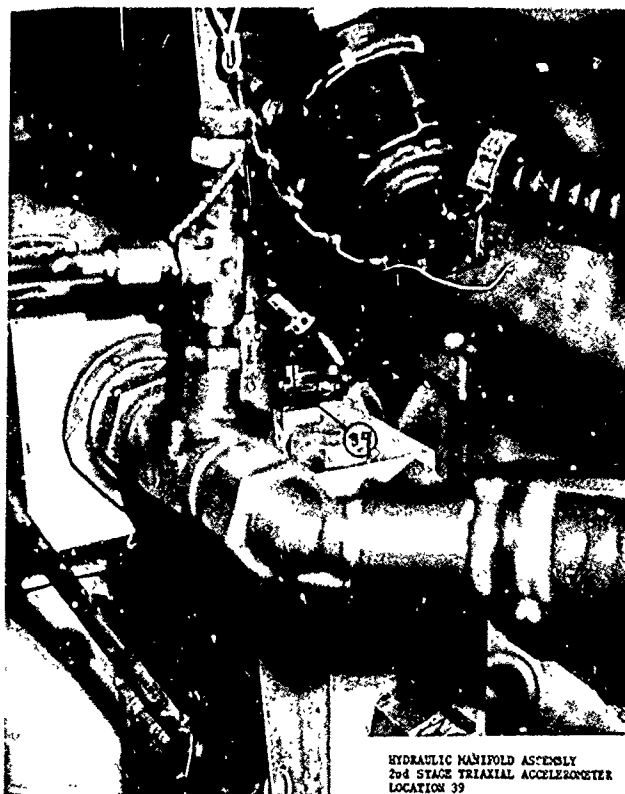


Photo 24.



HYDRAULIC LINE, CARGO HOIST POWER  
 TRIAXIAL ACCELEROMETER  
 LOCATION 38

Photo 25.



HYDRAULIC MANIFOLD ASSEMBLY  
 2nd STAGE TRIAXIAL ACCELEROMETER  
 LOCATION 39

Photo 26.

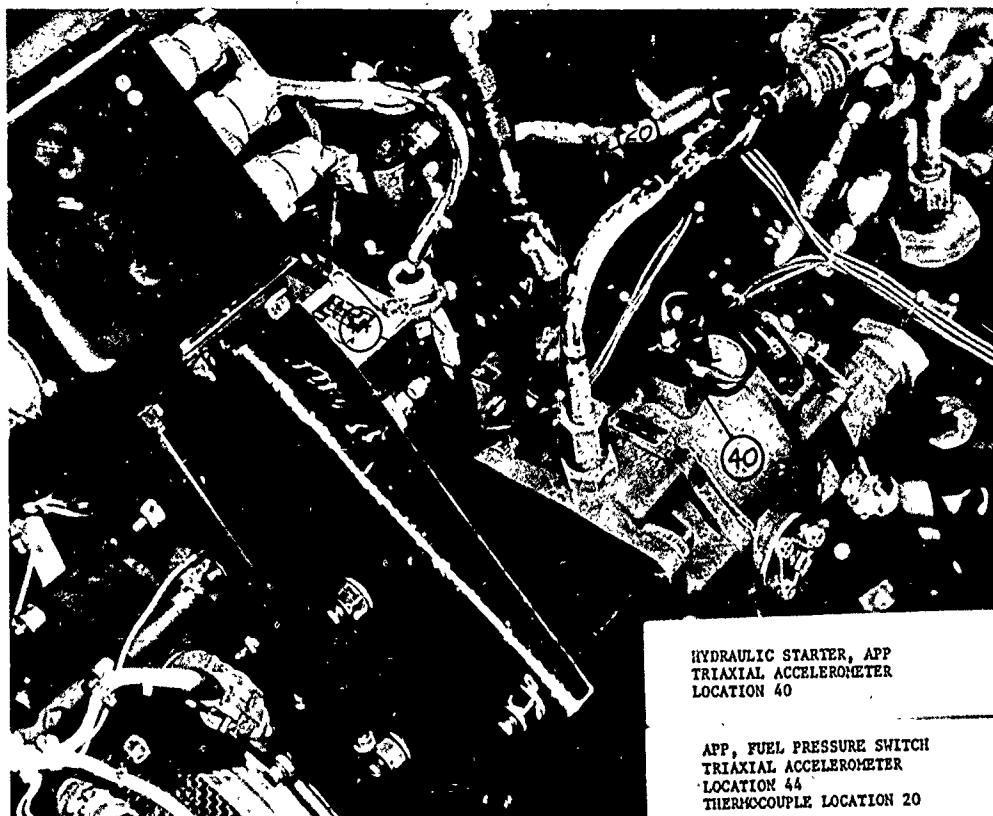


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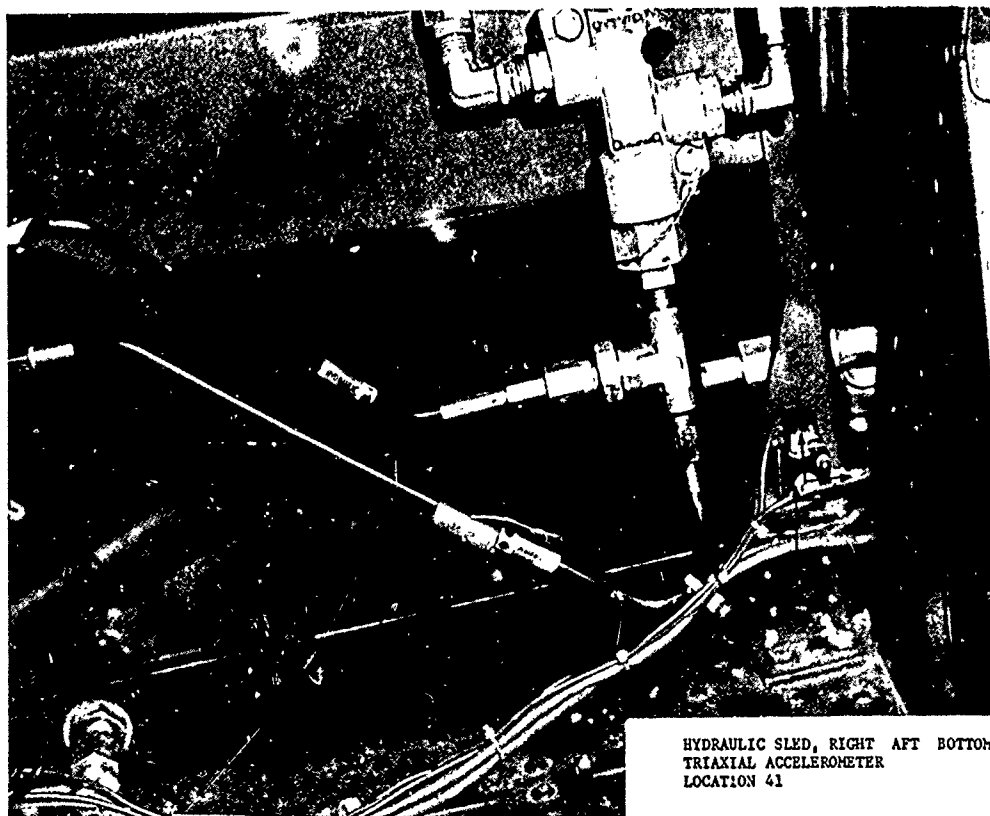
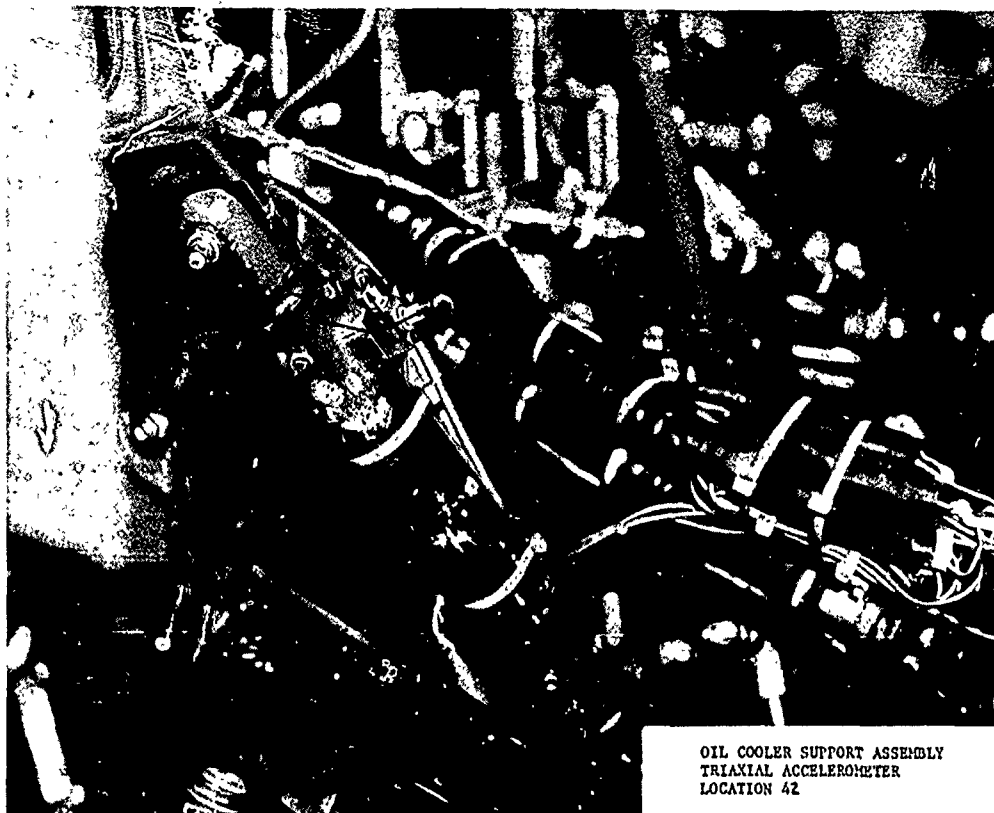


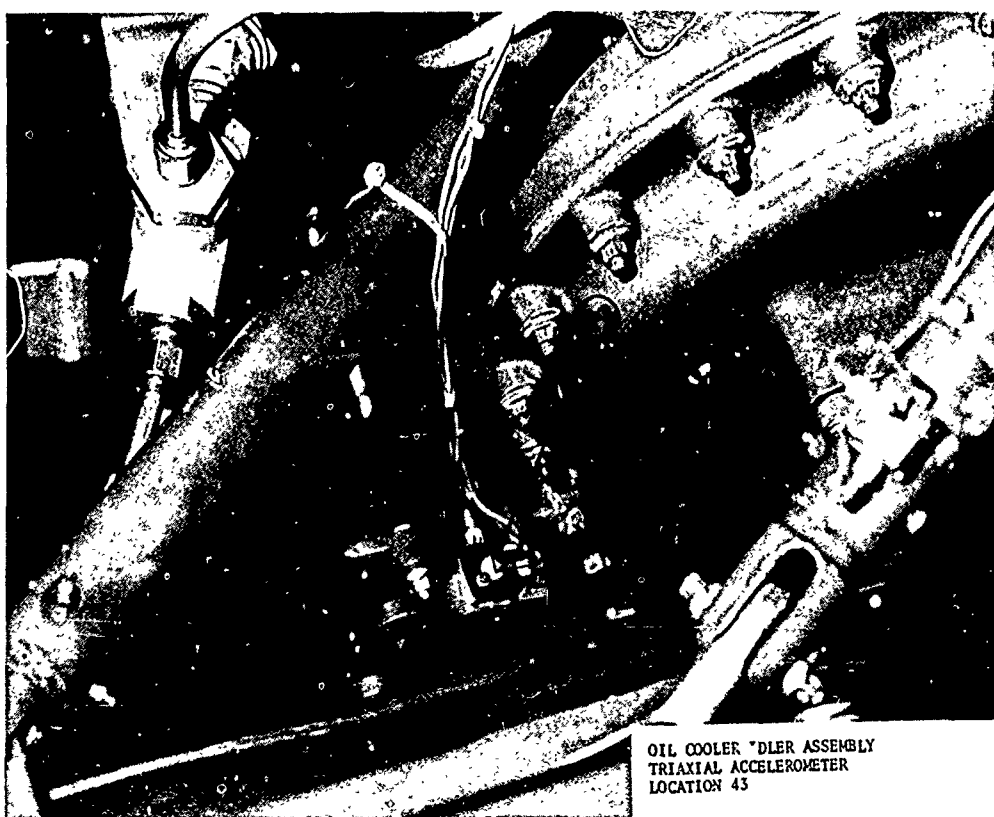
Photo 28.





OIL COOLER SUPPORT ASSEMBLY  
 TRIAXIAL ACCELEROMETER  
 LOCATION 42

Photo 29.



OIL COOLER \*DLER ASSEMBLY  
 TRIAXIAL ACCELEROMETER  
 LOCATION 43

Photo 30.



Photo 31.

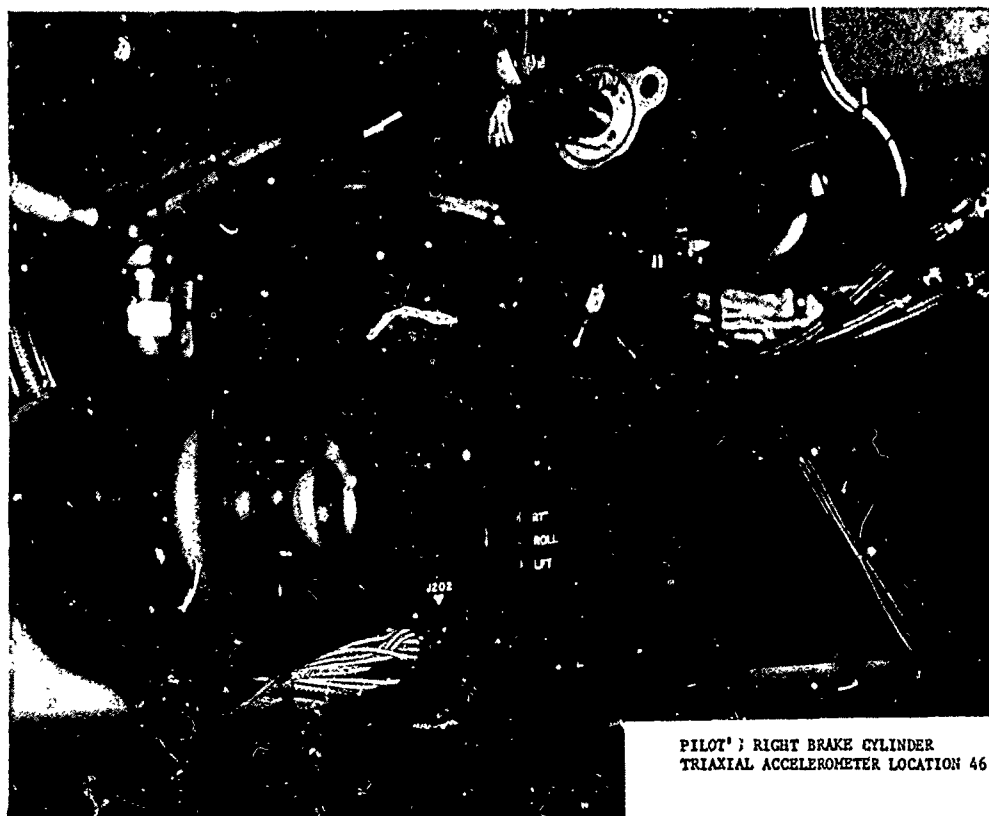


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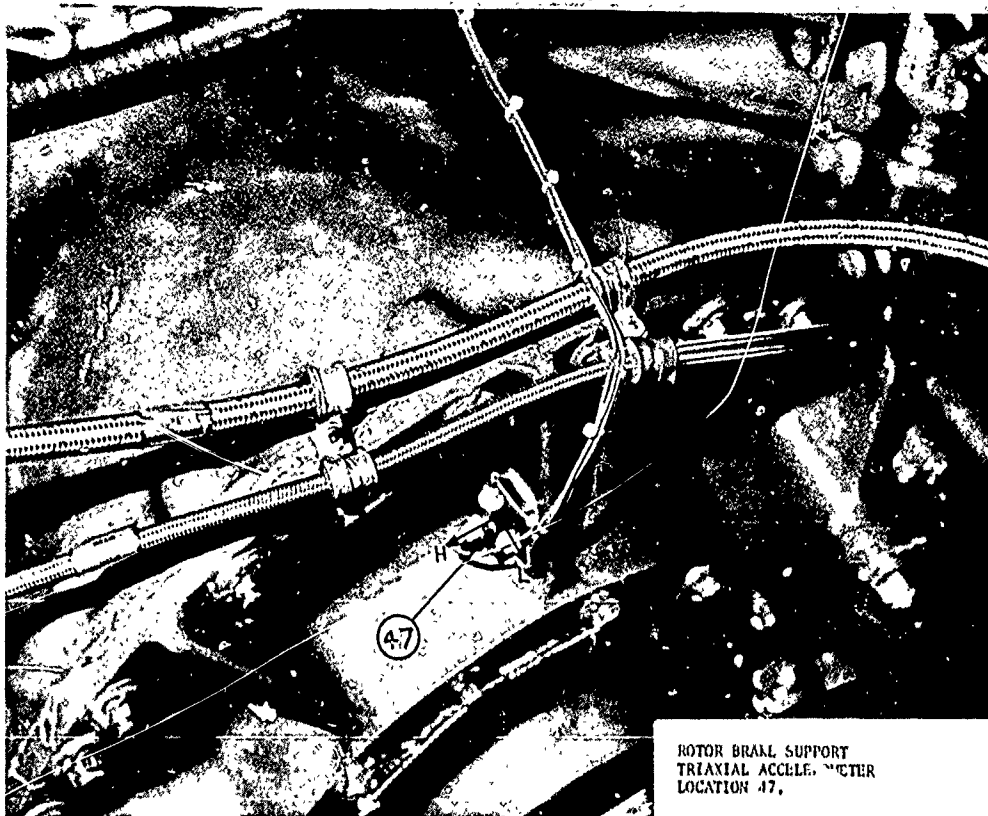


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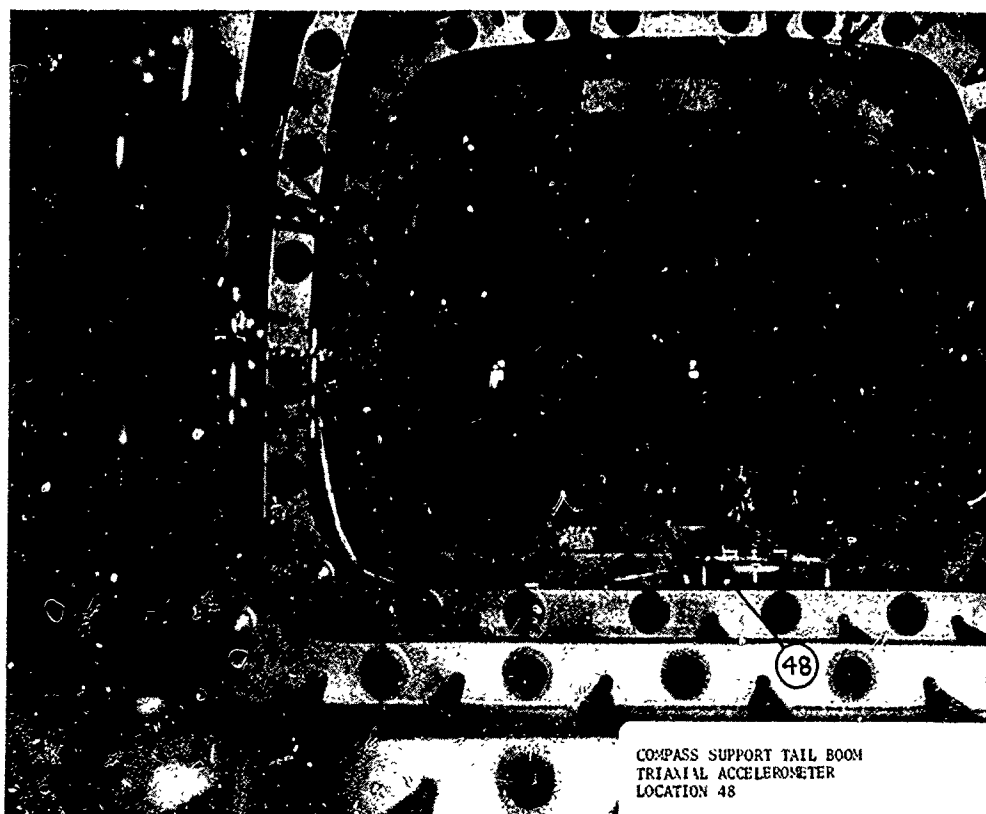


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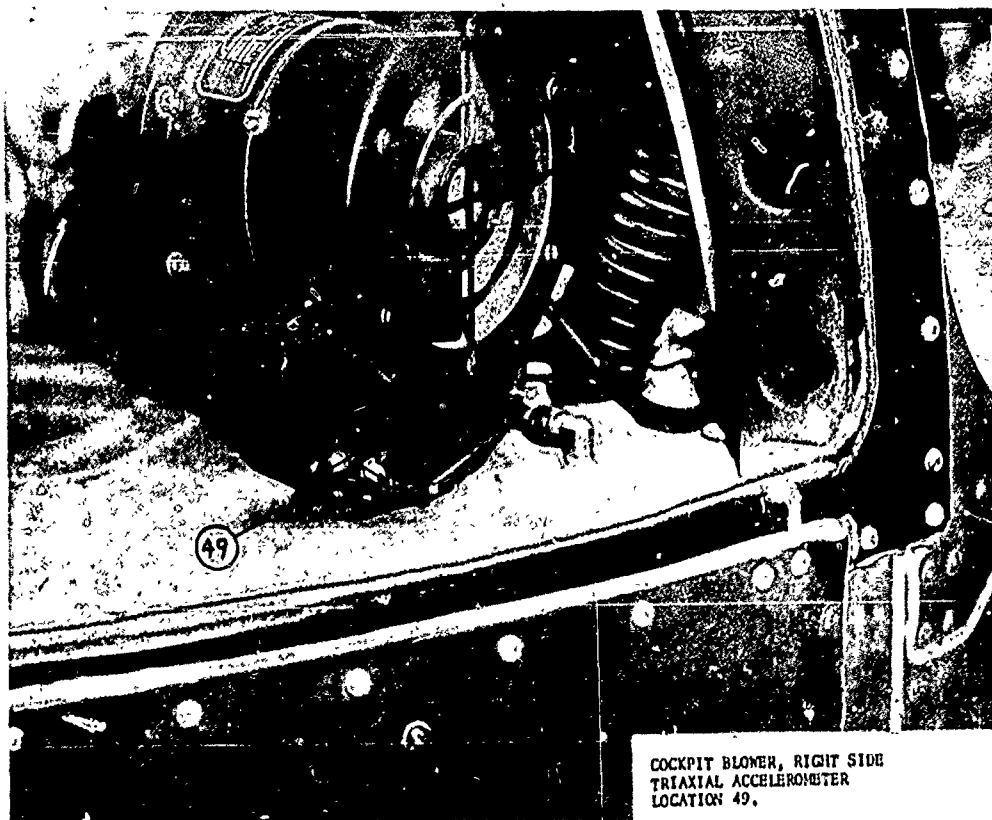


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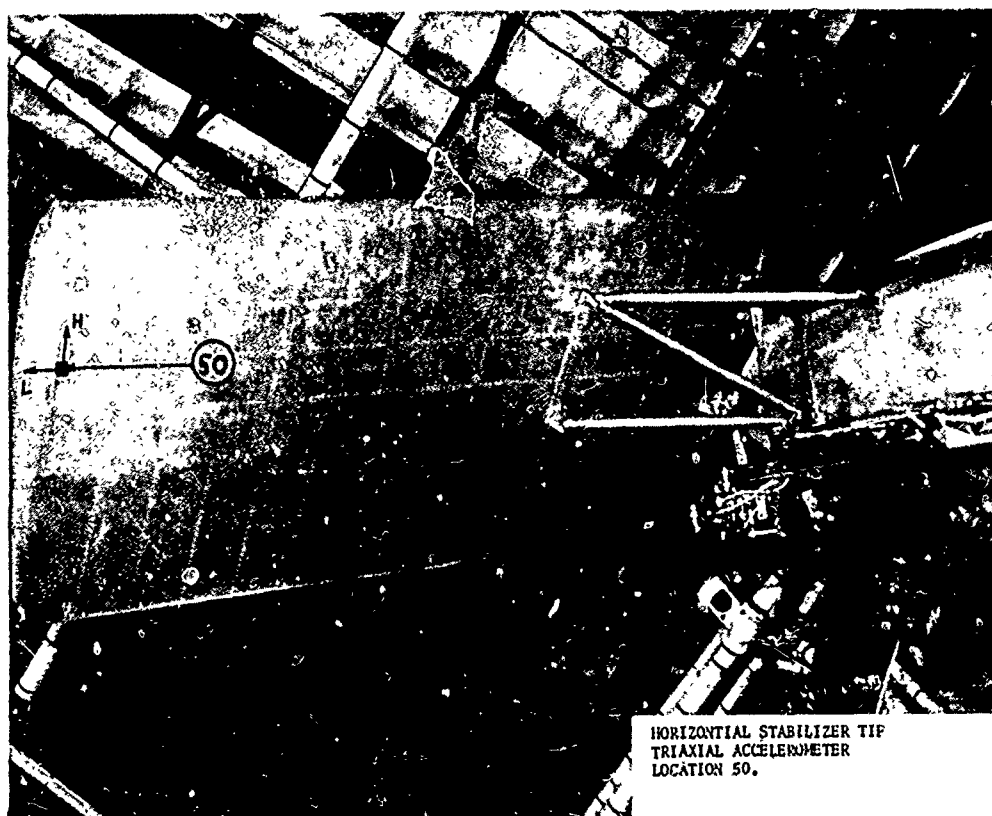


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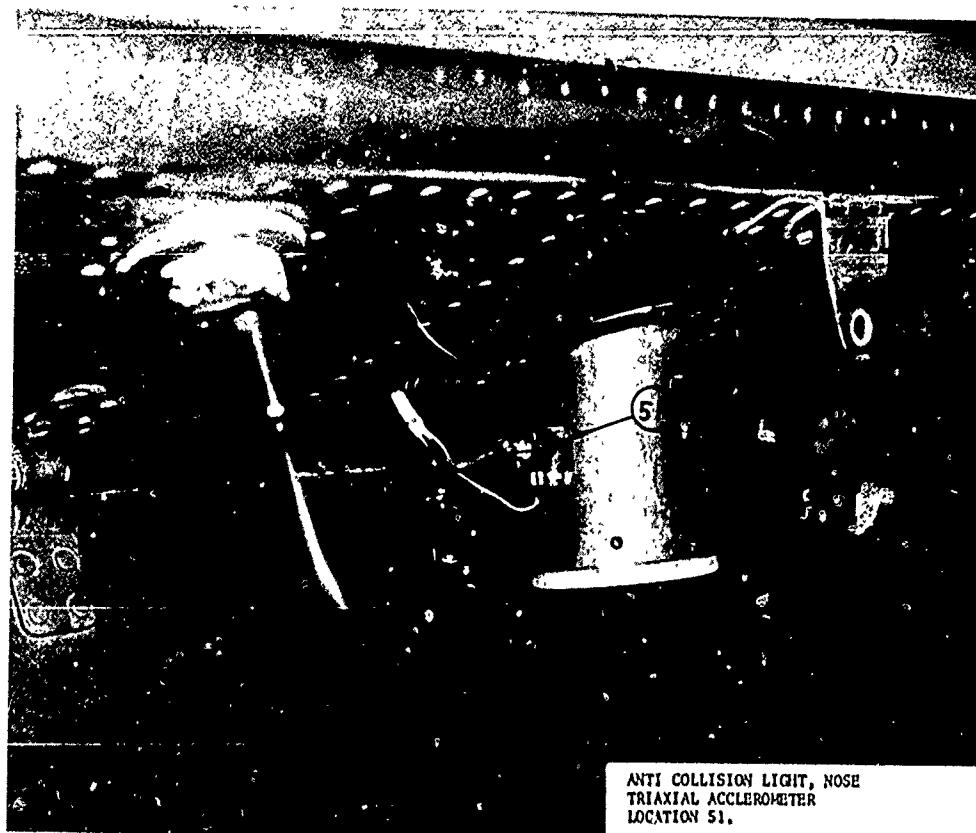


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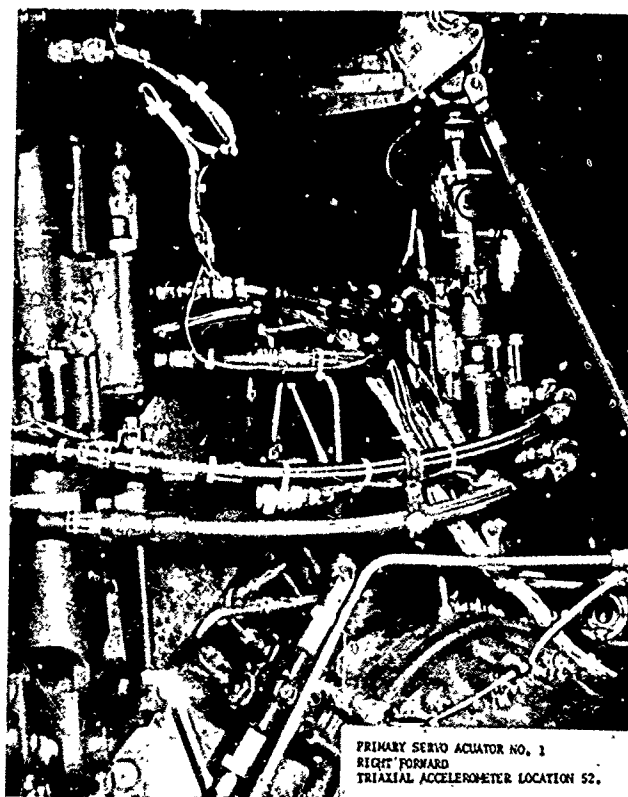


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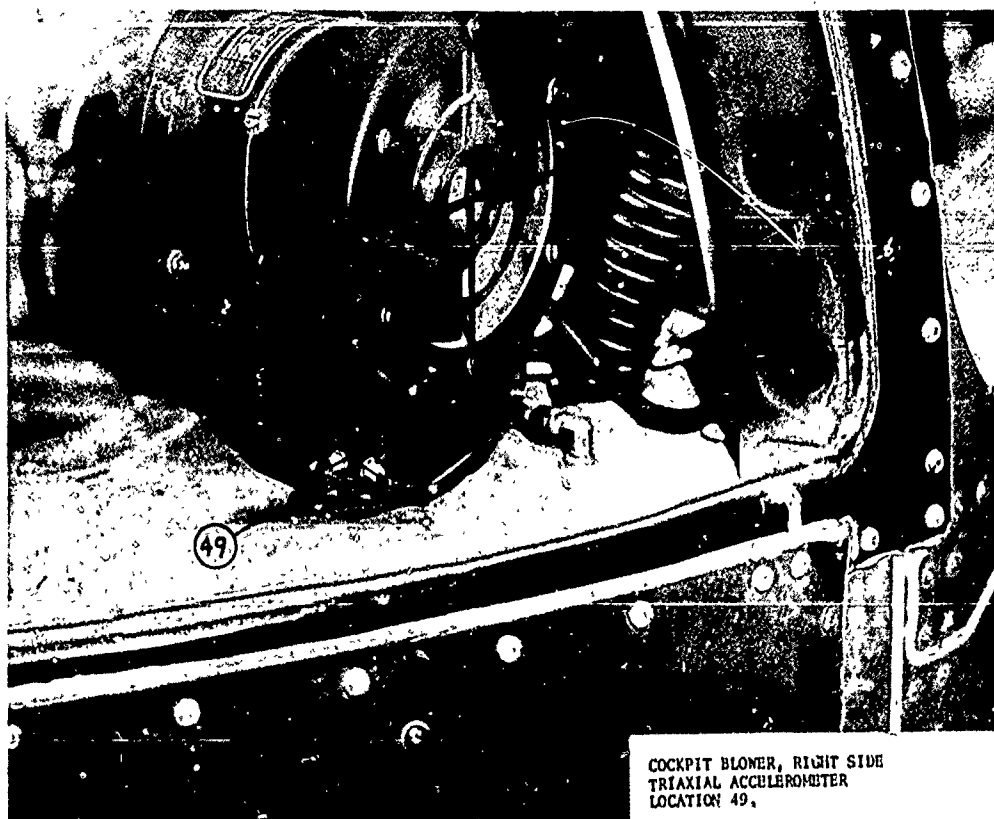


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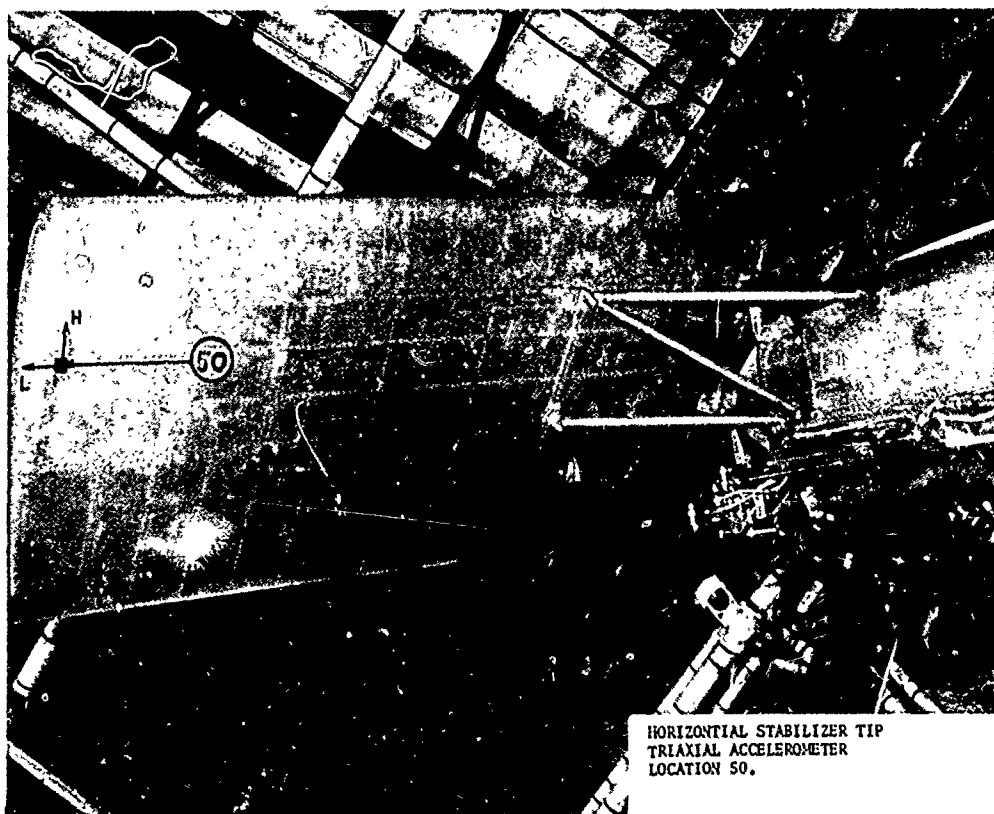


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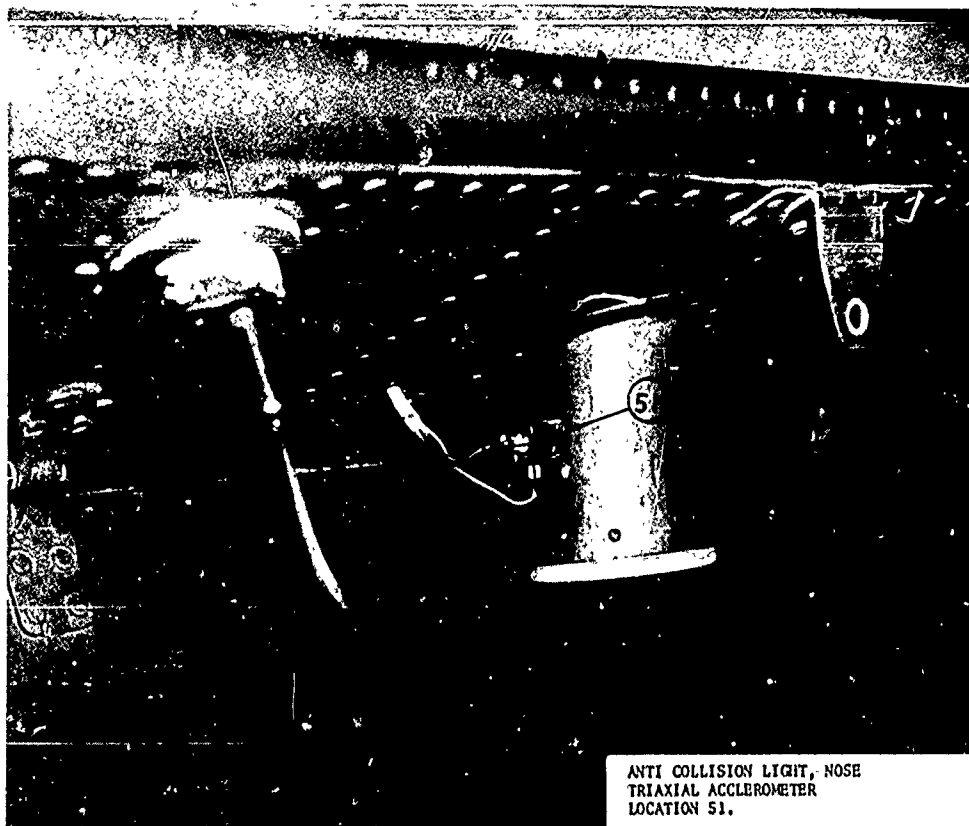


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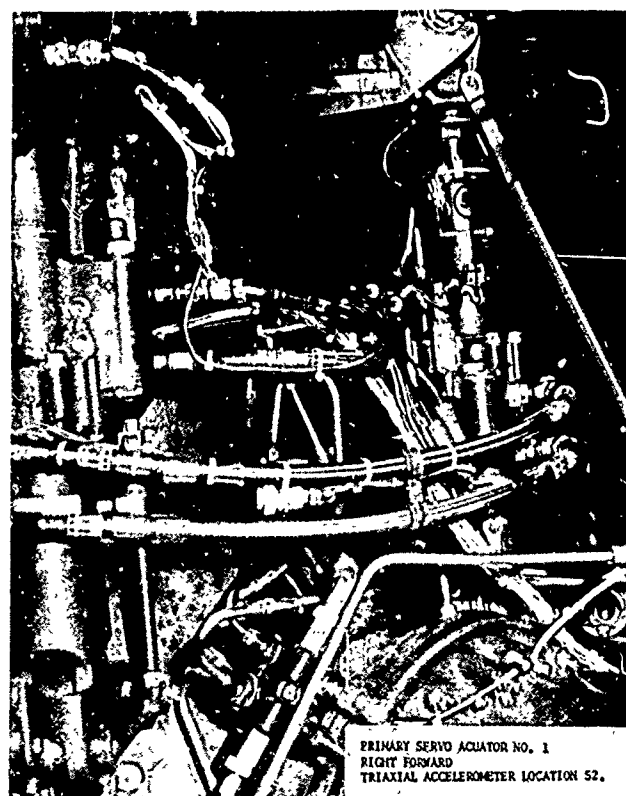


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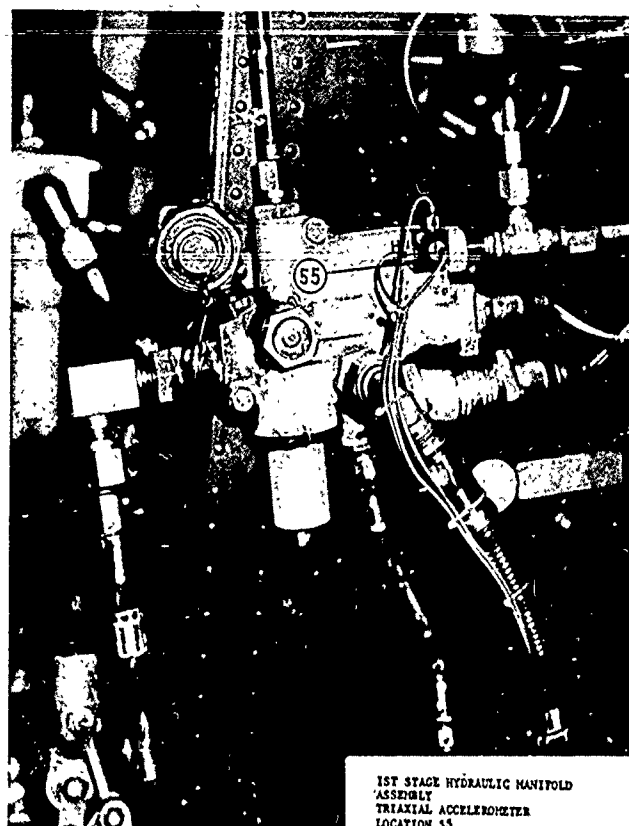


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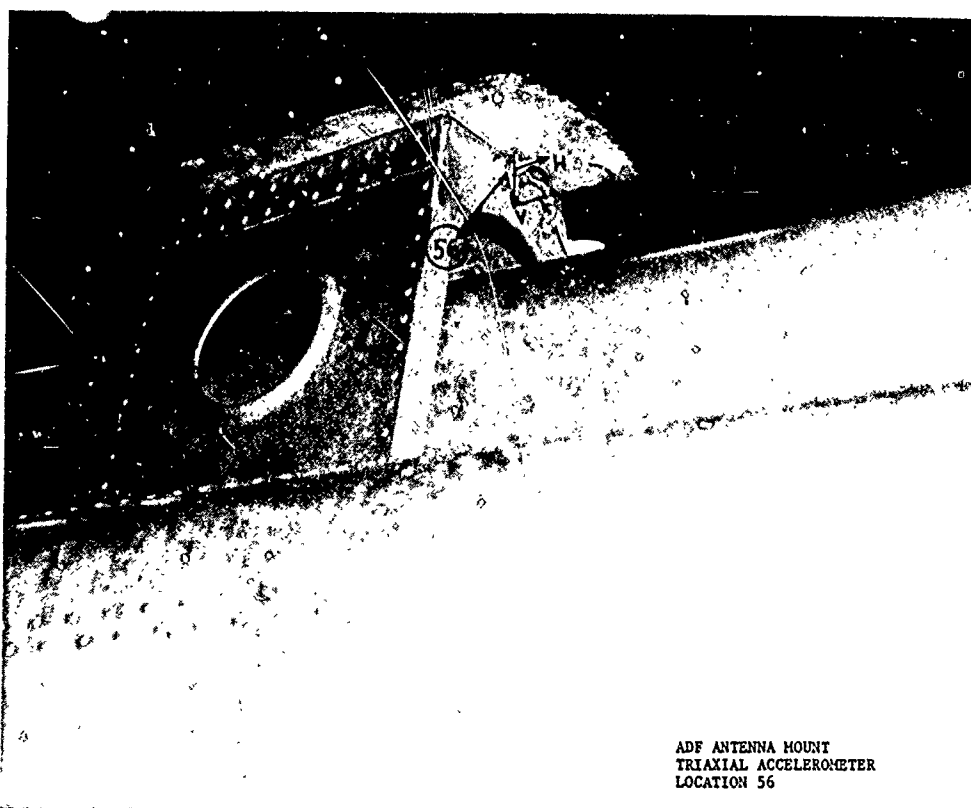
Photo 40.





1ST STAGE HYDRAULIC MANIFOLD  
ASSEMBLY  
TRIAXIAL ACCELEROMETER  
LOCATION 55

Photo 41.



ADF ANTENNA MOUNT  
TRIAXIAL ACCELEROMETER  
LOCATION 56

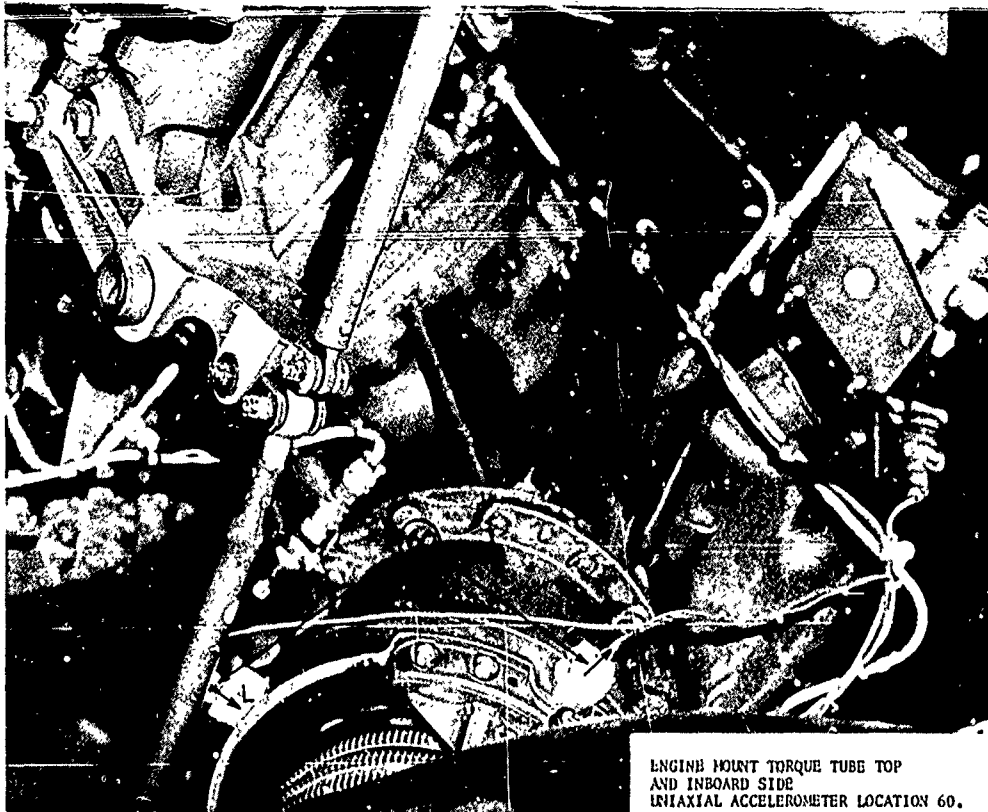
Photo 42.



Photo 43.

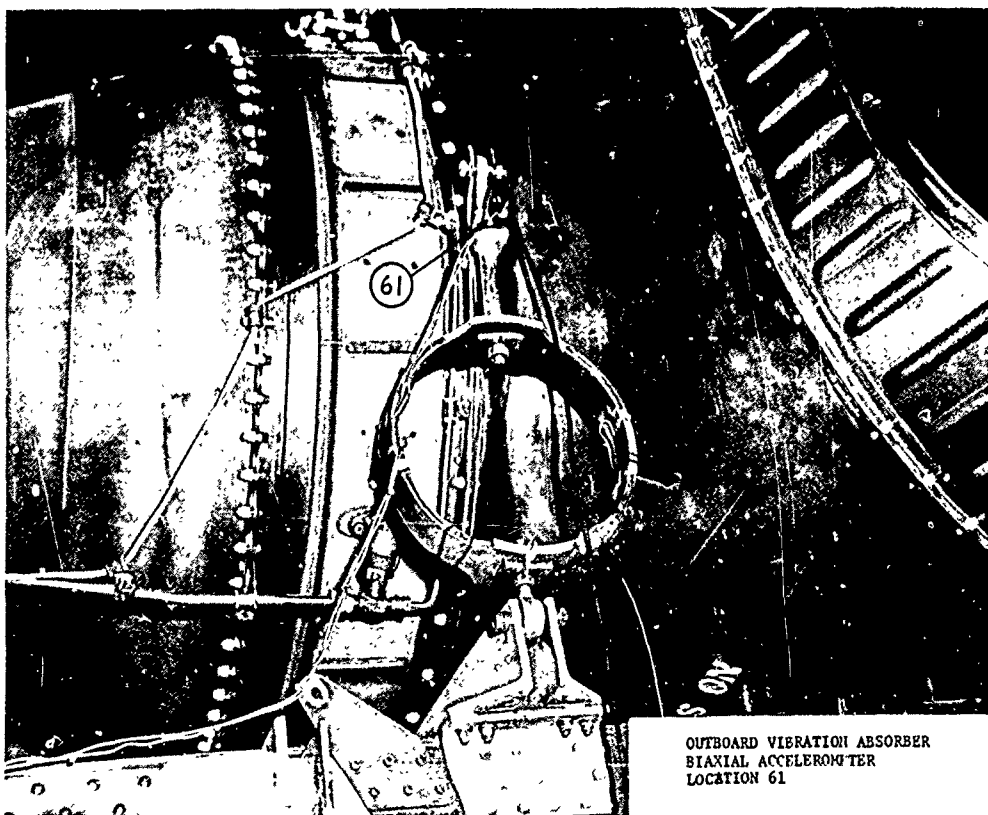


Photo 44.



ENGINE MOUNT TORQUE TUBE TOP  
AND INBOARD SIDE  
UNIAXIAL ACCELEROMETER LOCATION 60.

Photo 45.



OUTBOARD VIBRATION ABSORBER  
BIAXIAL ACCELEROMETER  
LOCATION 61

Photo 46.

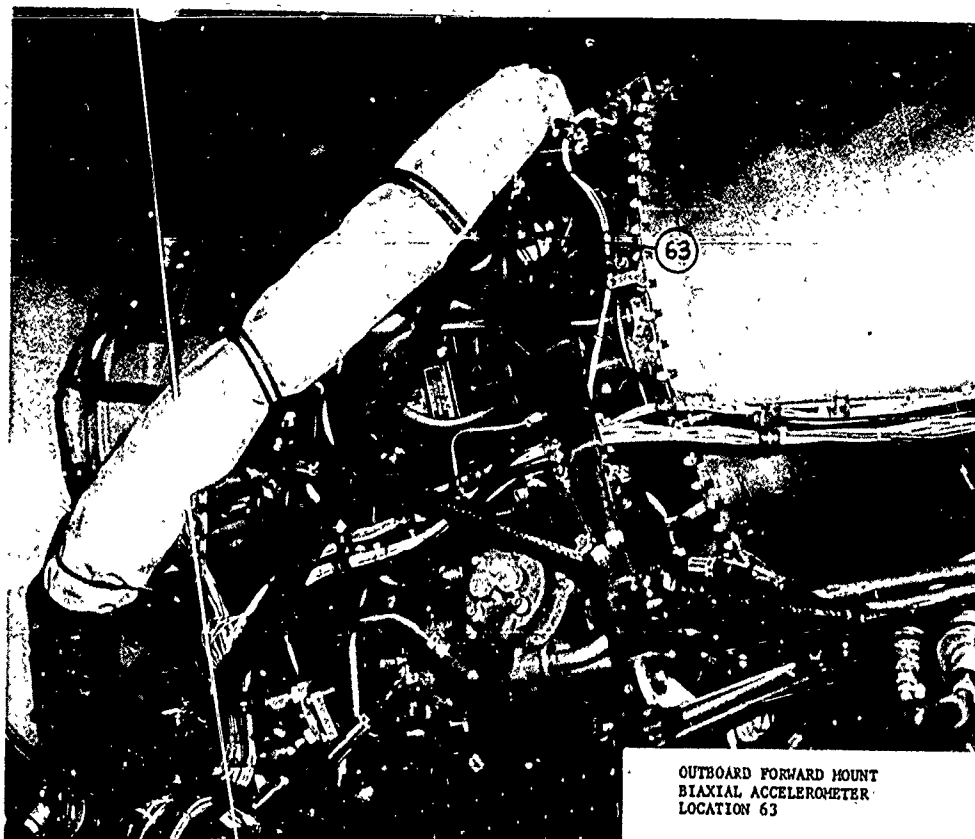


Photo 47.

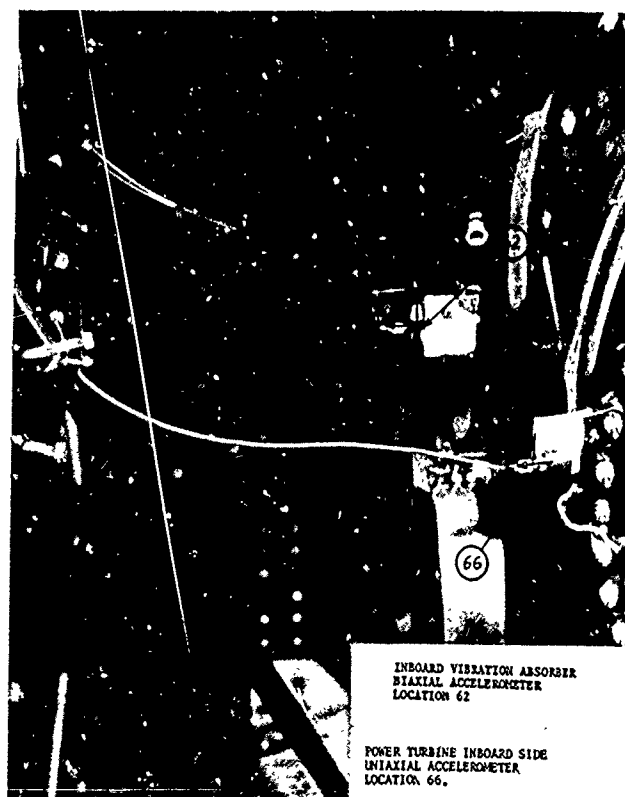


Photo 48.



Photo 49.

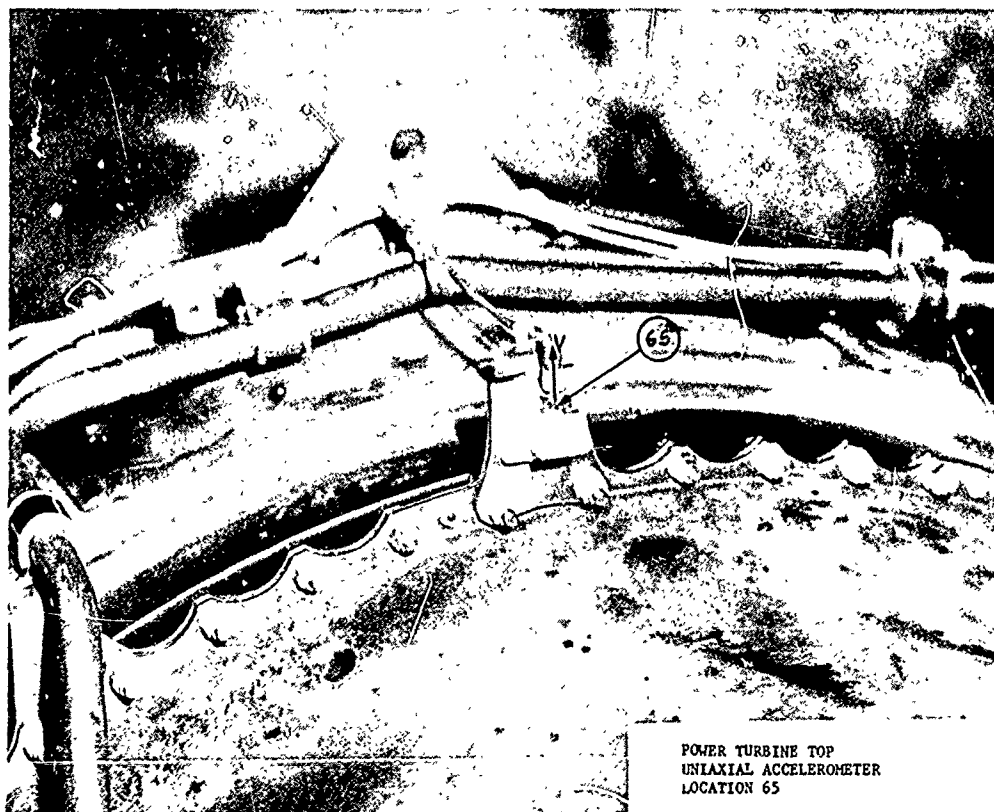


Photo 50.



Photo 51.

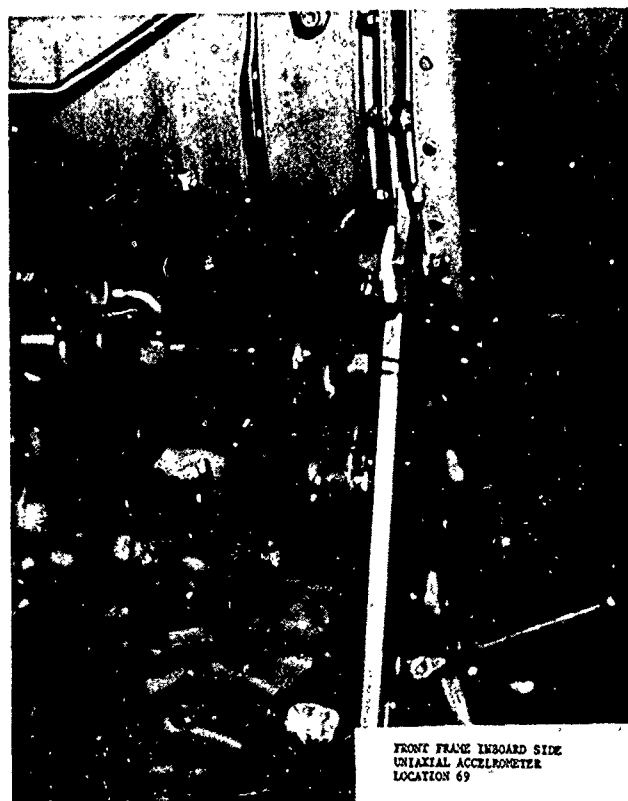
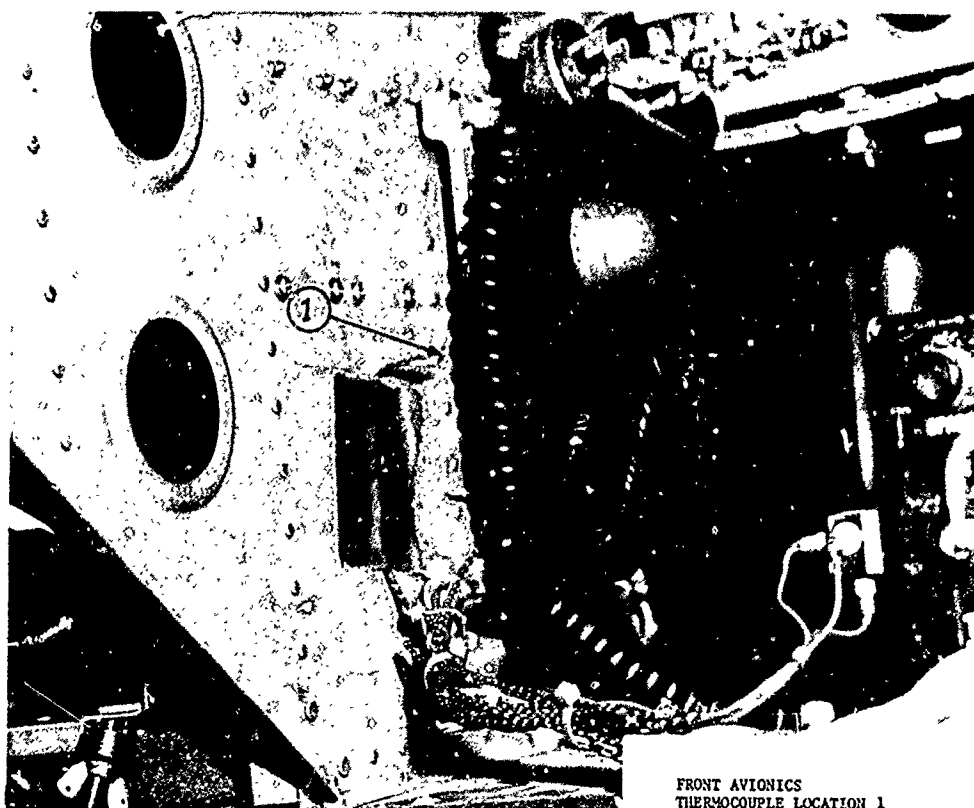


Photo 52.



FRONT FRAME TOP  
UNIAXIAL ACCELEROMETER  
LOCATION 70

Photo 53.



FRONT AVIONICS  
THERMOCOUPLE LOCATION 1

Photo 54.

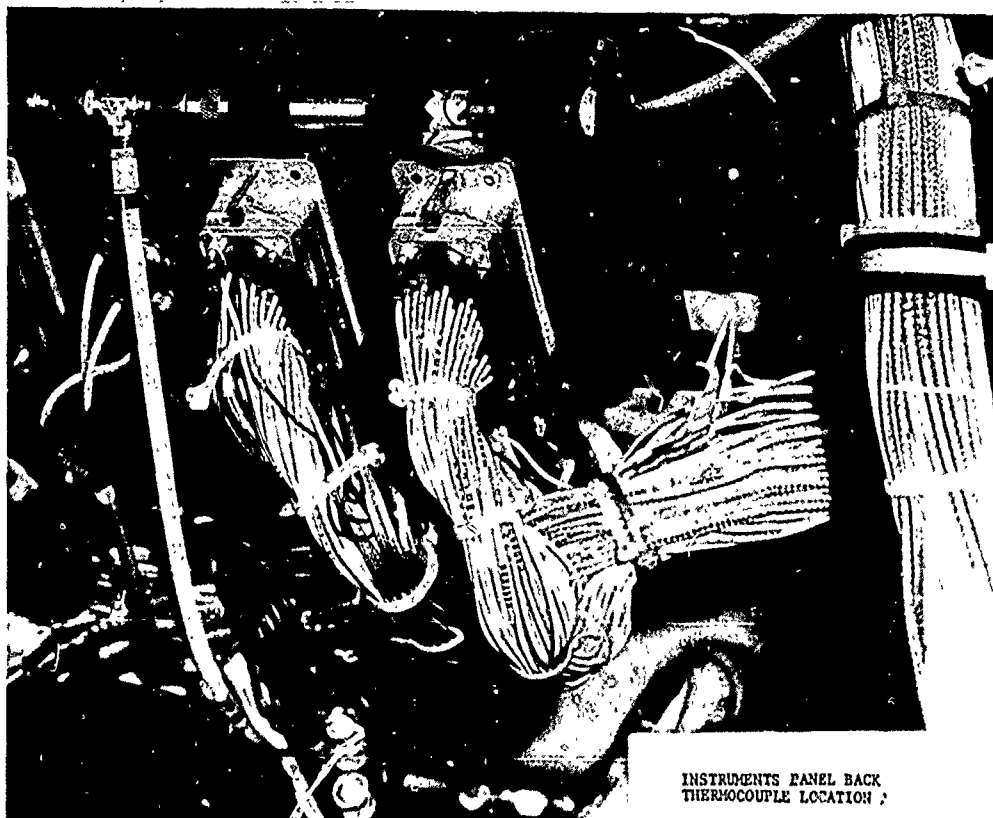


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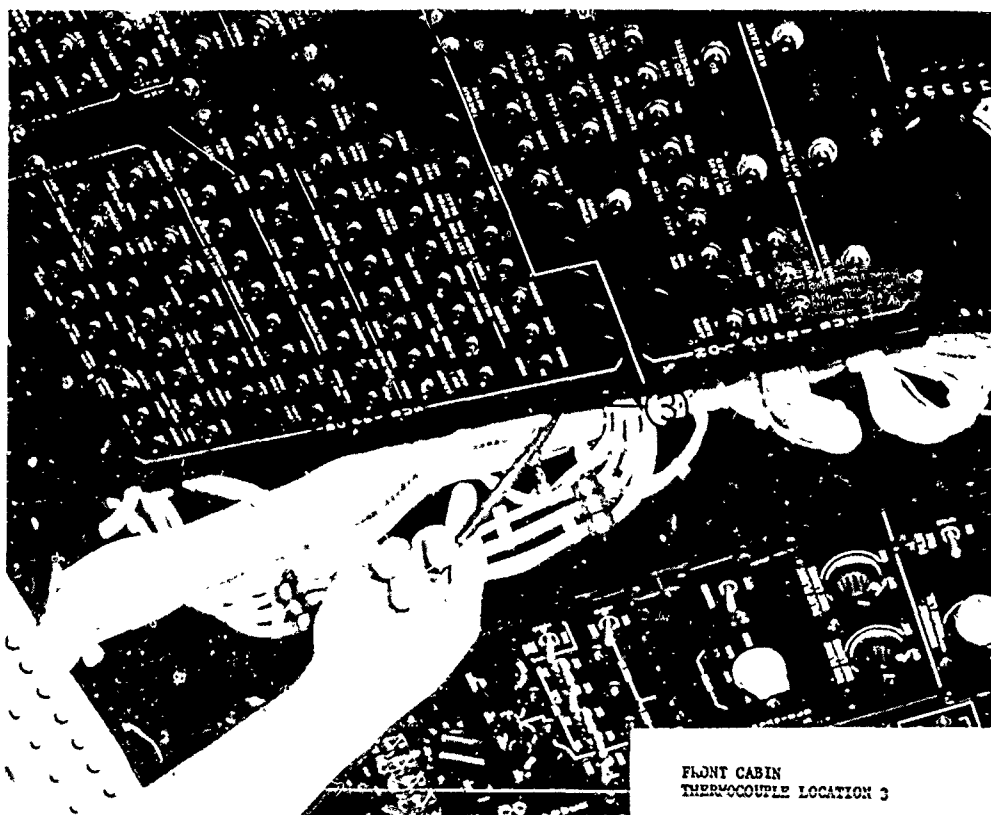


Photo 56.





Photo 57.

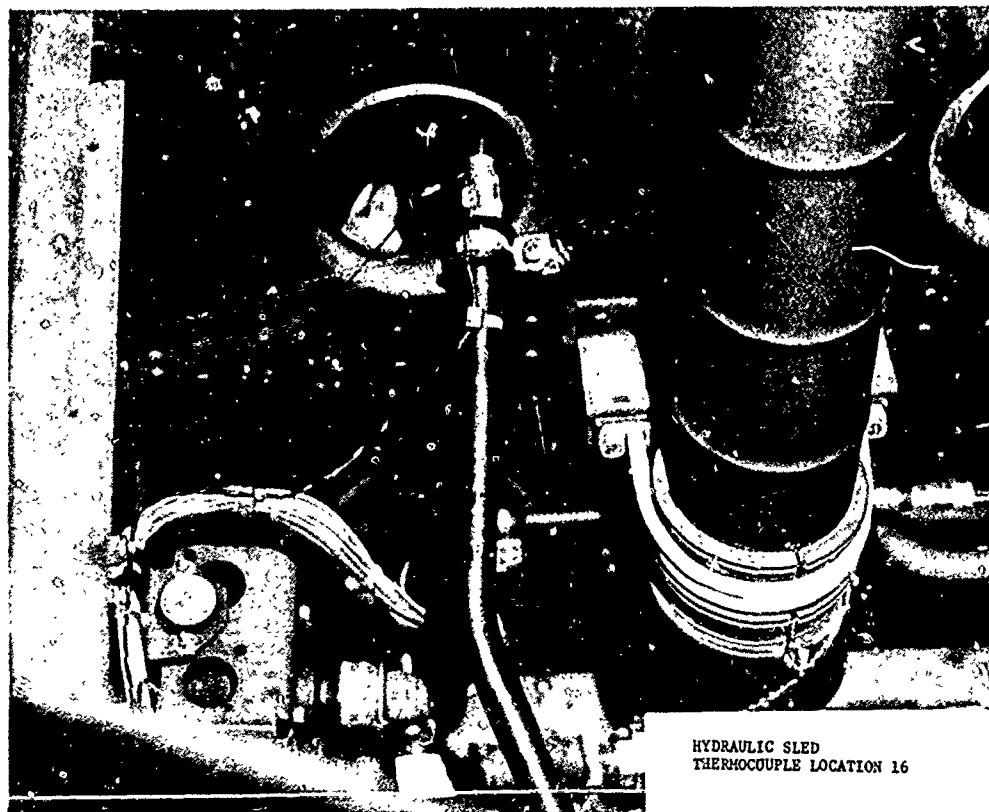


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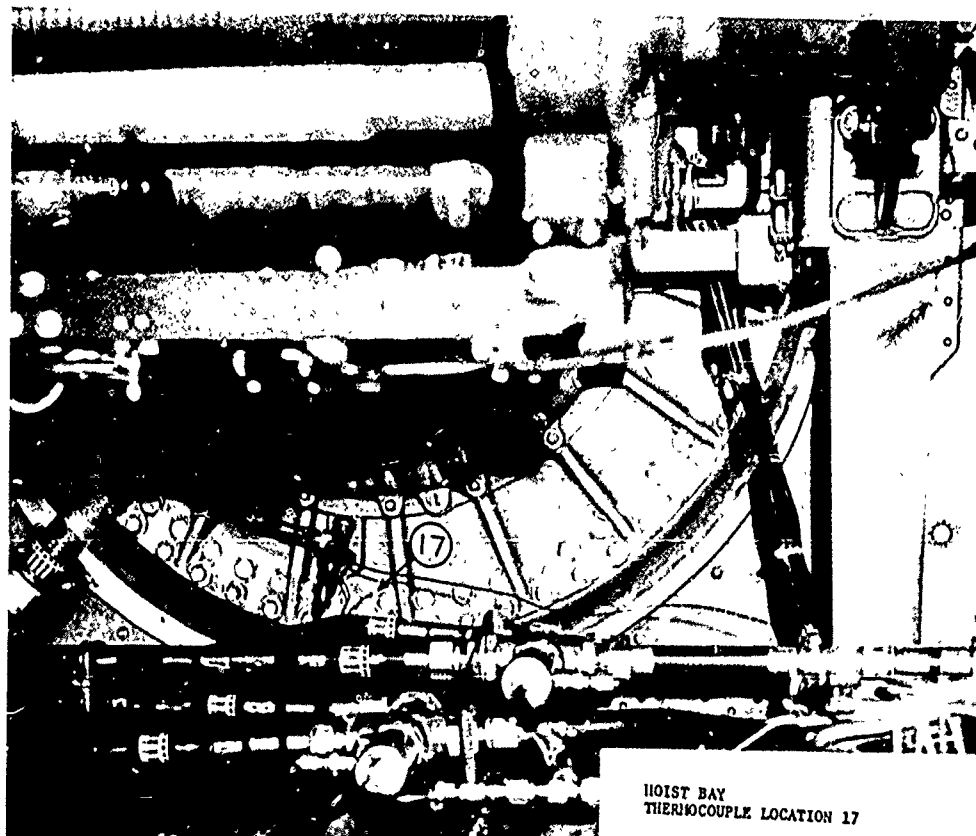


Photo 59.



Photo 60.

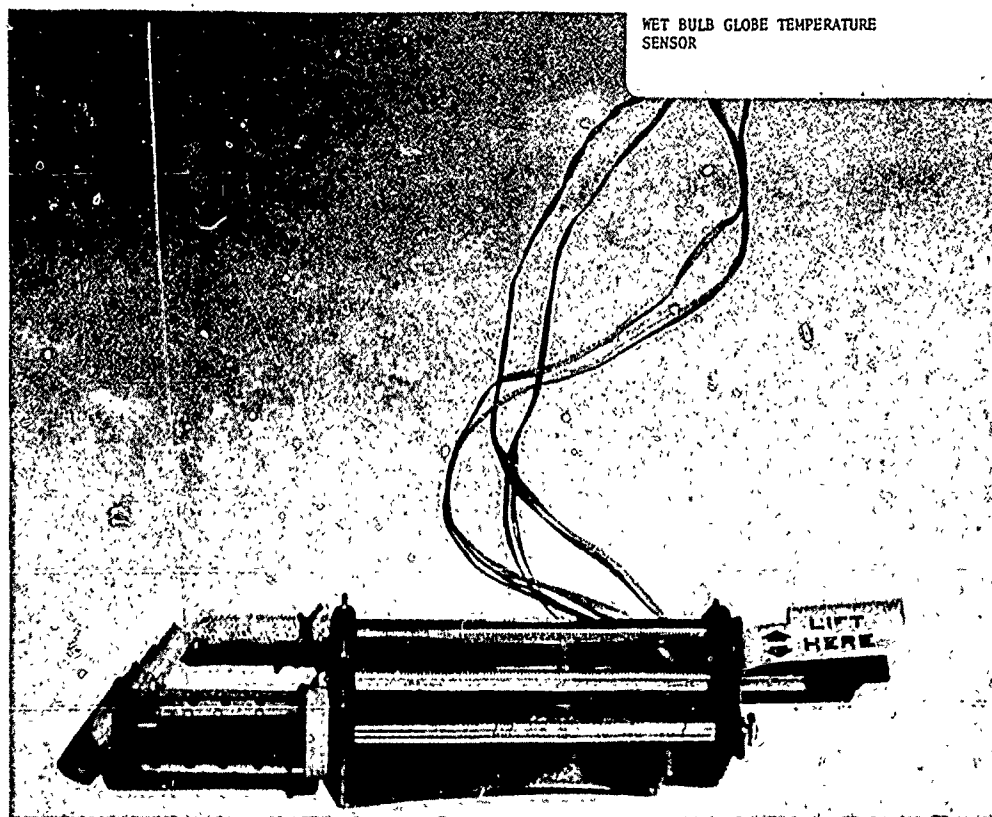


Photo 61.

## APPENDIX F. DATA REDUCTION METHODS

### VIBRATION DATA

1. Because of the discrete frequency content of the data, a narrow-band spectral analysis was performed. A Spectral Dynamics 301 real-time spectral analyzer was utilized to perform the spectral analysis. This spectral analysis converted the data from the time domain (acceleration as a function of time) to the frequency domain (acceleration as a function of frequency). The output of the spectral analysis was a digital plot of acceleration versus frequency composed of acceleration values at 500 discrete frequencies uniformly spaced over the selected frequency range of the spectrum analyzer. The data were analyzed over two frequency ranges: zero to 500 Hz for instruments, avionics, and the pilot station, and zero to 2000 Hz for all other locations with resolution bandwidths of 1 Hz and 4 Hz, respectively. The zero-to-500-Hz analysis range was utilized for all instruments, avionics, and pilot station data, since there were no data of interest above 500 Hz, and the frequency resolution was better on the 500-Hz range than on the 2000-Hz range. The zero-to-2000-Hz analysis range was used for all other locations, since there were significant data above 500 Hz and the maximum instrumentation frequency response was 2000 Hz. Because of the random variation in amplitude, the data were averaged over a period of time to determine the mean acceleration amplitude for each test condition. This data averaging was accomplished with a Spectral Dynamics 302B ensemble averager. Data were averaged over an 8-second time interval for steady-state nonweapons-firing flight conditions, a 2-second interval for maneuvering flight, and a 2-second interval for weapons firing. The 2-second maneuvering flight analysis time interval was selected to cover the most severe vibrations encountered during the maneuver.

2. The following equations were used to calculate the acceleration mean and standard deviation values:

a. Mean ( $\bar{X}$ ):

$$\bar{X} = \frac{\sum_{j=1}^N X_j}{N}$$

b. Standard deviation (S):

$$S = \sqrt{\frac{\sum_{j=1}^N (X_j - \bar{X})^2}{N}}$$

c. Mean plus standard deviation (Y):

$$Y = \bar{X} + S$$

Where:  $X_j$  = acceleration at a specific frequency

N = number of records compressed

3. Figures 1 and 2 are block diagrams of the spectral analysis and data compression procedures.

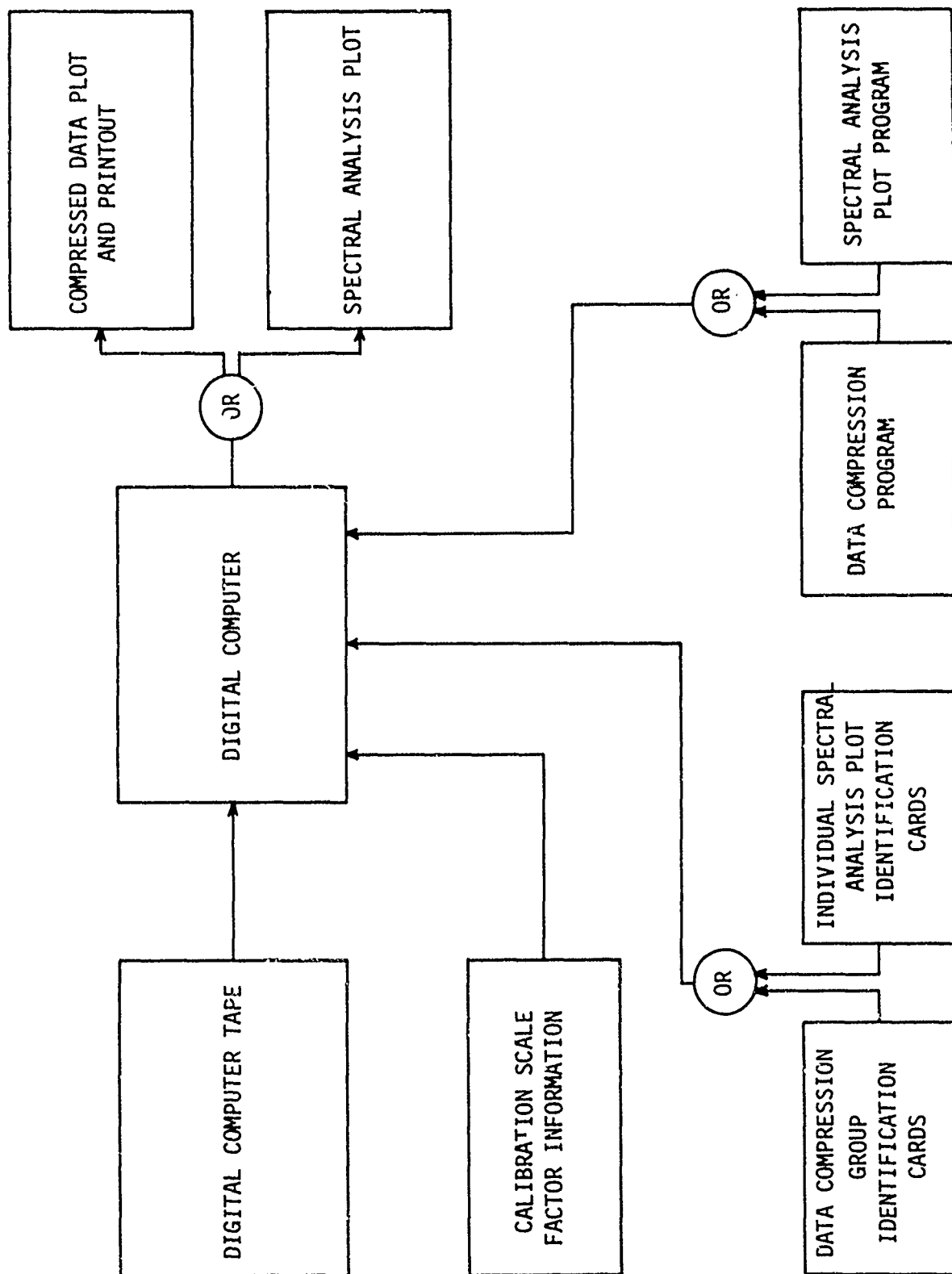
#### TEMPERATURE DATA

4. The electrical analogue shown in figure 3 was developed to predict the temperature of the cabin and avionics under static conditions at values of ambient air temperature and external radiation different than those tested. The results of this analysis are presented in figures 136 through 144, appendix G.

FIGURE 1



FIGURE 2  
PROJECT 70-15 VIBRATION DATA  
COMPRESSION PROCEDURE



<u>ELECTRICAL QUANTITY</u>	<u>HEAT TRANSFER QUANTITY</u>	<u>UNIT (°K)</u>
$V \sim$ Voltage	$T_a \sim$ Ambient air temperature	$^{\circ}\text{K}$
$V_c \sim$ Voltage across capacitor	$T_c \sim$ Transient temperature inside helicopter	$^{\circ}\text{K}$
	$T_{ss} \sim$ Steady-state temperature inside helicopter	$^{\circ}\text{K}$
	$T_o \sim$ Initial temperature inside helicopter	$^{\circ}\text{K}$
$R_1 \sim$ Resistance	$K_c \sim$ Conduction coefficient	$\text{Hr} \cdot ^{\circ}\text{K}/\text{BTU}$
$R_l \sim$ Resistance	$K_r \sim$ Radiation heat transfer coefficient	$\text{Hr} \cdot ^{\circ}\text{K}/\text{BTU}$
$C \sim$ Capacitor	$C \sim$ Heat capacity	$\text{BTU}/^{\circ}\text{C}$
$I \sim$ Current	$E_{ex} \sim$ Total external radiation	$\text{BTU}/\text{hr}$
	$E_a \sim$ Atmospheric radiation (total external radiation minus solar radiation)	$\text{BTU}/\text{hr}$
	$E_s \sim$ Solar radiation	$\text{BTU}/\text{hr}$
$t \sim$ Time	$t \sim$ Time	$\text{Hr}$

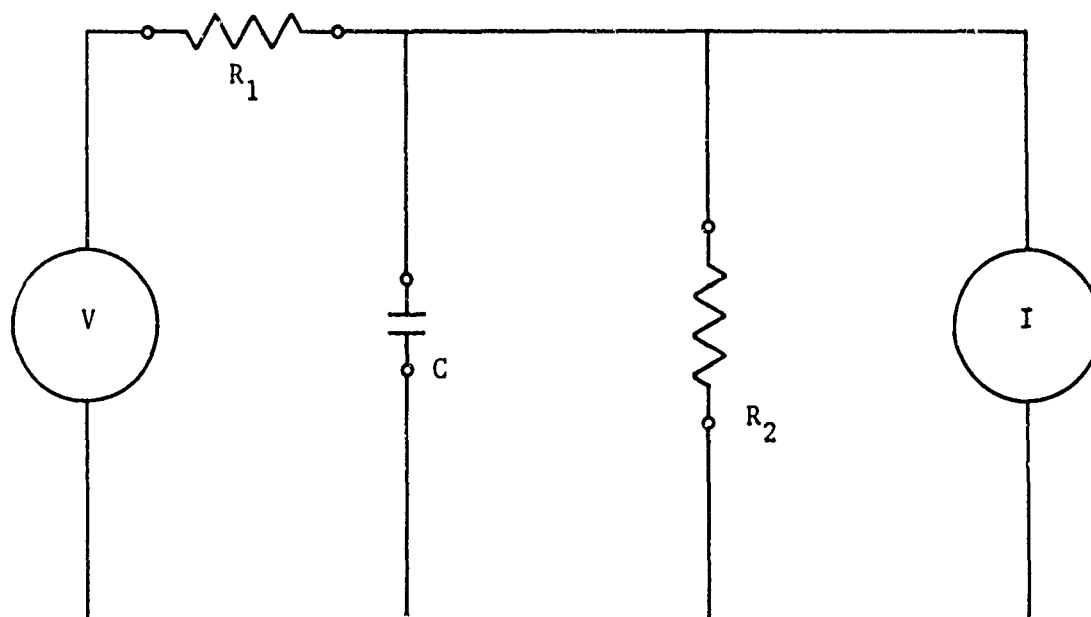


Figure 3. Heat Transfer Electrical Analog.



5. Using the circuit shown in figure 3, the equation describing the transient response of the helicopter to an ambient air temperature and source of external radiation can be written as:

$$T_c = e^{-t/K_{eq}C} \left[ T_0 - \frac{T_a K_r + E_{ex} K_c K_r}{K_c + K_r} \right] + \frac{T_a K_r + E_{ex} K_c K_r}{K_c + K_r} \quad (1)$$

Where:  $K_{eq} = \frac{K_c K_r}{K_c + K_r}$

When  $t$  (time)  $\rightarrow \infty$  the steady-state helicopter temperature  $T_{ss}$  is given by:

Where:  $T_{ss} = \frac{T_a K_r + E_{ex} K_c K_r}{K_c + K_r} \quad (2)$

$$E_{ex} = E_s + \sigma T_a^4$$

$$\sigma = 1.8 \times 10^{-8} \text{ BTU/ft}^2 \cdot \text{hour} \cdot ^\circ\text{K}^4$$

6. Equation 2 was used to find  $K_c$  and  $K_r$  by allowing the helicopter to reach its steady-state temperature at two different constant ambient air temperatures ( $T_{a1}$  and  $T_{a2}$ ) and at two different external radiation values ( $E_{ex1}$  and  $E_{ex2}$ ). This resulted in two equations with two unknowns,  $K_c$  and  $K_r$ , which were solved for  $K_c$  and  $K_r$ , equations 3 and 4.

$$K_c = \frac{T_{a2} T_{ss1} - T_{a1} T_{ss2}}{E_{ex1} T_{ss2} - E_{ex2} T_{ss1}} \quad (3)$$

$$K_r = \frac{T_{ss1} K_c}{T_{a1} + E_{ex1} K_c - T_{ss1}} \quad (4)$$

7. A different  $K_C$  and  $K_R$  were calculated for each temperature sensor location. Each location was considered to comprise an area of 1 square foot which enabled the measured external radiation value in units of BTU/ft<sup>2</sup>-hr to be converted to BTU/hr. These values of  $K_C$  and  $K_R$  were then inserted into equation 2 in order to calculate the steady-state temperature at each temperature sensor location for different values of solar radiation and ambient air temperature than those tested (figs. 136 through 144, app. G).

#### WET BULB GLOBE TEMPERATURE CALCULATION

8. The WBGT index is calculated from the following equation:

$$WBGT = 0.7WB + 0.2GT + 0.1DB$$

Where: WB = Naturally convected wet bulb temperature - °F

DB = Dry bulb temperature - °F

GT = Globe temperature - °F

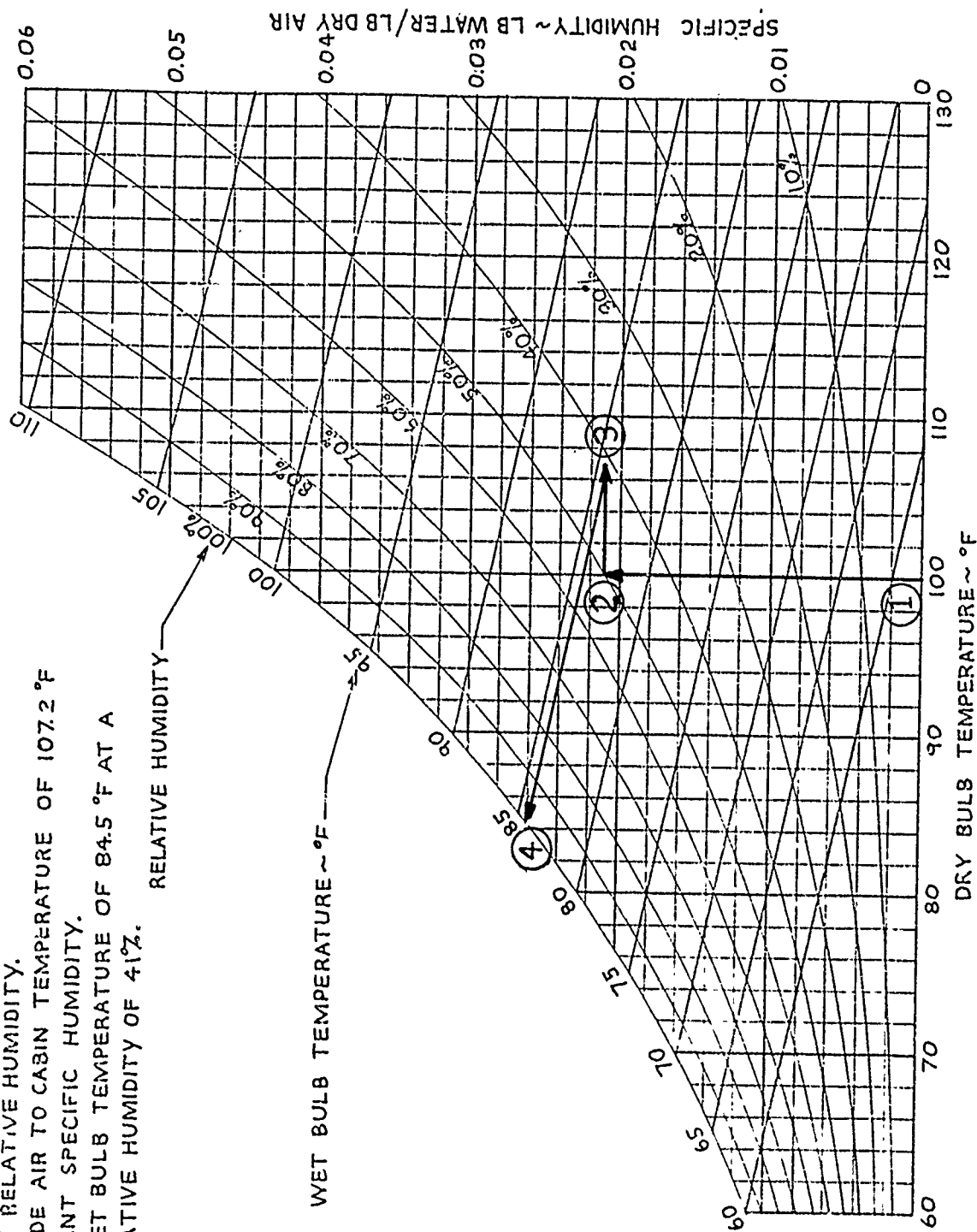
For an outside air temperature of 100°F, a solar radiation value of 250 BTU/hr-ft<sup>2</sup> and an airspeed of 80 KCAS, a cabin temperature of 114.4°F and a globe temperature of 124.8°F can be determined from figure G. At a relative humidity of 50 percent at 100°F, a psychrometric chart can be used to determine a wet bulb temperature of 86.5°F for a cabin dry bulb temperature of 114.4°F. Using these temperature values, the WBGT can be calculated.

$$WBGT = (0.7)(86.5) + (0.2)(124.8) + (0.1)(114.4) = 97.0^\circ\text{F}$$

# FIGURE 4 PSYCHROMETRIC CHART

BAROMETRIC PRESSURE 29.92 IN. Hg

1. ENTER CHART AT OUTSIDE AIR TEMPERATURE OF 100 °F.
2. GO TO 50% RELATIVE HUMIDITY.
3. HEAT OUTSIDE AIR TO CABIN TEMPERATURE OF 107.2 °F AT CONSTANT SPECIFIC HUMIDITY.
4. GO TO A WET BULB TEMPERATURE OF 84.5 °F AT A CABIN RELATIVE HUMIDITY OF 41%.



# APPENDIX G. TEST DATA

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FIGURE 1  
FIRST PASS DATA COMPRESSION ARRAY

[illegible]

FIGURE 1  
FIRST PASS DATA COMPRESSION ARRAY  
CN-54B USA 34 64-18463

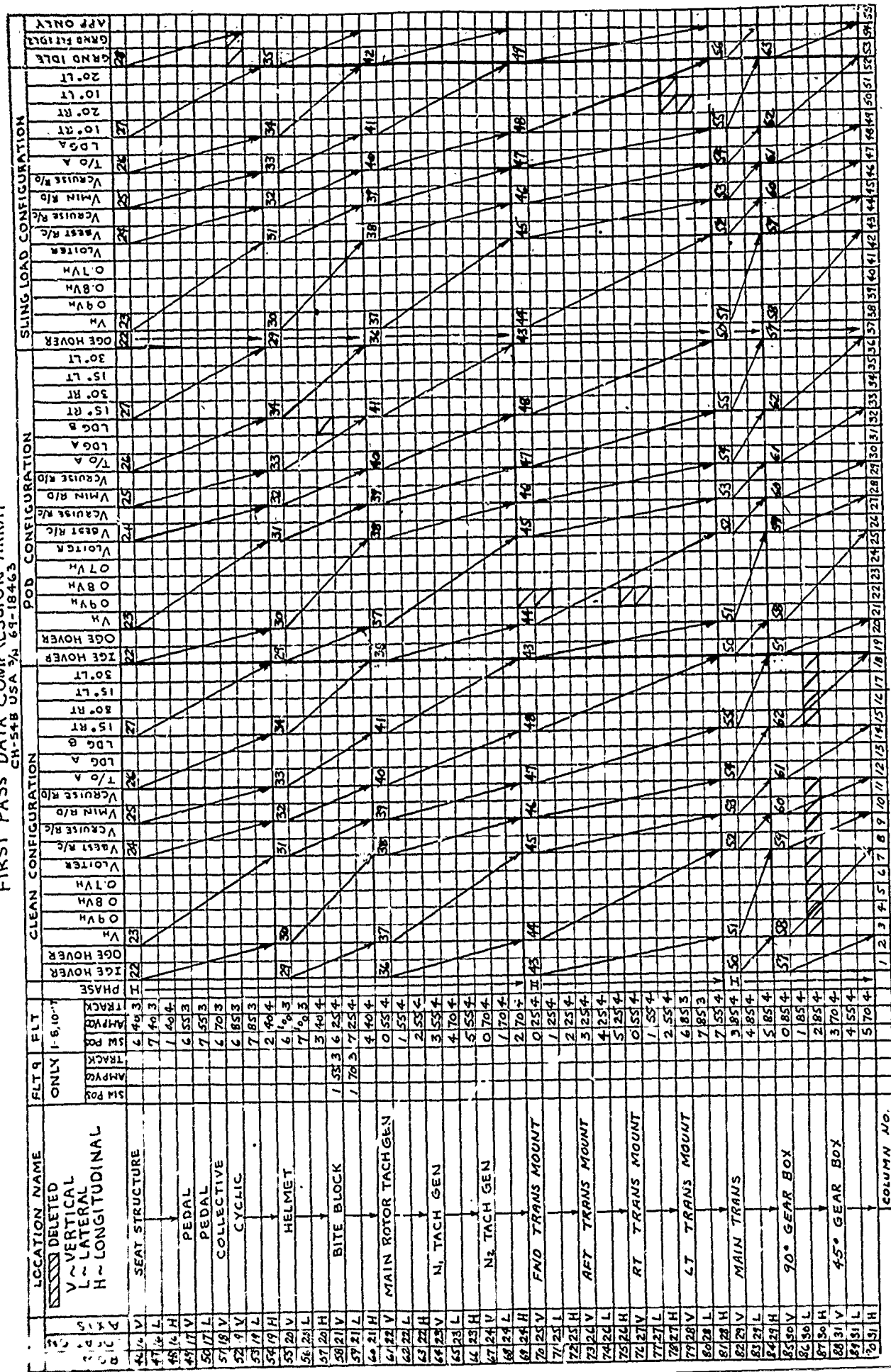


FIGURE 1  
FIRST PASS DATA COMPRESSION ARRAY

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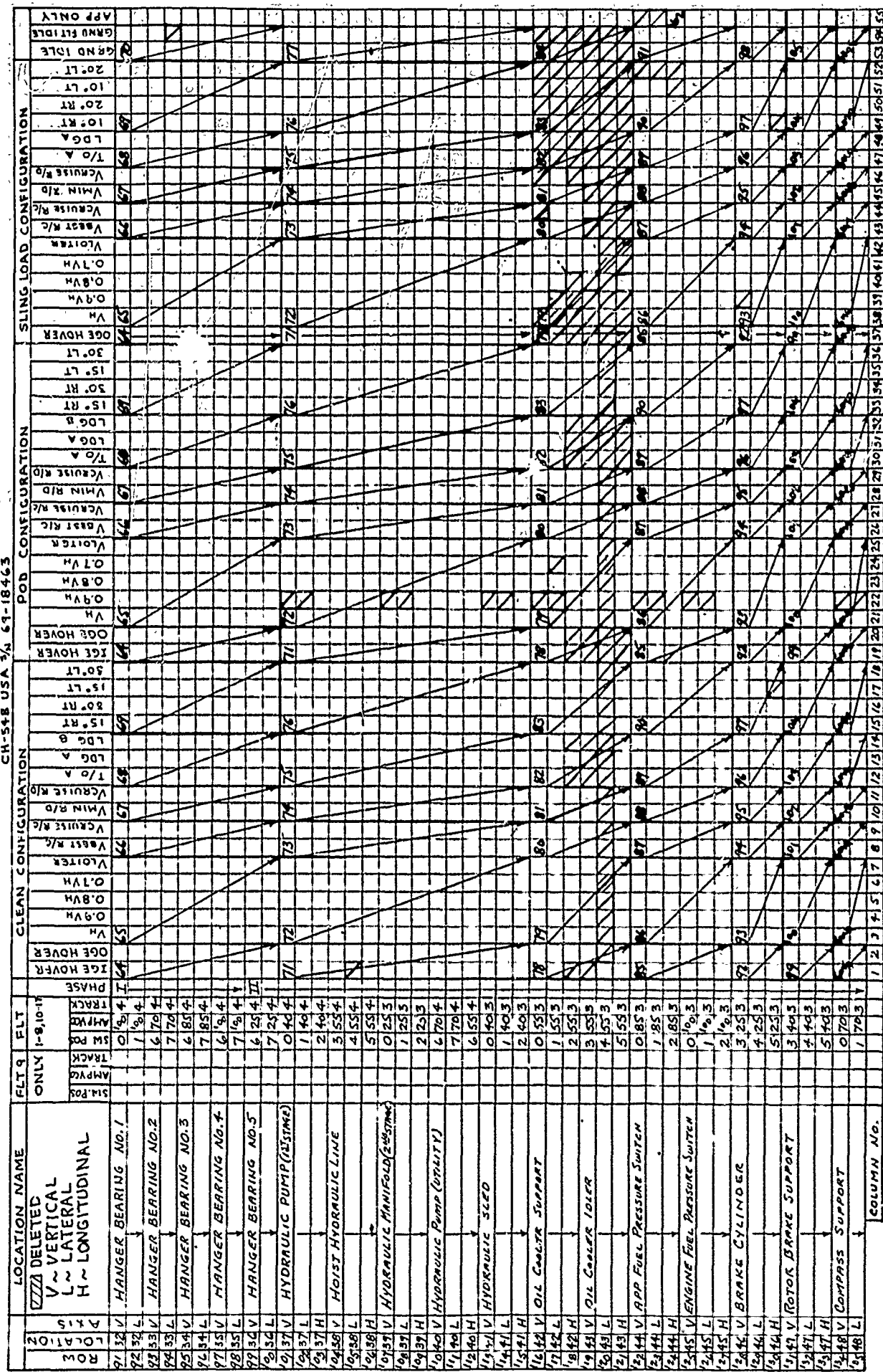




FIGURE 1  
FIRST PA'S DATA COMPRESSION ARRAY  
CH-542 USA 34 69-18463

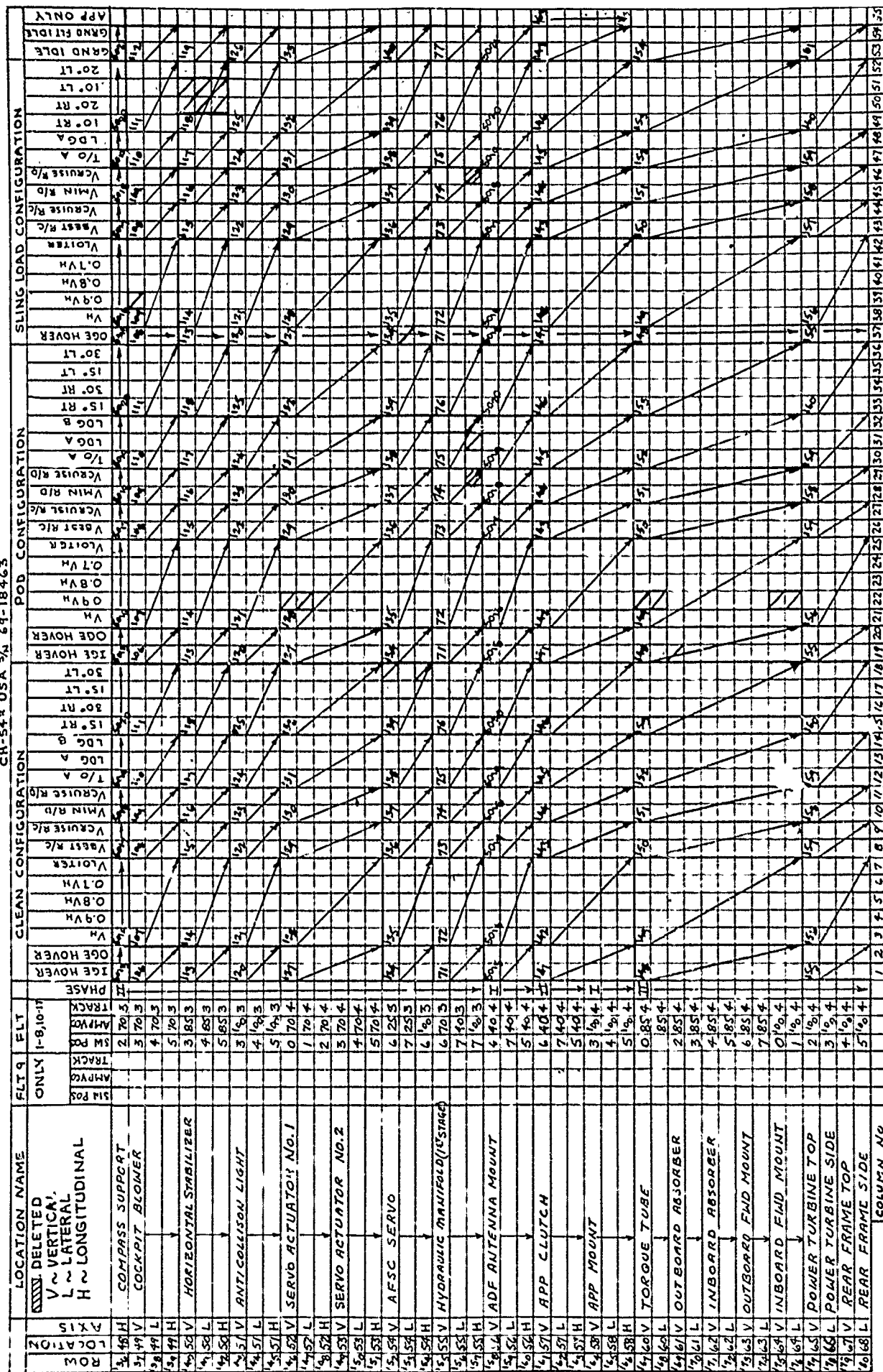


FIGURE 1  
FIRST PASS DATA COMPRESSION ARRAY

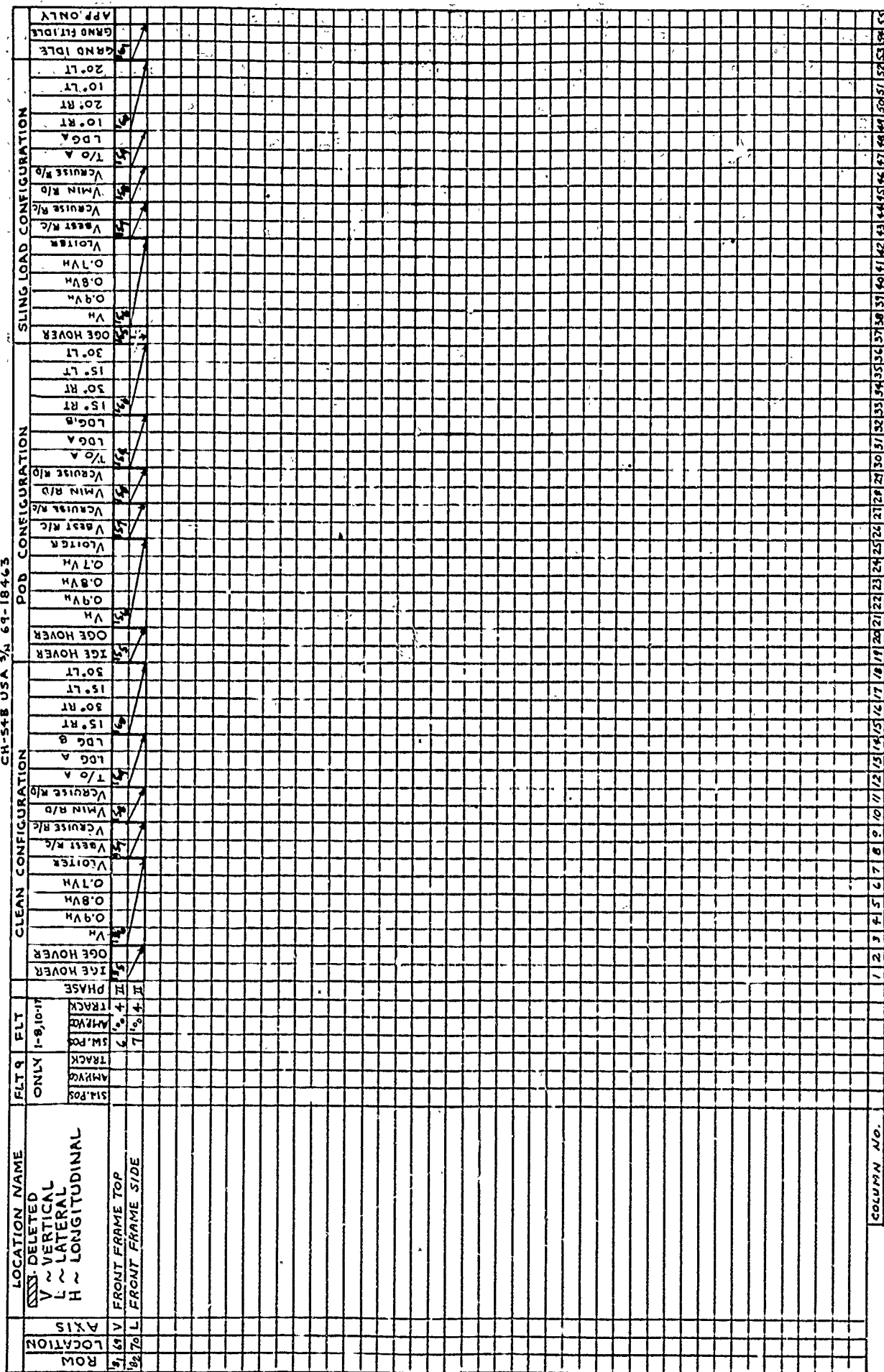


FIGURE 2  
SECOND PASS DATA COMPRESSION ARRAY

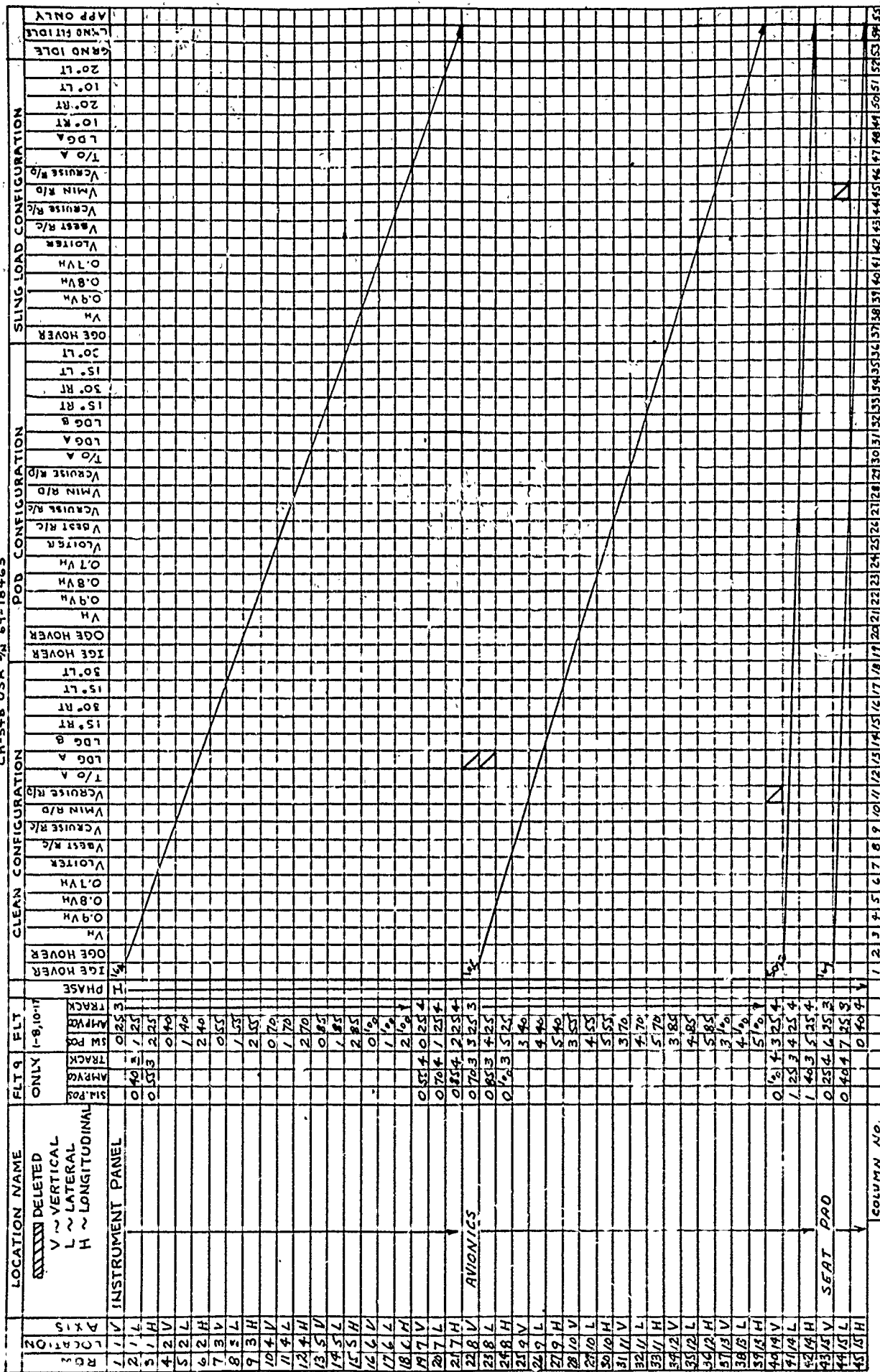


FIGURE 2  
SECOND PASS DATA COMPRESSION ARRAY  
CH-54B USA 3/4 69-18463

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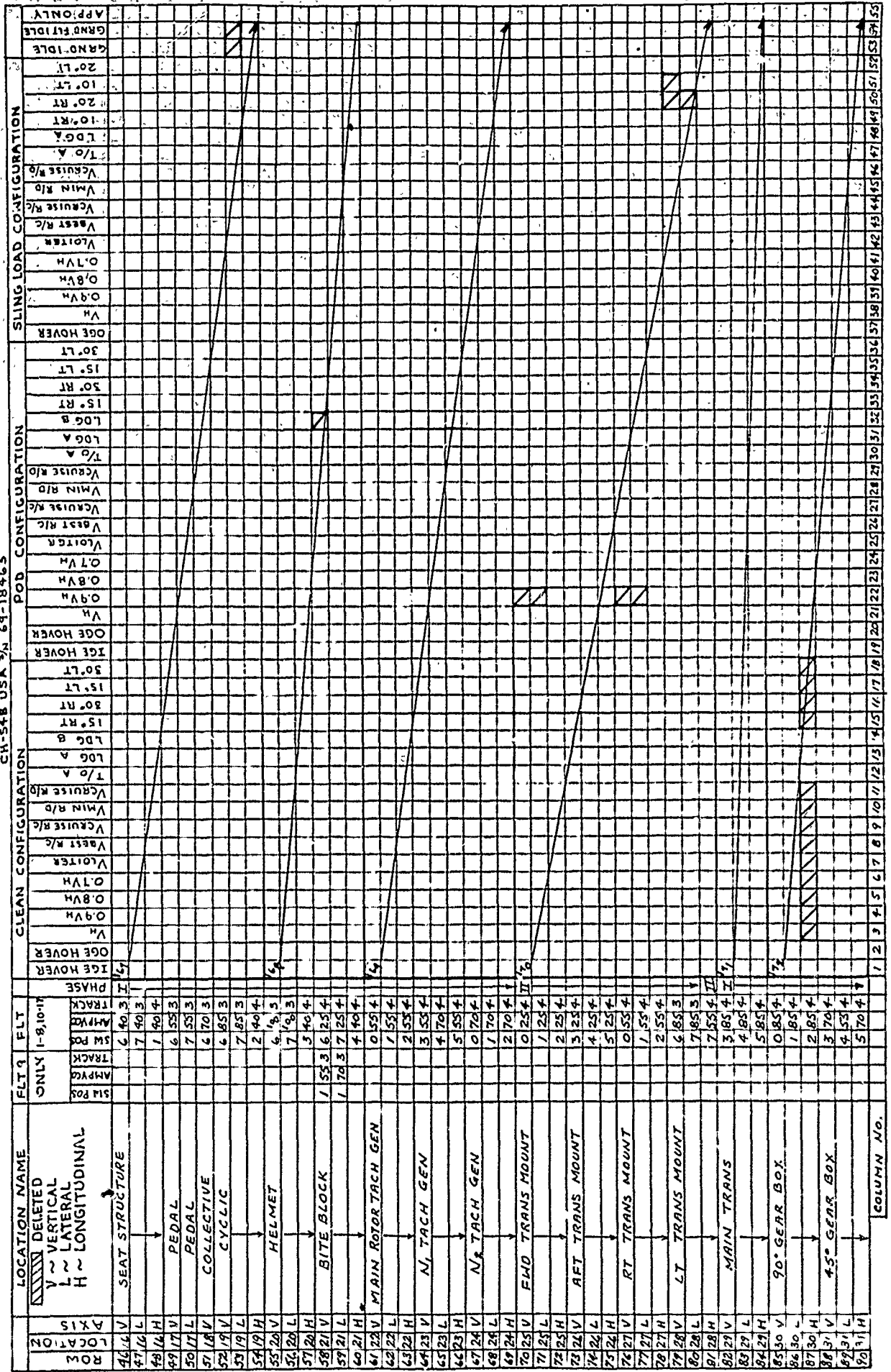




FIGURE 2  
SECOND PASS DATA COMPRESSION ARRAY

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FIGURE 3  
THIRD PASS DATA COMPRESSION ARRAY

PAGE 1 OF 1

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COLUMN NO.

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55

**FIGURE 3**

[illegible]



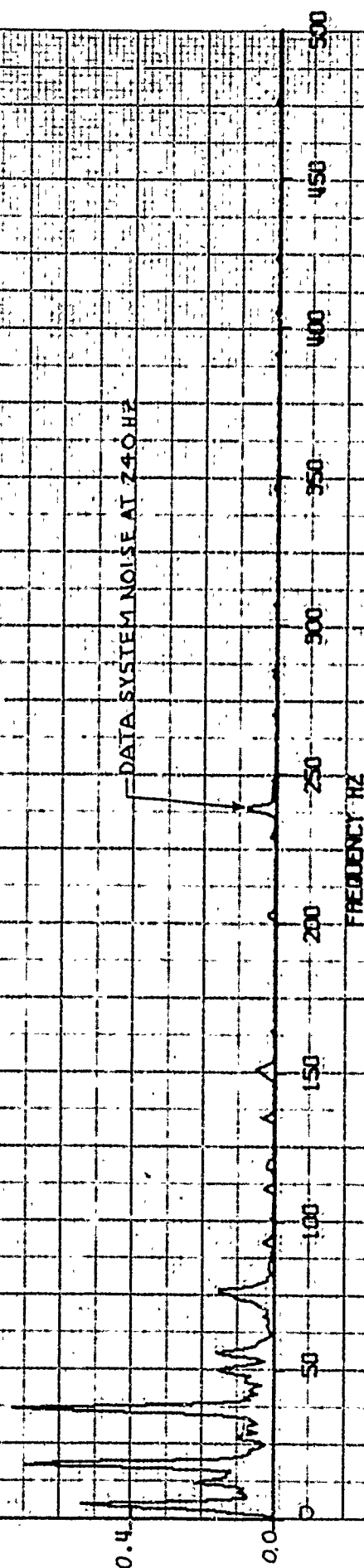
FIG. 4

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH-53B USA S/N 89-18163  
 GROSS WT 28400 AND 41900 LB AVG CG STR-MID CONF G-CLEAR/POD/SLING  
 COMBINED FLT-COND INSTA-PANEL COMBINED AXIS-VIB PLOT 184  
 SENSOR LOC 1.2.3.4.5.6.7 COMPRESSION PASSING 2

CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION 164	
FREQUENCY ~ HZ	FLT COND	CONFIG	AXIS	LOCATION NUMBER	VIB AMPL ~ g	
5.0	OGE	SLING LOAD	LONG	7	0.54	
12.0	LDG A	POD	LONG	7	0.82	
18.0	LDG A	POD	LONG	7	0.70	
37.0	LDG A	POD	LONG	2	0.73	
50.0	25° LT	POD	LONG	1	0.16	
56.0	LDG B	CLEAN	LONG	1	0.17	
76.0/77.0	VERUISE R/C	CLEAN	LONG	1	0.15	

ACCELERATION G'S



FREQUENCY HZ

FIG 5

## COMPRESSED VIBRATION DATA

CH 516 USA 3/1 69-18163  
GROSS WT 28400 AND 11900 LB AVG CG STA MID CONFIG-CLEAN/NOO/S INC  
COMBINED FLT BANDS INSTR-PANEL COMBINED AXIS Y18 PLT 181  
SENSOR LOC 1.2.3.4.5.6.7 COMPRESSION PASS NO.2

MEAN ACCELERATION  
MEAN PULSE 3 SIGMA UPPER ACCELERATION LIMIT

MEAN ACCELERATION  
MEAN PULSE 3 SIGMA UPPER ACCELERATION LIMIT

DATA SYSTEM NOISE AT 240HZ

FREQUENCY HZ

77

100

FIG. 6

## COMPRESSED VIBRATION DATA - MAXIMUM ACCELERATION

GROSS WT 2800 AND 4190 LB. USA SN 69-18063  
 CONFIG CLEANZ POD/SLING  
 COMBINED FLT COND. AVGNES COMBINED AXES VIB FLT 195  
 SENSOR LOC 8.9, 10.1, 12.13 COMPRESSION PASSING 2

2.0

CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION J25	
FREQUENCY ~ HZ	FLT COND	CONFIG	AXIS	LOCATION NUMBER	VIB AMPL ~ g	
18.0	LDG B	CLEAN	LONG	13	0.53	
37.0	LDG A	POD	LAT	13	0.11	
55.0	LDG B	CLEAN	VERT	12	0.13	
76.0	10° RT	SLING LOAD	VERT	13	0.13	
256.0	LDG A	POD	LONG	12	0.24	
262.0	T/O	SLING LOAD	LONG	12	0.21	
352.0	25° LT	POD	LAT	12	0.16	
368.0	LF (VH)	CLEAN	LAT	13	0.35	
375.0	LF (VH)	CLEAN	LAT	13	0.28	
380.0	15° LT	CLEAN	LAT	13	0.26	

ONE HALF PERK TO PEAK ACCELERATION G

1.6

1.2

0.8

0.4

0.0

DATA SYSTEM NOISE AT 240 HZ

50

100

150

200

250

300

350

400

450

500

FREQUENCY HZ

12

FIG. 7

## COMPRESSED VIBRATION DATA

CH-54B USA S/N 69-18463  
 GROSS WT 2840G-RND 11900LB  
 COMBINED FLT C-405 AVIONICS COMBINED AX-S-V10-PL01-195  
 SENSOR LOC 8,9,10,11,12,13 COMPRESSION PASS NO 2

2.0

1.6

1.2

0.8

0.4

0.0

ONE HALF PEAK TO PEAK ACCELERATION G

MEAN ACCELERATION

MEAN RMS 3 SIGMA UPPER ACCELERATION LIMIT

DATA SYSTEM NOISE AT 240HZ

B

50

100

150

200

250

300

350

400

450

500

FREQUENCY Hz

15



FIG 8

COMPRESSED VIBRATION DATA MAXIMUM RECELERATION

GT-SUG USR SN 69-18063  
 CROSS RT 2800LB AVG LG STR MID COMB LG-CLEAN  
 COMBINED FLT COND W/ONICS RT FUEL POC COMBINED AXIS VIB PL 5022  
 SENSOR LOCATION'S 13, 48, 56

CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION 5022
FREQUENCY ~HZ	FLT COND	CONFIG	AXIS	LOCATION NUMBER	VIB AMPL ~g
12.0	LDG A	CLEAN	VERT	48	1.39
52.0	LDG B	CLEAN	VERT	48	4.27
228.0	25° RT	POD	LAT	56	1.39
332.0	OGE	SLING LOAD	LONG	56	1.73
404.0	IGE	CLEAN	LONG	56	1.64
1360.0	VERUISE R/D	CLEAN	LONG	48	2.45
1376.0	VERUISE R/D	CLEAN	LONG	48	2.62
1396.0	25° LT	POD	LAT	14	5.03
1420.0	T/O	POD	LAT	14	4.14
1900.0	LDG A	SLING LOAD	LONG	14	2.16
1916.0	T/O	POD	LONG	14	3.06
1932.0	OGE	SLING LOAD	VERT	14	3.14
1944.0	T/O	POD	VERT	14	3.57

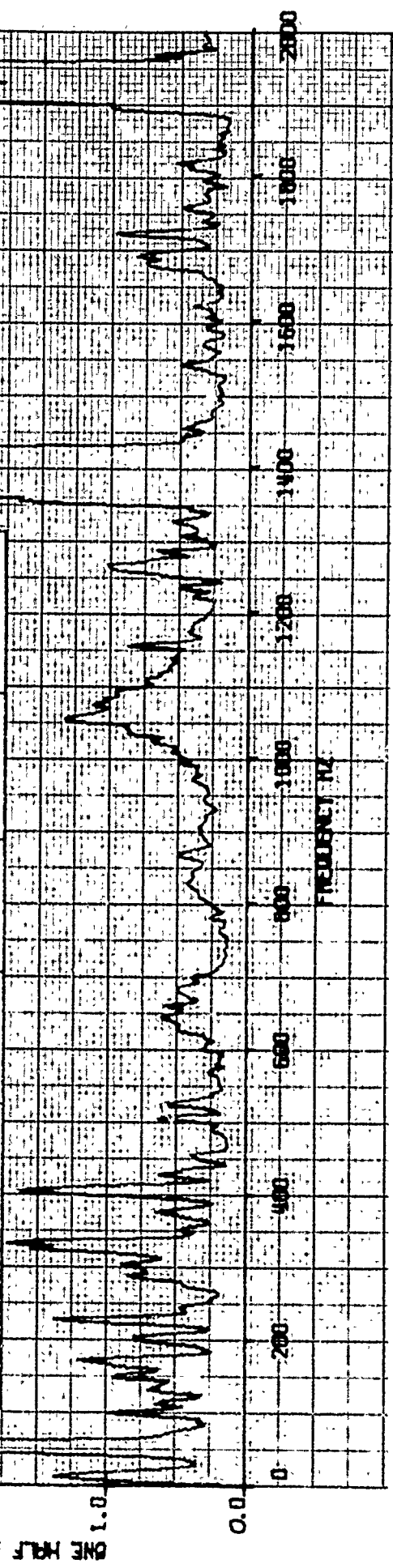


FIG. 9

## COMPRESSED VIBRATION DATA

CH-54B LSR 3/N 69-18463

Q1033-11 204000.0 AVG CC STR N10 CONF10-CLEAN  
COMBINED FC CONES AVIATION-RT FUSELAGE COMBINED MBS VIB P1-B1 5022  
SENSOR LOCATIONS 14, 48, 56

5.0

4.0

3.0

2.0

1.0

0.0

ONE HALF PEAK TO PEAK ACCELERATION G

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

0 200 400 600 800 1000 1200 1400 1600 1800 2000

FREQUENCY Hz

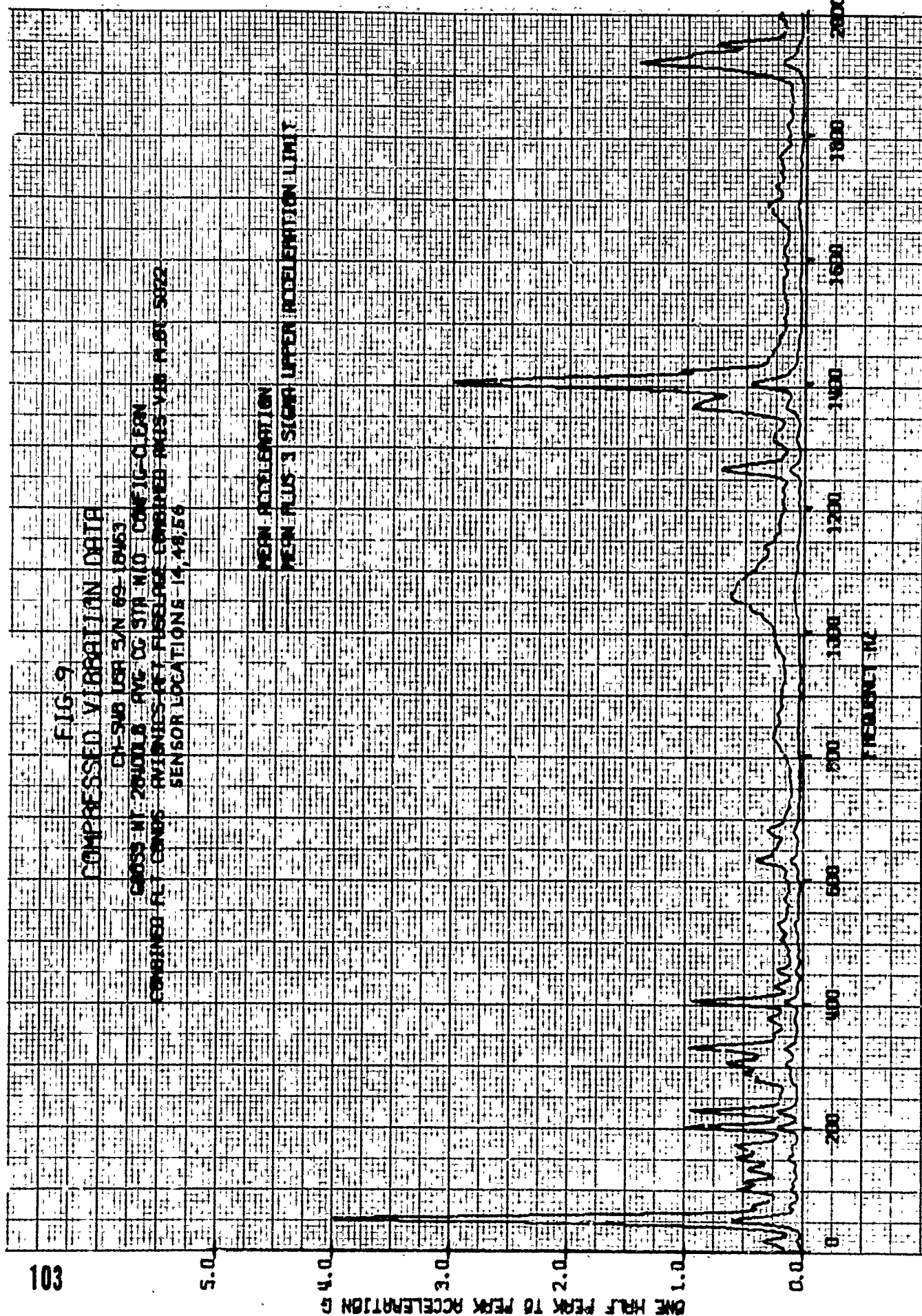


FIG 10

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CM-548 USA S/N 59-18463  
 GROSS WT 28000 AND 41900LB AVG CG STATION CONE/CLEAN/POD/SLING  
 COMBINED-FLT-COND HUMAN FACTORS INPUT COMBINED AXIS VIB. PLOT 157  
 SENSOR LOC 15, 16, 17, 18, 19 COMPRESSION PASS NO. 2

2.0

ONE HALF PEAK TO PEAK ACCELERATION G

1.6

1.2

0.8

0.4

0.2

CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION 167	
FREQUENCY ~ HZ	FLT COND	CONFIG	AXIS	LOCATION NUMBER	VIB AMPL ~ g	
4.0	LF (VLOITER)	SLING LOAD	LAT	19	0.22	
18.0	LDG A	SLING LOAD	LONG	15	0.27	
77.0	LF (2 V4)	SLING LOAD	VERT	19	0.24	
148.0	LDG A	POD	VERT	17	0.26	
152.0	LDG A	SLING LOAD	VERT	17	0.27	
159.0	LDG A	SLING LOAD	VERT	17	0.33	
164.0	LDG A	SLING LOAD	VERT	17	0.33	
168.0	LDG A	SLING LOAD	VERT	17	0.42	
353.0	25° LT	POD	LAT	17	0.26	
364.0	LDG A	SLING LOAD	LAT	17	0.24	

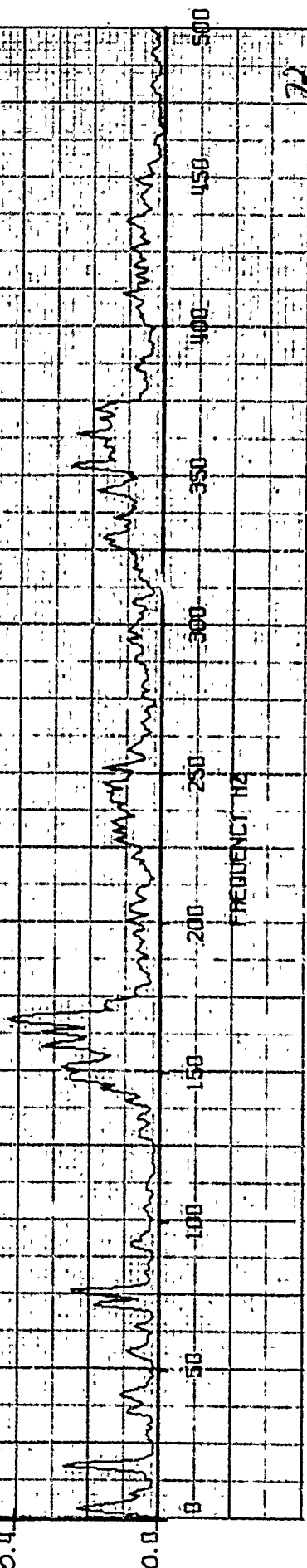


FIG. 11

## COMPRESSED VIBRATION DATA

CRASS RT 28400 AND DISMOLB HVG CG STR-MID CONF-UTERN/POH/SLING  
 COMBINED FLT CORUS HUMAN FACTORS INFLT COMBINED AXIS Y18 PLOT 167  
 SENSOR LOC 15 16 17 18 19 COMPRESSION PASS NO. 2

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

ONE HALF PEAK TO PEAK ACCELERATION G

2.0

1.6

1.2

0.8

0.4

0.0

500

400

300

200

100

0

-100

-200

-300

-400

-500

FREQUENCY HZ



FIG 12

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH-54B USA S/N 69-10463  
 GROSS WT: 28400 AND 41900LB AVG CG STA-M10 CONFIG-CLEAN/POD/SLING  
 COMBINED FLT COND'S HUMAN FACTORS OUTPUT COMBINED AXIS VIB PLOT 168  
 SENSOR LOC 20.21 COMPRESSION PASS NO.2

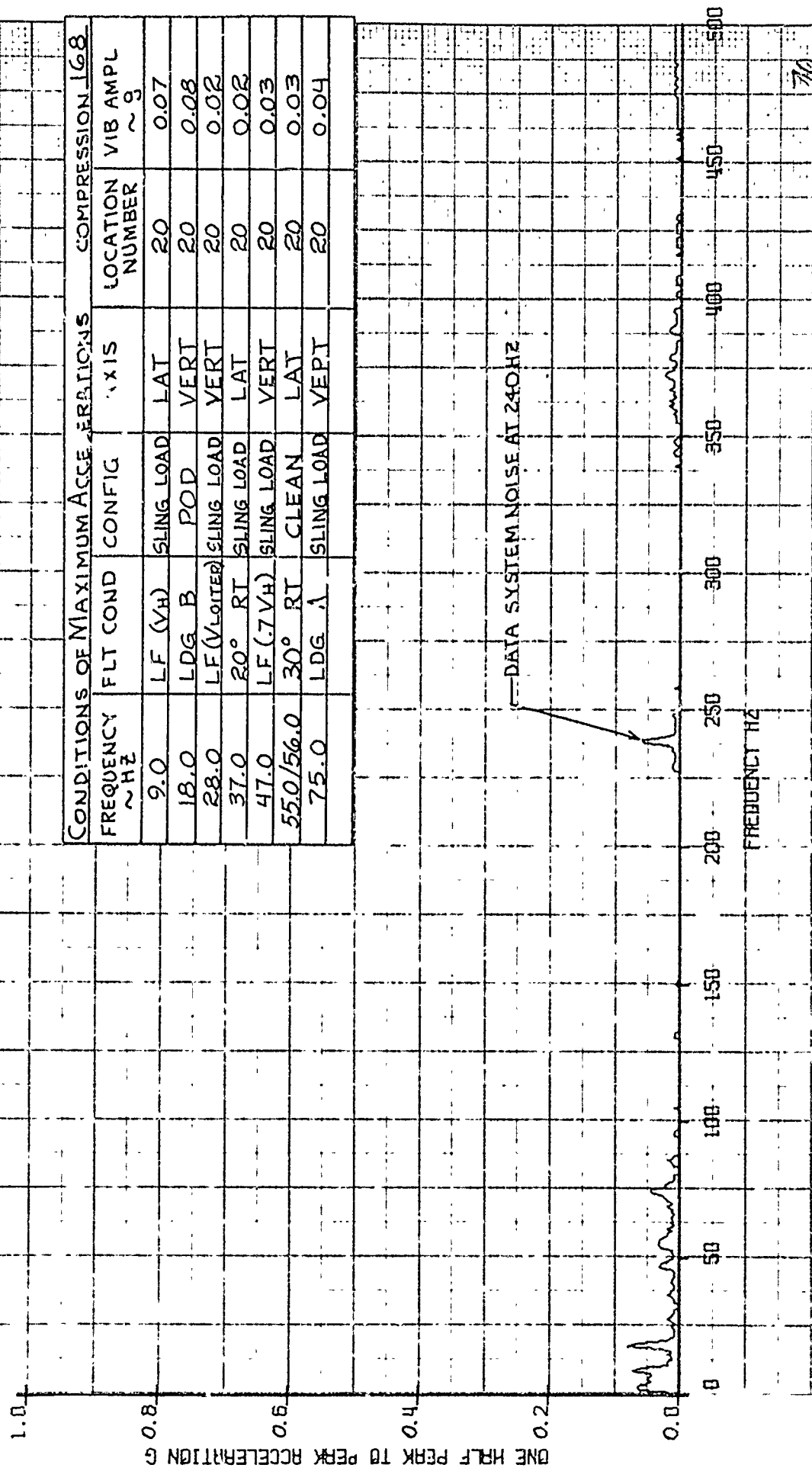


FIG 13

## COMPRESSED VIBRATION DATA

CH-54B USA S/N 69-18463  
 GROSS WT 28400 AND 41900LB AVG CG STA-MID CONFIG-CLEAN/P00/SLING  
 COMBINED FLT CONDS HUMAN FACTORS OUTPUT COMBINED AXIS Y18 PLOT 168  
 SENSOR LOC 20,21 COMPRESSION PASS NO12

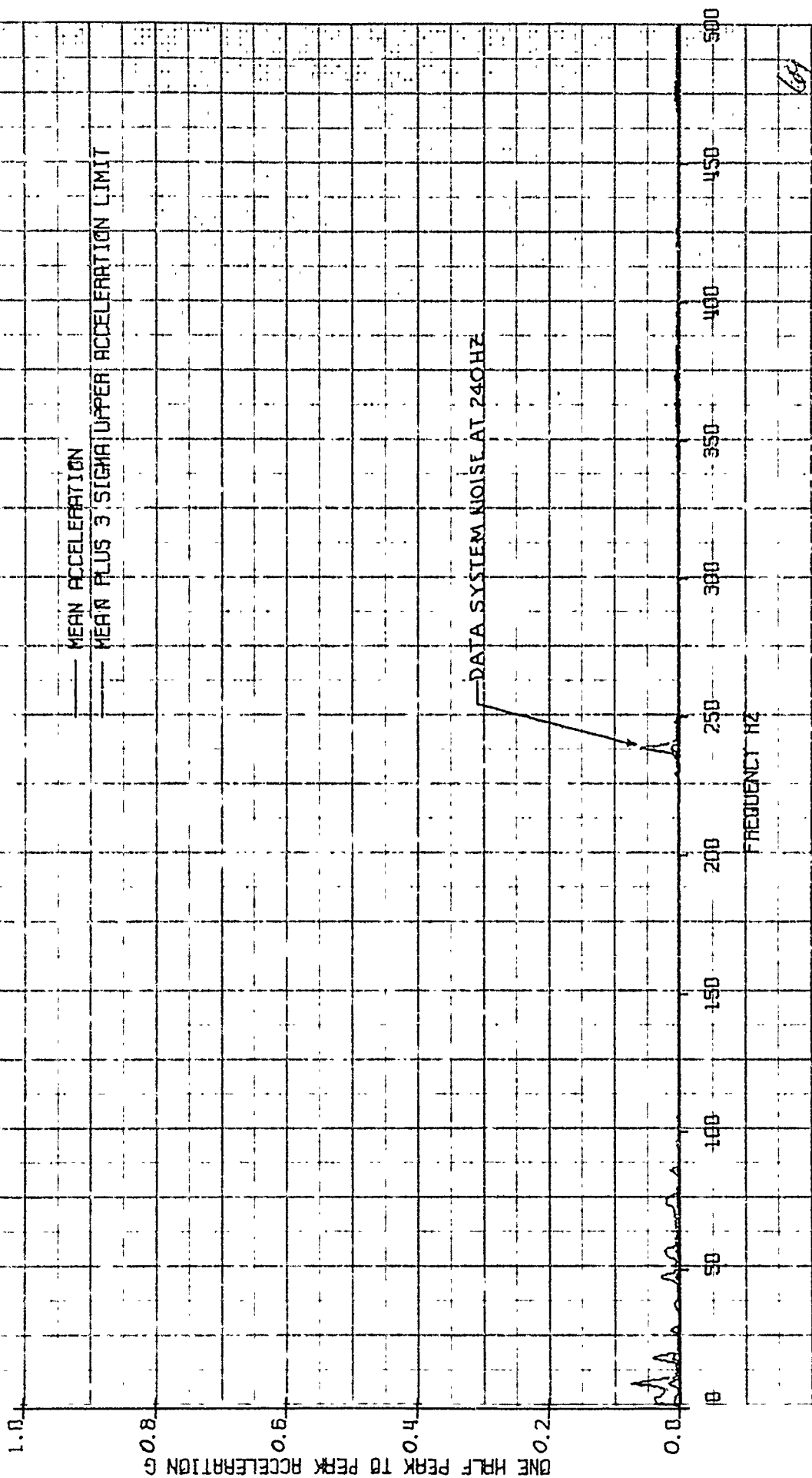


FIG 14

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH 546 USA S/N 59-18463  
 GROSS HT 28400 AND 41300018 AVG EG STR MID CONE LG CLEAN/POD/SLING  
 COMBINED FLT CONDS TACH GENERATORS COMBINED AXIS VIB PLOT 169  
 SENSOR LOT 22-23-24 COMPRESSION PRESS MD-2

CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION 169
FREQUENCY ~ HZ	FLT COND	CONFIG	AXIS	LOCATION NUMBER	VIB AMPL ~ g
120.0	LF (.8VH)	CLEAN	VERT	22	7.51
180.0	LF (.8VH)	CLEAN	VERT	22	8.88
220.0	LF (.8VH)	CLEAN	VERT	24	10.82
256.0	VBEST R/C	POD	LAT	24	16.30
1372.0	10° LT	SLING LOAD	LONG	22	9.04
1780.0	T/O	SLING LOAD	LONG	22	13.03
1796.0	OGE	SLING LOAD	LONG	22	13.32
1908.0	T/O	POD	VERT	22	82.43
1928.0	T/O	SLING LOAD	LONG	22	109.59
1944.0	OGE	SLING LOAD	LONG	22	88.64

ONE HALF PEAK TO PEAK ACCELERATION G

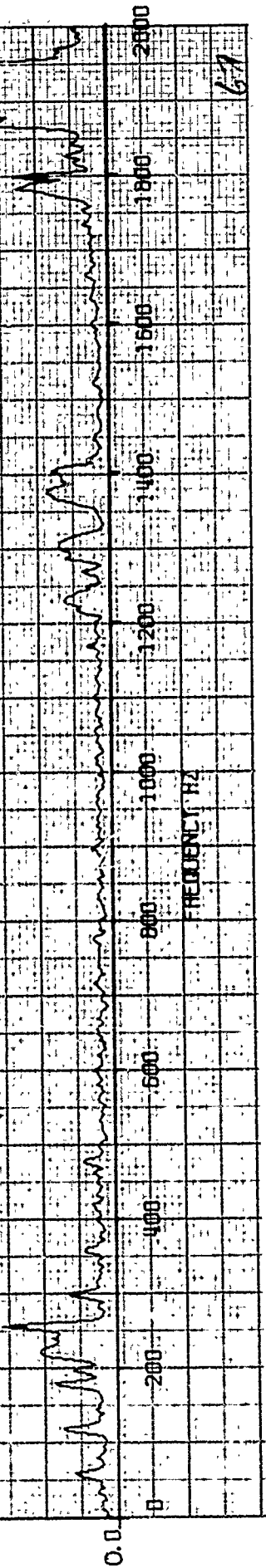


FIG. 115

COMPRESSED VIBRATION DATA

GN-548: USA 54N 68-18463  
 GROSS MT 28400 AND 41900 LB AVG CG STR-M10 CONF-G-DEEN/700/S-ING  
 COMBINED F-T CO-OS TRUCK GENERATORS COMBINED AXIS V18 PLAT 168  
 SENSOR LOC 21-23-21 COMPRESSION PRESS NO. 2

MEAN ACCELERATION

MEAN RMS 3 SIGMA UPPER ACCELERATION LIMIT

ONE HALF PEAK TO PEAK ACCELERATION G

100

80

60

40

20

0.0

0 200 400 600 800 1000 1200 1400 1600 1800 2000

FREQUENCY Hz

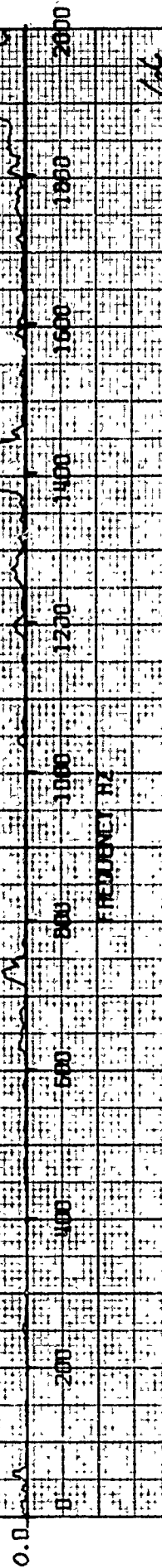
FIG 16

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH-548 USB S/N 59-18463  
 GP555 HT 28000 RPM V1900LB AVG CG STR-M10 CONFIG CLEAN/POD/SLING  
 COMBINED FLT COND TRANS MOUNTS COMBINED AXIS VIB PLOT 170  
 SENSOR LOT 25-26-27-28 COMPRESSION PRESS NO.2

CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION 170
FREQUENCY ~HZ	FLT COND	CONFIG	AXIS	LOCATION NUMBER	VIB AMPL ~g
1396.0	QGE	POD	VERT	25	7.42
1920.0	T/O	SLING LOAD	LONG	25	38.02
1968.0	LDG A	SLING LOAD	LONG	28	6.71

ONE HALF PEAK TO PEAK ACCELERATION G





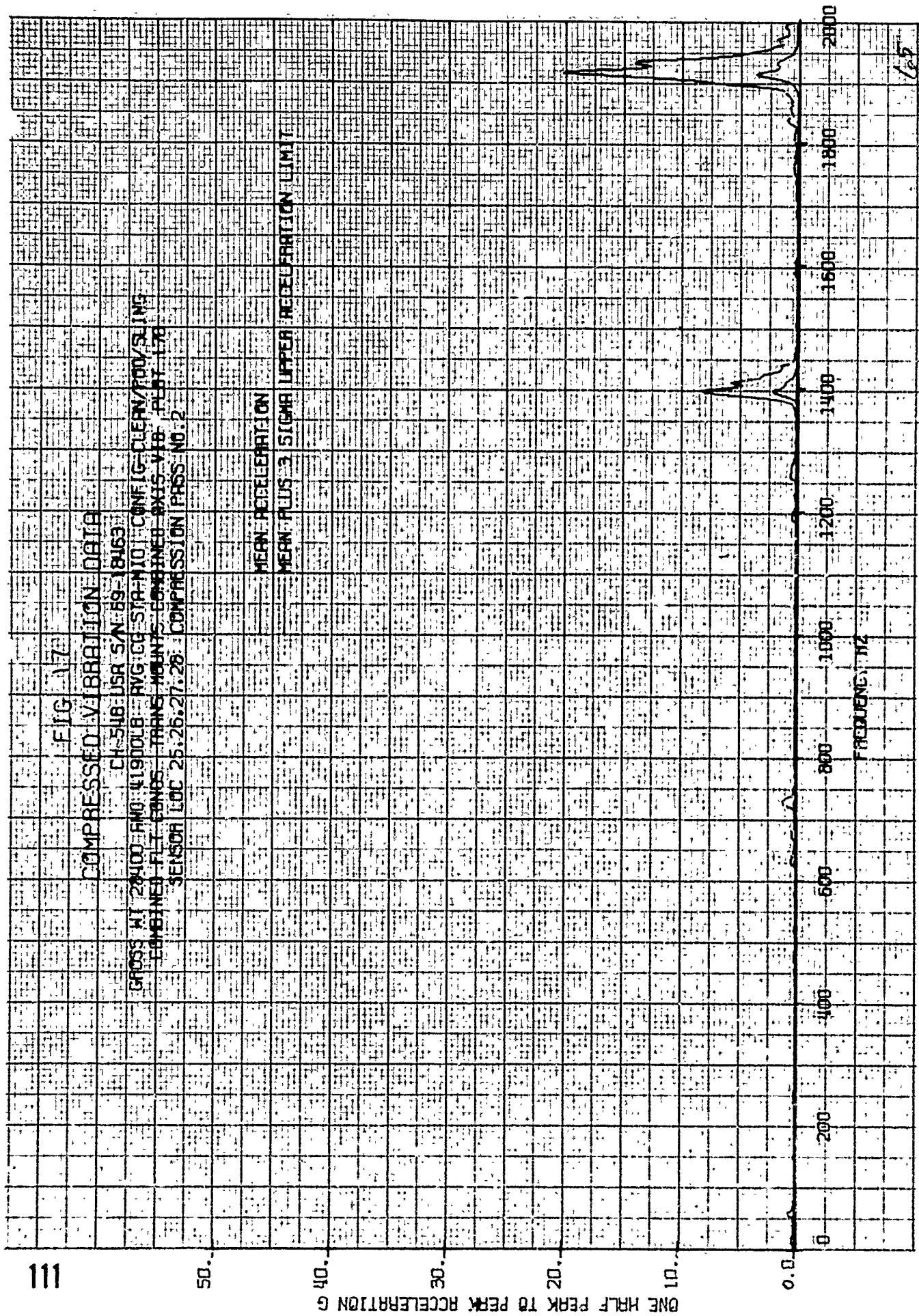


FIG 18

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH-54B USA 5A 5N 89 18463  
 CROSS WT 20400 AND 41900 LB AVG CG STA M10 CONFIG CLEAN/POD/SLING  
 COMBINED FLT BANDS UPPER-MN TRANS COMBINED AXIS VIB PLG 7-17  
 SENSIT LOC 29 COMPRESSION PRESS NO 22

CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION 171	
FREQUENCY ~ HZ	FLT COND	CONFIG	AXIS	LOCATION NUMBER	VIB AMPL ~ g	
1264.0	IGE	CLEAN	LAT	29	3.43	
1396.0	VGRUPE R/C	POD	LONG	29	12.58	
1916.0	T/O	POD	LONG	29	30.62	
1932.0	T/O	SLING LOAD	LONG	29	18.55	
1944.0	OGE	SLING LOAD	LONG	29	17.44	

ONE HALF PEAK TO PEAK ACCELERATION G

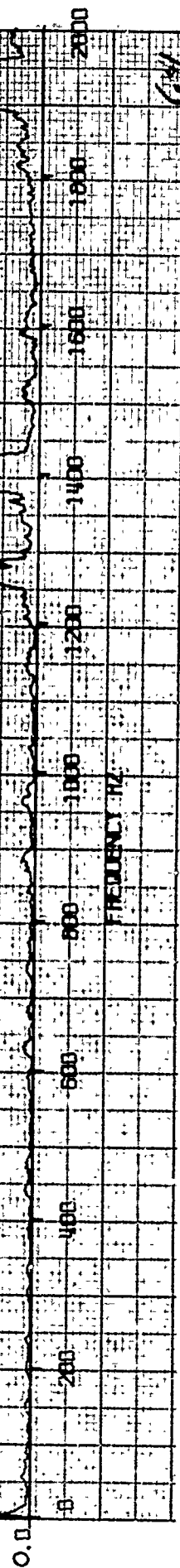


FIG 19

## COMPRESSED VIBRATION DATA

CH-54B USA S/N: 69-18463  
GROSS WT 28400 AND 41900LB AVG CG STA-M10 CONFIG-CLEAN/POD/SLING  
COMBINED FLT COMBS UPPER-MN TRANS COMBINED AXIS #18 PLAT 1-1  
SENSOR LOC 28 COMPRESSION PRESS NO.2

— MEAN ACCELERATION  
— MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

50

40

30

20

10

0.0

ONE HALF PEAK TO PEAK ACCELERATION G

0 200 400 600 800 1000 1200 1400 1600 1800 2000

FREQUENCY HZ

63

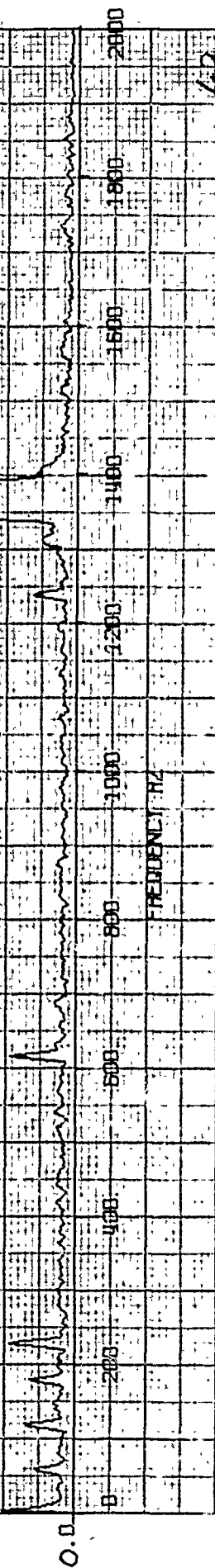


FIG. 20

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH-54B USA S/N 89-18163  
 GROSS WT 28400 AND 41900LB. AVG CG STA-M10. CONFIG-CLEAN/POD/SLING  
 COMBINED FLT EDMS 45-AND-9886G-88-COMBINED AXES-VIB-REPT-172  
 SENSOR LOC 30:31 COMPRESSION PASS NO. 2

CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION
FREQUENCY ~ HZ	FLT COND	CONFIG	AXIS	LOCATION NUMBER	VIB AMPL ~ g
60.0	LF (.8VH)	CLEAN	VERT	30	2.80
120.0	LF (.8VH)	CLEAN	VERT	30	3.57
180.0	LF (.8VH)	CLEAN	VERT	30	3.17
228.0	10° RT	SLING LOAD	VERT	31	4.68
616.0	GND IDLE	GND RUN	VERT	31	4.72
1236.0	GND IDLE	GND RUN	LONG	31	3.13
1368.0	25° LT	POD	LONG	31	33.74
1384.0	OGE	SLING LOAD	LAT	31	20.93



115

FIG. 21

COMPRESSED VIBRATION DATA

CH-518 USA 57N 69-18463  
 GROSS WT 28400 LBS: 41900 LB: AVG CG STA-M10 CONF G-CLEAN/100/S/LING  
 COMBINED FLT CONDS HS-HW 908EG-08-COMBINED-RX15-VIB PEST-172  
 SENSOR LOC 50.31 COMPRESSION-PASS NO. 2

50

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

40

30

20

10

0.0

ONE HALF PEAK TO PEAK ACCELERATION G

0

200

400

600

800

1000

1200

1400

1600

1800

2000

FREQUENCY HZ

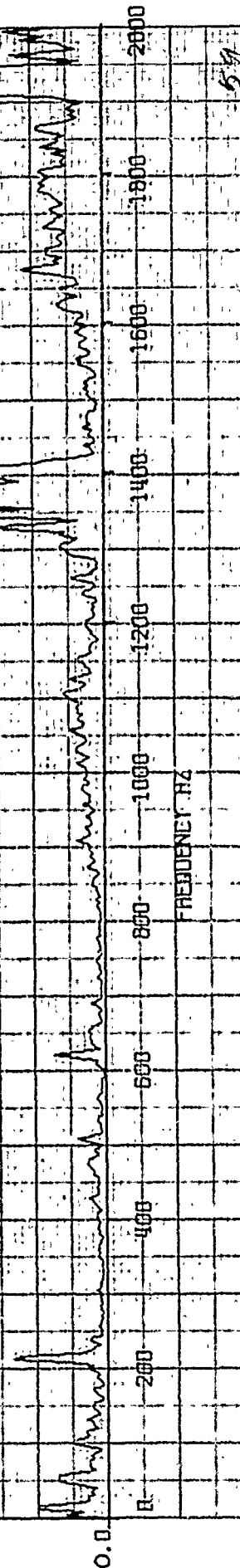
61

FIG 22

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH-54B USA S/N 59-18463  
 GROSS WT 28400 AND 41800LB AVG CS STR-MID CONF (G-CLEAN/POD/SLING  
 COMBINED FLT ENDS TAIL ROT SHFT HBR PASS-COMBINED AXIS VIB PLOT 173  
 SENSOR LOC 132 33 34 35 36 COMPRESSION PASS NO.2

CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION
FREQUENCY ~HZ	FLT COND	CONFIG	AXIS	LOCATION NUMBER	VIB AMPL ~g
16.0	20° LT	SLING LOAD	VERT	36	2.00
212.0	LDG B	POD	VERT	33	2.70
1328.0	25° RT	POD	VERT	36	3.10
1344.0	VERUISE R/C	POD	VERT	36	4.72
1364.0	LF (9VH)	POD	LAT	36	5.14
1404.0	OGE	SLING LOAD	LAT	36	4.01
1672.0	LDG B	POD	VERT	33	2.32
1912.0	LDG B	POD	VERT	34	8.28
1928.0	OGE	SLING LOAD	LAT	36	22.36
1940.0	OGE	SLING LOAD	VERT	32	6.46



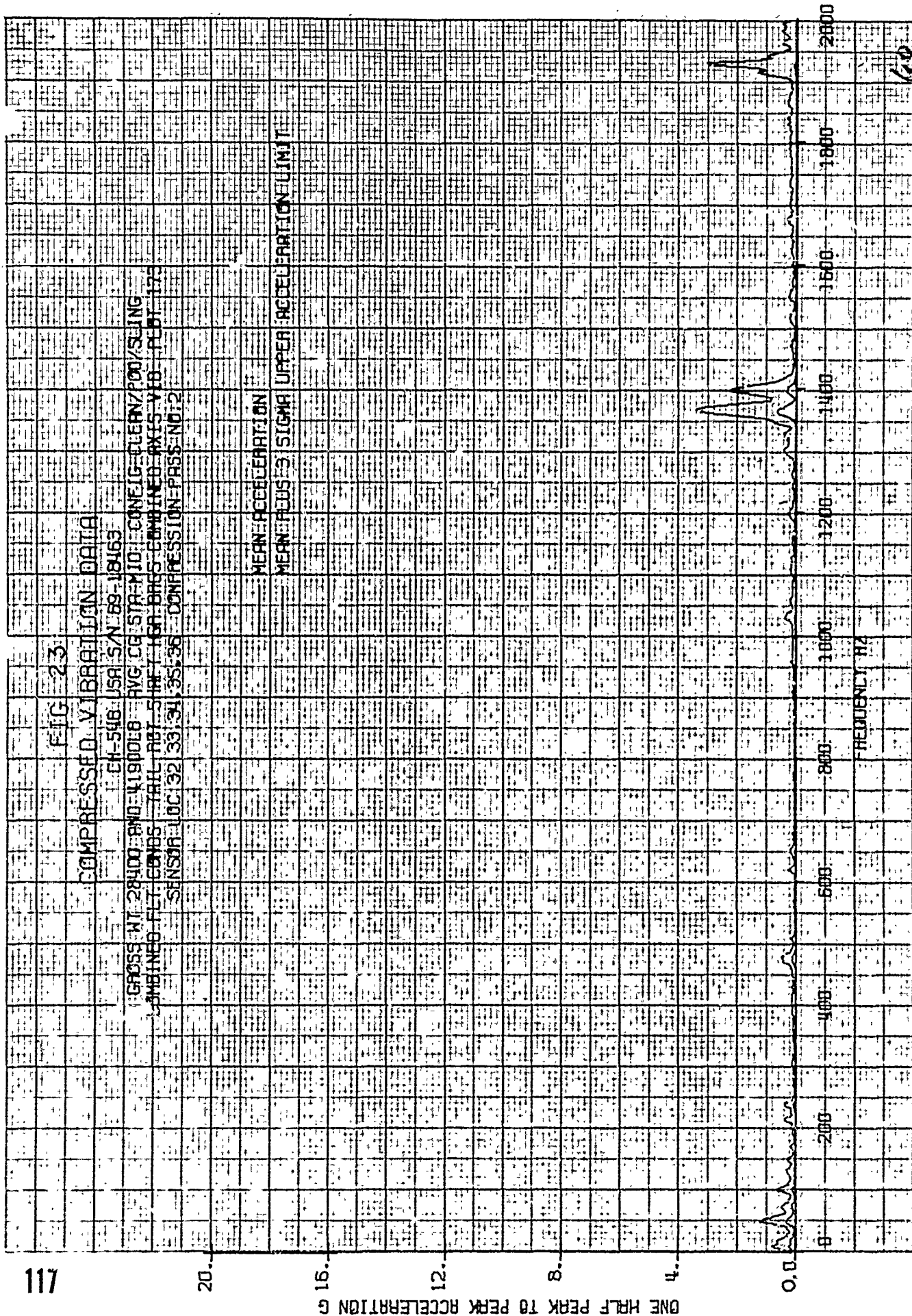


FIG 24

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH-54B USA S/N 69-18463  
 GROSS WT 28000 AND 11900LB. AVG CG STA-M10. CONFIG-CLEAR/P007/SLING  
 COMBINED FLT COND. HYDRAULIC SYS COMBINED AXIS VIB PLOT 174  
 SENSOR LOC 37.38/39.40, 41.55. COMPRESSION PRESS. NO. 2

CONDITIONS OF MAXIMUM ACCELERATIONS			COMPRESSION 174	
FREQUENCY ~ HZ	FLT COND	CONFIG	AXIS	LOCATION VIB AMPL NUMBER ~ g
20.0	OGE	SLING LOAD	LAT	37 10.01
576.0	LDG A	SLING LOAD	LONG	41 9.93
1372.0	VCruise R/C	POD	LAT	38 14.40
1404.0	10° RT	SLING LOAD	LAT	37 23.39
1416.0	LDG A	POD	LAT	38 11.37
1724.0	OGE	SLING LOAD	LAT	38 41.62
1740.0	LDG A	SLING LOAD	LAT	38 29.04
1904.0	IGE	POD	VERT	37 59.50
1928.0	OGE	SLING LOAD	VERT	37 46.38
1940.0	VCruise R/C	POD	VERT	37 34.21
1960.0	VCruise R/C	POD	LONG	37 12.11

ONE HALF PEAK TO PEAK ACCELERATION G

10.

20.

30.

40.

50.

0.0

B

200

400

600

800

1000

1200

1400

1600

1800

2000

FREQUENCY HZ

52



119

FIG. 25

# COMPRESSED VIBRATION DATA

CH-548 USA S/N: 69-18463  
 GROSS WT 28400 LBS AVG CG STA: 110' CONFIG: CLEAN/COMPRESSING  
 COMBINED FLT: 60406 HYDRAULIC SYS COMBINED AXIS: Y18: PLOT 121  
 SENSOR LOC: 37.38.39.40.41.55 COMPRESSION PASS: NO. 2

50.

40.

30.

20.

10.

0.0

ONE HALF PEAK TO PEAK ACCELERATION G

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

200

400

600

800

1000

1200

1400

1600

1800

2000

FREQUENCY Hz

57

120

200.

ONE HALF PEAK TO PEAK ACCELERATION

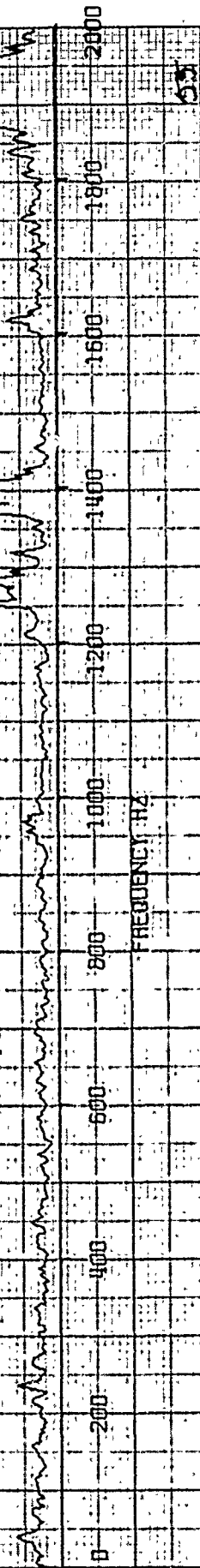
0.0

FIG. 26

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH-548 USA S/N 69-18463  
 GROSS WT 28400 AND 41900LB AVG CG STA-M10 CONFIG-CLEAN/POD/SLING  
 COMBINED FLT CONDS OIL COOLER SUPPORT COMBINED AXIS-VIB PLOT 175  
 SENSOR LOC 42.45 COMPRESSION PASS NO.2

CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION 175
FREQUENCY ~ HZ	FLT COND	CONFIG	AXIS	LOCATION NUMBER	VIB AMPL ~ g
1252.0	VCRUISE R/C	CLEAN	LONG	43	20.56
1276.0	VCRUISE R/C	CLEAN	LONG	43	23.29
1372.0	VCRUISE R/C	POD	LONG	43	38.81
1388.0	VCRUISE R/C	CLEAN	LONG	43	35.57
1880.0	VCRUISE R/C	POD	LONG	43	146.12
1900.0	VCRUISE R/C	CLEAN	LONG	43	187.03
1908.0	T/O	CLEAN	LONG	43	126.08
1916.0	OGE	CLEAN	LONG	43	126.35
1928.0	VBEST R/C	POD	LONG	43	193.80
1952.0	VCRUISE R/C	POD	LAT	42	43.27



53

FIG. 27

## COMPRESSED VIBRATION DATA

CH-546 USA SN 69-18463  
GROSS WT 28400 AND 41900LB AVG CG STA-N101 CONF IG-CLEAN/POD/SLING  
COMBINED FLT CONDS. OIL COOLER SUPPORT COMBINED AXES V10 PLOT 175  
SENSOR LOC 42.43 COMPRESSION PRESS NO. 2

200.

160.

120.

80.

40.

0.0

ONE HALF PEAK TO PEAK ACCELERATION G

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

FREQUENCY HZ

2000

1800

1600

1400

1200

1000

800

600

400

200

0

50



FIG 28

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH 548 USA S/N 59-18463  
 GROSS WT 28400 AND 41900LB AVG CG STR MID CONFIG-CLEAN/POD/SLING  
 COMBINED FLT COND APPRNG ENG FUEL PRESS S/G COMBINED AXIS VIB PLT 176  
 SENSOR LOC 44-45 COMPRESSION PRESS NO 2

CONDITIONS OF MAXIMUM ACCELERATIONS				COMPRESSION 176	
FREQUENCY ~ HZ	FLT COND	CONFIG	AXIS	LOCATION NUMBER	VIB AMPL ~ g
56.0	20° LT	SLING LOAD	LAT	44	1.37
76.0	LDG B	POD	VERT	44	1.03
112.0	LDG B	POD	VERT	44	0.84
200.0	OGE	POD	LAT	45	2.19
656.0	LDG A	SLING LOAD	VERT	44	0.99
964.0	FLT IDLE	GND RUN	LONG	44	3.19
1360.0	FLT IDLE	GND RUN	LONG	44	1.81
1408.0	OGE	SLING LOAD	LONG	44	1.37
1680.0	FLT IDLE	GND RUN	LONG	44	1.31
1916.0	T/O	POD	LONG	44	0.91

ONE HALF PEAK TO PEAK ACCELERATION G

5.0

4.0

3.0

2.0

1.0

0.0

0 200 400 600 800 1000 1200 1400 1600 1800 2000 2200

FREQUENCY HZ

34

FIG 29

## COMPRESSED VIBRATION DATA

CH-546 USA S/N 69-18463  
GROSS WT 28400 LBS AVG CG STA-MID CONFIG-TIERN/POD/SLING  
COMBINED FLT CONDS APP AND ENG-FUEL PRESS SWS COMBINED AXIS VIB PLOT 1.76  
SENSOR LOC 44.45 COMPRESSION PASS NO.2

5.0

4.0

3.0

2.0

1.0

0.0

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

ONE HALF PEAK TO PEAK ACCELERATION G

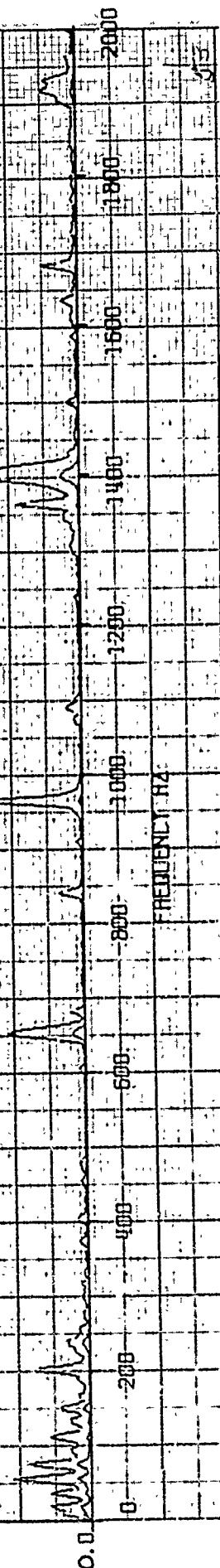


FIG. 30

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH-548 USA S/N 69-18463  
 GROSS WT 28400 AND V190018 AVG CG STA-M10 CONFIG CLEAN/POD/SLING  
 COMBINED FLT CONDS BRAKE CYL COMBINED AXIS V18 PLOT 177  
 SENSOR LOC 46 COMPRESSION PASS NO. 2

CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION 177	
FREQUENCY ~ Hz	FLT COND	CONFIG	AXIS	LOCATION NUMBER	VIB AMPL ~ g	
19.0	LDG A	POD	LONG	46	0.28	
57.0	T/O	CLEAN	LAT	46	0.12	
76.0	VCRUISE R/C	POD	LAT	46	0.23	
93.0	LDG A	CLEAN	LAT	46	0.13	
130.0	LDG A	CLEAN	LAT	46	0.15	
226.0	VCRUISE R/C	POD	LONG	46	0.36	

ONE HALF PEAK TO PEAK ACCELERATION G

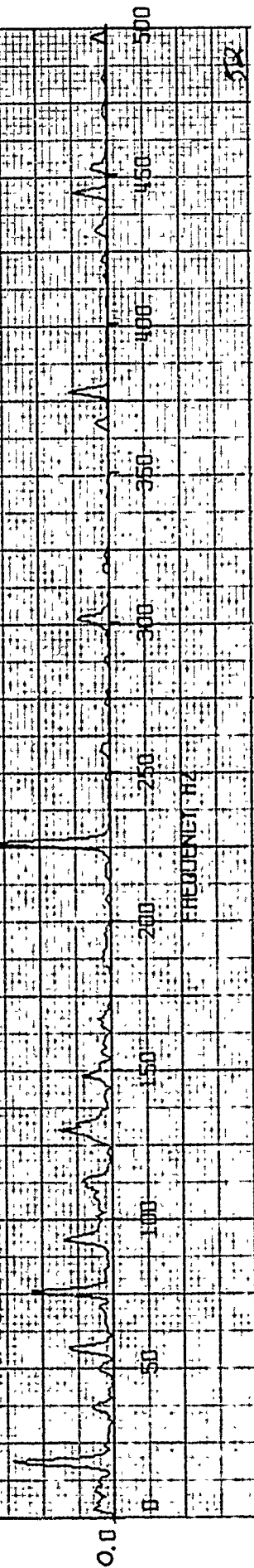


FIG. 31

## COMPRESSED VIBRATION DATA

CROSS AT 28400 AND 41900LB AVG CG STA-N10, CONFIG-CLEAN/P00/SLING  
COMBINED FLT-ENRGS BRKLE CYL COMBINED AXIS-VIB PLAT-177  
SENSOR-LMC-46 COMPRESSION PASS NO.2

2.0

1.6

1.2

0.8

0.4

0.0

MEAN ACCELERATION  
MEAN PEAK-3 SIGMA UPPER RECELERATION LIMIT

250

300

350

400

450

500

200

250

300

350

400

450

500

550

600

650

700

750

800

850

900

950

1000

1050

1100

1150

1200

1250

1300

1350

1400

1450

1500

1550

1600

1650

1700

1750

1800

1850

1900

1950

2000

2050

2100

2150

2200

2250

2300

2350

2400

2450

2500

2550

2600

2650

2700

2750

2800

2850

2900

2950

3000

3050

3100

3150

3200

3250

3300

3350

3400

3450

3500

3550

3600

3650

3700

3750

3800

3850

3900

3950

4000

4050

4100

4150

4200

4250

4300

4350

4400

4450

4500

4550

4600

4650

4700

4750

4800

4850

4900

4950

5000

5050

5100

5150

5200

5250

5300

5350

5400

5450

5500

5550

5600

5650

5700

5750

5800

5850

5900

5950

6000

6050

6100

6150

6200

6250

6300

6350

6400

6450

6500

6550

6600

6650

6700

6750

6800

6850

6900

6950

7000

7050

7100

7150

7200

7250

7300

7350

7400

7450

7500

7550

7600

7650

7700

7750

7800

7850

7900

7950

8000

8050

8100

8150

8200

8250

8300

8350

8400

8450

8500

8550

8600

8650

8700

8750

8800

8850

8900

8950

9000

9050

9100

9150

9200

9250

9300

9350

9400

9450

9500

9550

9600

9650

9700

9750

9800

9850

9900

9950

10000

10050

10100

10150

10200

10250

10300

10350

10400

10450

10500

10550

10600

10650

10700

10750

10800

10850

10900

10950

11000

11050

11100

11150

11200

11250

11300

11350

11400

11450

11500

11550

11600

11650

11700

11750

11800

11850

11900

11950

12000

12050

12100

12150

12200

12250

12300

12350

12400

12450

12500

12550

12600

12650

12700

12750

12800

12850

12900

12950

13000

13050

13100

13150

13200

13250

13300

13350

13400

13450

13500

13550

13600

13650

13700

13750

13800

13850

13900

13950

14000

14050

14100

14150

14200

14250

14300

14350

14400

14450

14500

14550

14600

14650

14700

14750

14800

14850

14900

14950

15000

15050

15100

15150

15200

15250

15300

15350

15400

15450

15500

15550

15600

15650

15700

15750

15800

15850

15900

15950

16000

16050

16100

16150

16200

16250

16300

16350

16400

16450

16500

16550

16600

16650

16700

16750



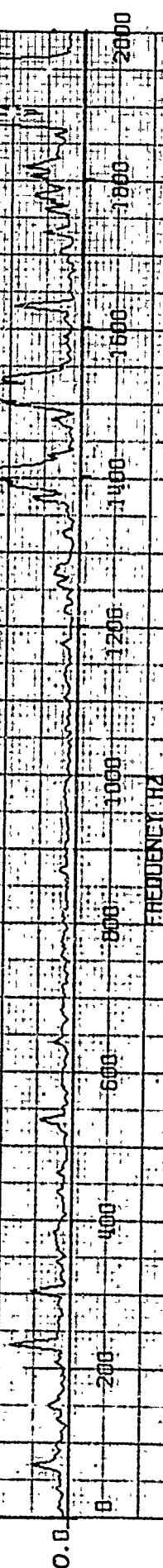
FIG 32

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

GROSS WT 28400 LBS VIBRATOR S/N 89-18463  
 COMBINED FLT COND AVG LG STAFF IDT CONF LG CLEAN/POD/SLING  
 COMBINED FLT COND ROTER BRAKE SUPPORT COMBINED AXIS VIB PLT 178  
 SENSOR LOC 47 COMPRESSION PRESS NO. 2

CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION 178
FREQUENCY ~ HZ	FLT COND	CONFIG	AXIS	LOCATION NUMBER	VIB AMPL ~ g
232.0	VERUISE R/C	SLING LOAD	LONG	47	4.27
1408.0	OGE	SLING LOAD	LAT	47	8.08
1504.0	GND IDLE	GND RUN	LONG	47	8.37
1520.0	GND IDLE	GND RUN	LAT	47	10.81
1628.0	VERUISE R/C	SLING LOAD	LONG	47	4.88
1880.0	VERUISE R/C	POD	LAT	47	16.85
1912.0	OGE	POD	LONG	47	32.79
1936.0	T/O	SLING LOAD	LONG	47	20.44
1956.0	LDG A	SLING LOAD	LONG	47	17.56

ONE HALF PEAK TO PEAK ACCELERATION G



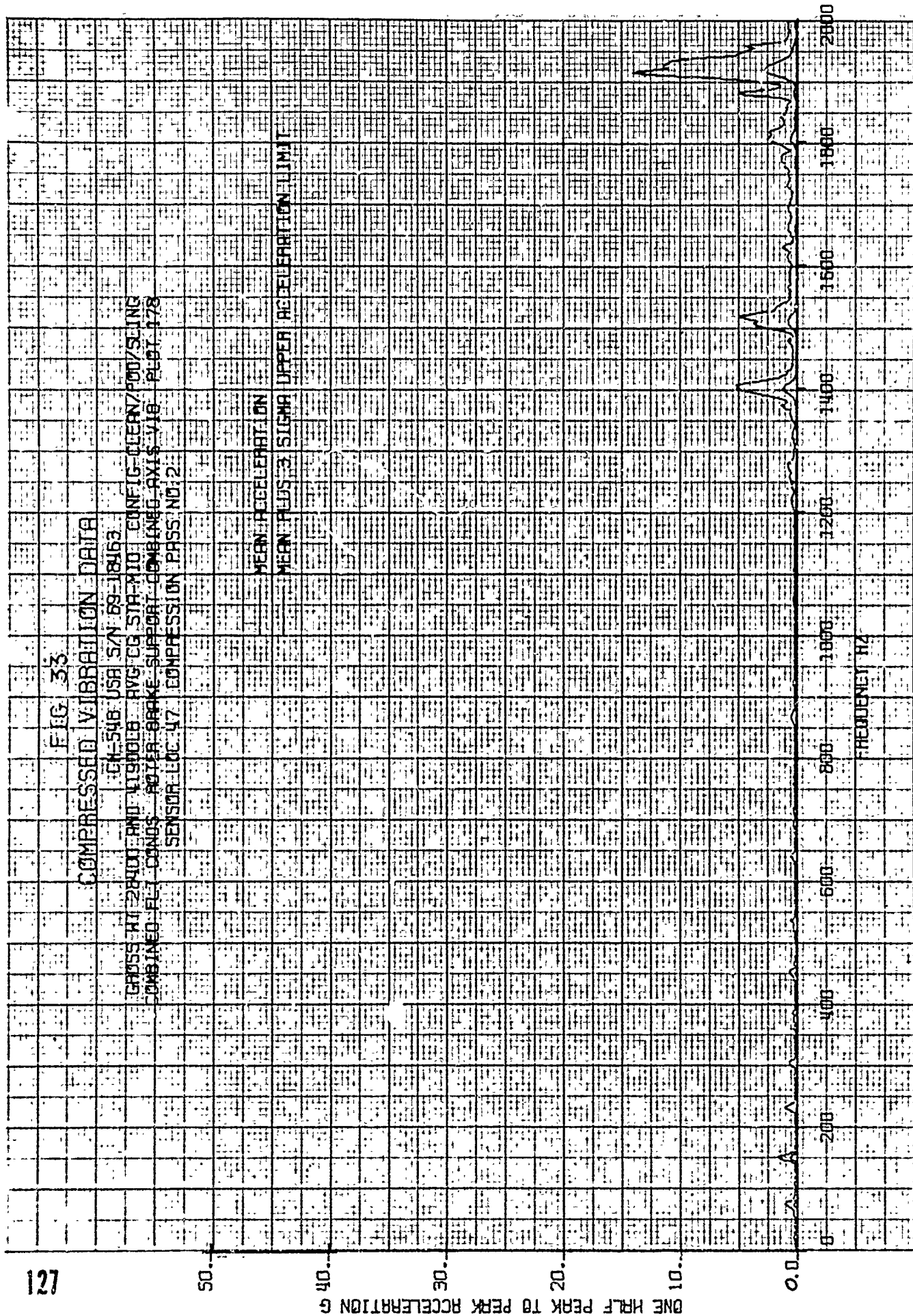


FIG 34

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH-518 USA S/N 69-18463  
 GROSS WT 28400 LBS. AVG CG STR-N101 CONFIG-CLEAN/POD/SLING  
 COMBINED FLT COND. SKEWED-BLOWER, COMBINED AXIS VIB. PLT 179  
 SENSOR LOC 49 COMPRESS-PASS NO. 2

2.0

1.6

1.2

0.8

0.4

0.0

ONE HALF PERK TO PERK ACCELERATION G

CONDITIONS OF MAXIMUM ACCELERATIONS				COMPRESSION 179	
FREQUENCY ~ HZ	FLT COND	CONFIG	AXIS	LOCATION NUMBER	VIB AMPL ~ g
19.0	LDG B	CLEAN	VERT	49	0.23
95.0	OGE	POD	LONG	49	0.33
100.0	OGE	CLEAN	VERT	49	1.00
104.0	LF (VLOITER)	POD	VERT	49	0.79
109.0	VCRUISE R/D	POD	VERT	49	0.68
481.0	LF (.7 Vh)	POD	VERT	49	0.81
490.0	LF (.7 Vh)	POD	VERT	49	0.23

DATA SYSTEM NOISE AT 240 HZ

0.0

50

100

150

200

250

300

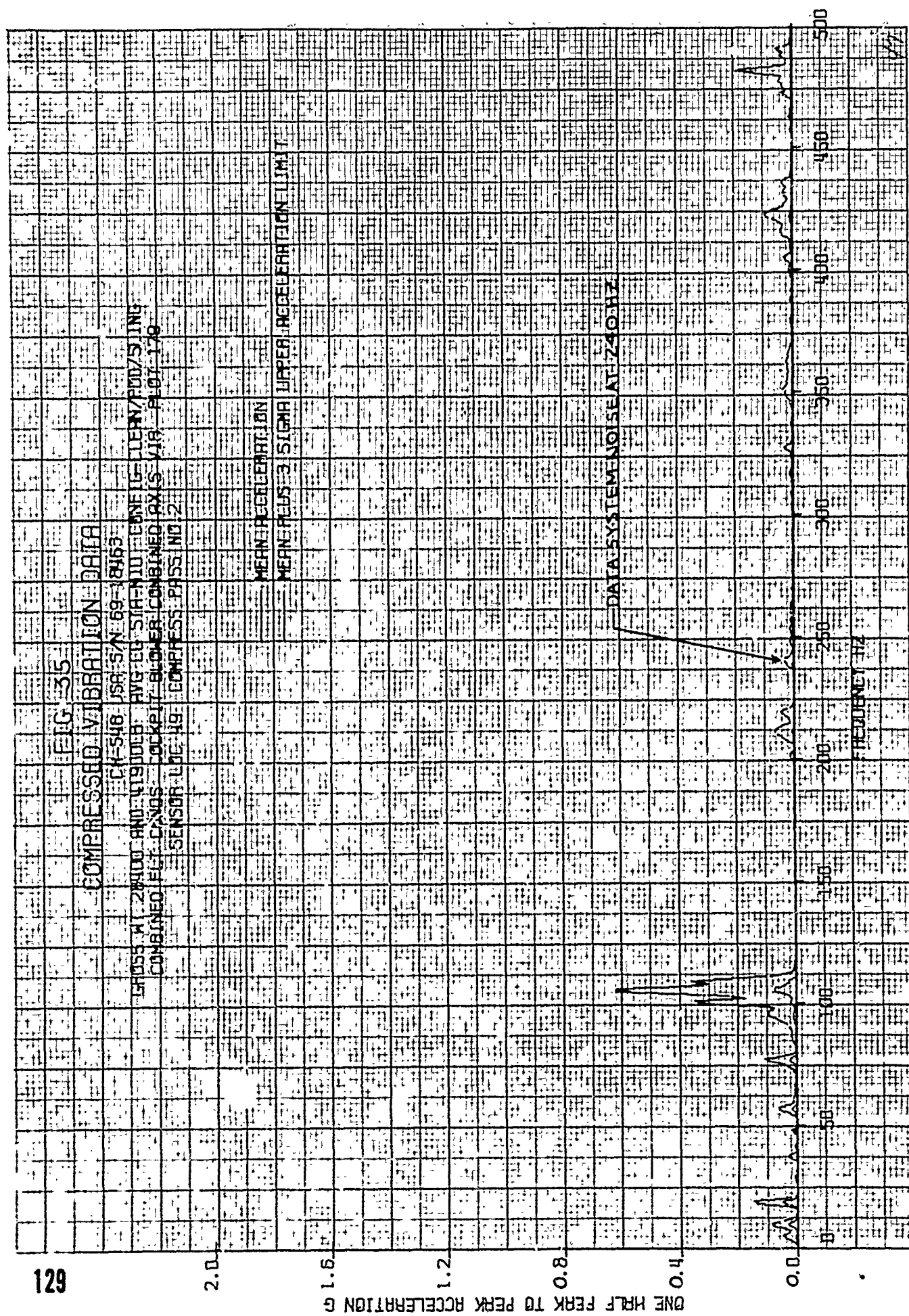
350

400

450

500

FREQUENCY HZ





130

20.

16.

12.

8.

4.

0.0

ONE HALF PEAK TO PEAK ACCELERATION G

## COMPRESSION VIBRATION DATA MAXIMUM ACCELERATION

GROSS WT 28400 RND 41900LB AVG CG STA 110' CONFIG=CLEAN/POD/SLING  
ENGINEER FLT EMBLS HBRIZ STABILIZER ENGINEER AXIS VIB PLGT 188  
SENSOR LOC 50' COMPRESSION PASS NO 2

## CONDITIONS OF MAXIMUM ACCELERATIONS

FREQUENCY ~ HZ	FLT COND	CONFIG	AXIS	LOCATION NUMBER	COMPRESSION VIB AMPL ~ 8
56.0	15° LT	POD	VERT	50	7.61
112.0	OGE	POD	VERT	50	6.05
168.0	VCRUISER/C	POD	VERT	50	11.20
224.0	VCRUISER/C	POD	LAT	50	4.05
256.0	LDG B	POD	LONG	50	4.34
344.0	VCRUISER/C	SLING LOAD	LAT	50	5.58
364.0	VCRUISER/C	SLING LOAD	LAT	50	4.43
392.0	VCRUISER/C	POD	LONG	50	8.17

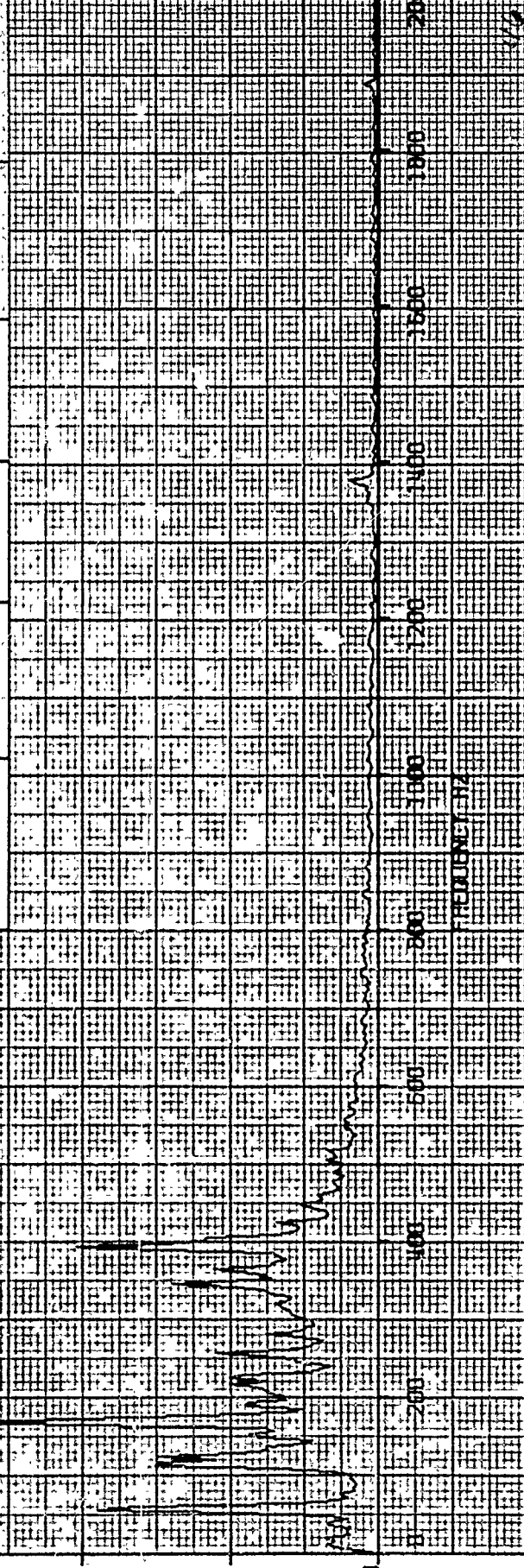


FIG 37

## COMPRESSED VIBRATION DATA

GROSS WT 28400 RWD #190018 AVG CG STA-HIQ CONFIG-CLEAN/POD/SLING  
COMBINED ACT COMB5 H0112 SEATTLE/SEA COMBINED AXIS VIB PL07 186  
SENSOR LOC 50 COMPRESSION PASS NO 2

20.

16.

12.

8.

4.

0.0

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

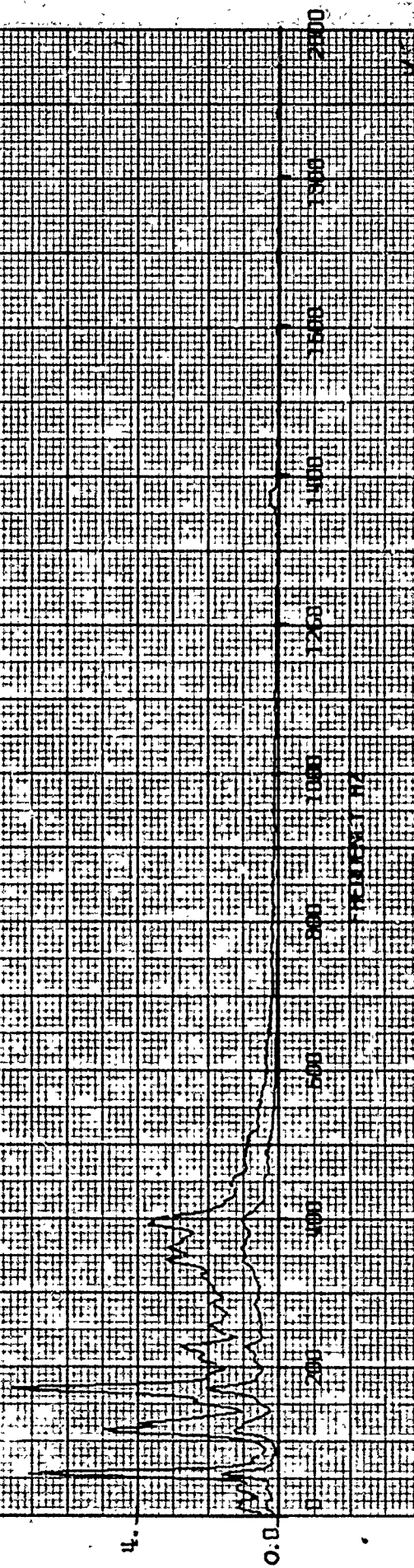


FIG 38

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH-518 USA SN 89-18463  
 GROSS M (2000) AND USQUEB AVG CG STATION CONFIG-JERK/POD/SLING  
 COMBINED LF COND. INT. COLLISION LIGHT COMBINED AXIS VIB PLT 183  
 SENSOR LOC 51 COMPRESSION PASS NO 2

5.0

ONE HALF PEAK TO PEAK ACCELERATION G

4.0

3.0

2.0

1.0

0.0

CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION 181	
FREQUENCY ~HZ	FLT COND	CONFIG	AXIS	LOCATION NUMBER	VIB AMPL ~g	
14.0	LF (7VH)	POD	VERT	51	1.08	
22.0	LF (7VH)	POD	VERT	51	0.77	
38.0	T/O	SLING LOAD	LONG	51	0.69	
41.0	LF (7VH)	POD	VERT	51	0.63	
53.0	LF (7VH)	POD	VERT	51	0.36	

FREQUENCY HZ

200

250

300

350

400

450

500



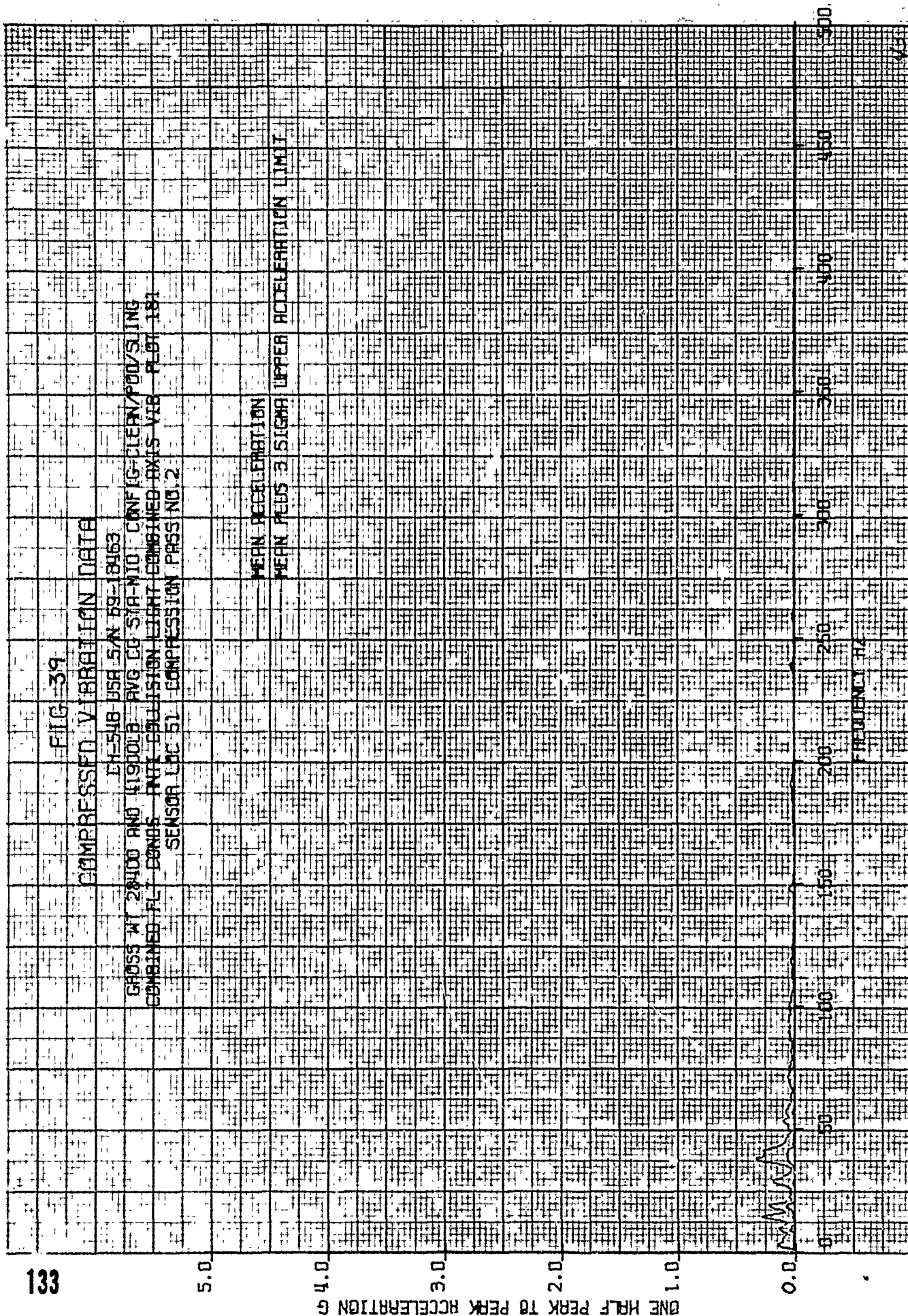


FIG 40

COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH-51B USA 5/N 59-194333  
 CROSS AT 28400 RND 4190018 AVG CG 57A-M10, CONFIG-CLEN/P00/SLING  
 KEINER-FL-2000S-PAI-SERVO-RETURNERS-COMBINED-AXIS-VIB-PLAT 182  
 SENSOR LDC-52-53 COMPRESSION PASS NO 2

CONDITIONS OF MAXIMUM ACCELERATIONS				COMPRESSION 182
FREQUENCY ~ HZ	FLT COND	CONFIG	AXIS	LOCATION NUMBER
1372.0	VCRUISE/R/C	POD	VERT	53
1404.0	10° RT	SLING LOAD	LAT	53
1880.0	VCRUISE/R/C	POD	LAT	53
1912.0	OGE	POD	VERT	52
1928.0	OGE	SLING LOAD	VERT	52

VIB AMPL  
~ 9  
4.23  
6.70  
9.37  
15.47  
16.49

ONE HALF PEAK TO PEAK ACCELERATION G



FIG. 41

## COMPRESSED VIBRATION DATA

CH-548 USA S/N: 69-19133  
 GROSS WT: 28400 LBS AVG CG STA: MID CONFIG: CLEAN/POD/SLING  
 COMBINED FLT CONDS: P1, SERVO, ACTUATORS, COMBINED, AXIS V18, PLOT 182  
 SENSOR LOC: 52, 53, COMPRESSION PASS NO. 2

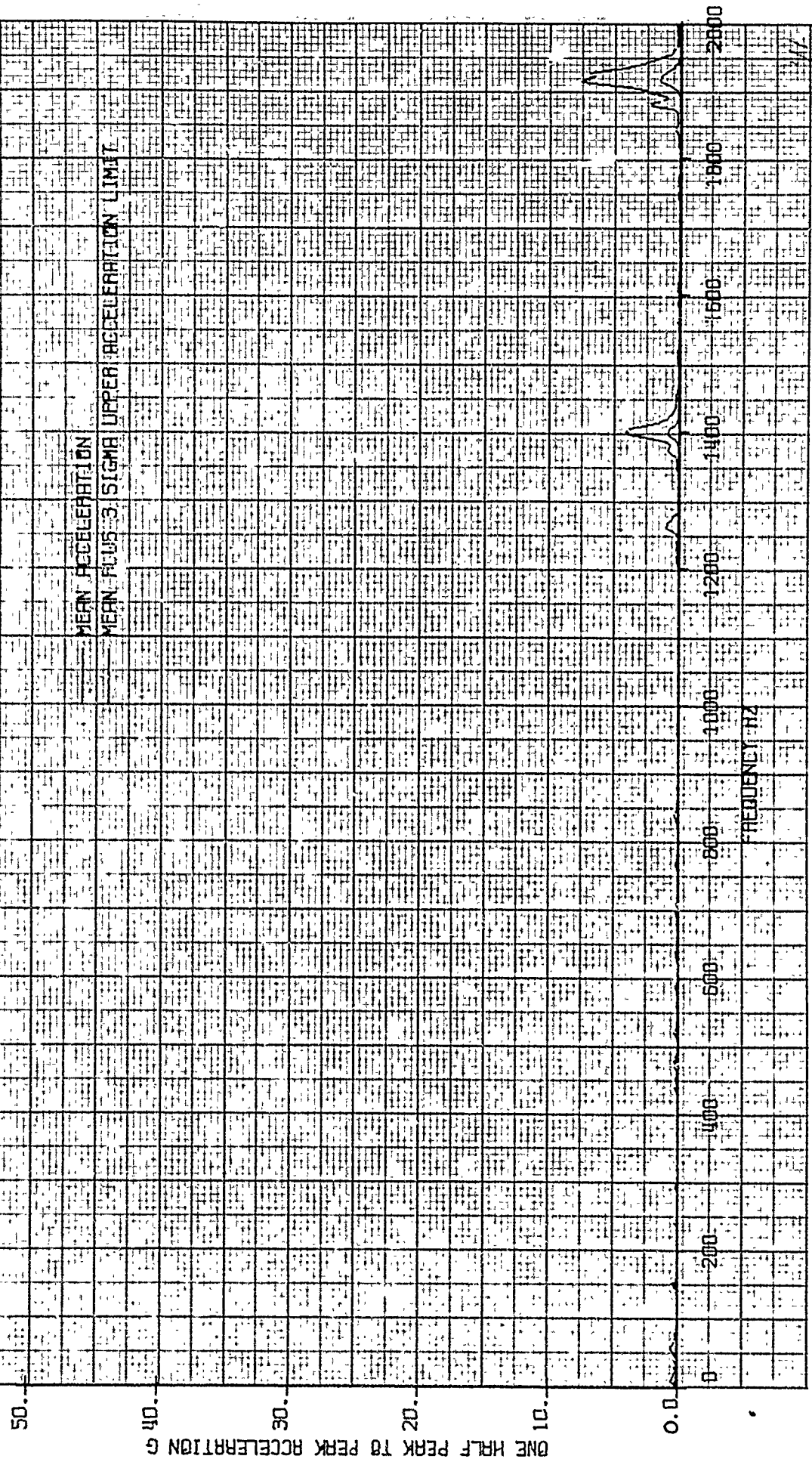




FIG. 42

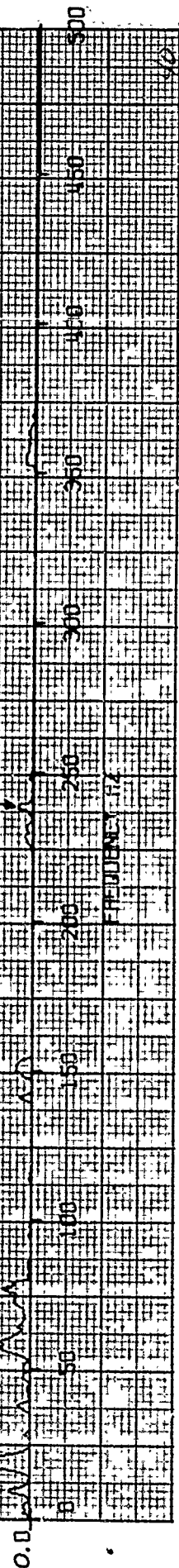
## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH-54B USA 5A1 69-18463  
 GP055 WT 28400 AND 41910LB AVG CG STA-110 CONFIG-CLEAN/POD/SLING  
 COMBINED FLT CARDS AFCS SERVO COMBINED AXIS VIB PLOT 183  
 SENSOR LOC 54 COMPRESSION PASS NO 2

CONDITIONS OF MAXIMUM ACCELERATIONS				COMPRESSION 183	
FREQUENCY ~HZ	FLT COND	CONFIG	AXIS	LOCATION NUMBER	VIB AMPL ~g
9.0	LF (8VH)	CLEAN	LONG	54	0.06
19.0	LDG A	SLING LOAD	VERT	54	0.58
57.0	T/O	CLEAN	LONG	54	0.09
77.0	LF (9VH)	CLEAN	LAT	54	0.08

ONE HALF PEAK TO PEAK ACCELERATION G

DATA SYSTEM NOISE AT 240HZ



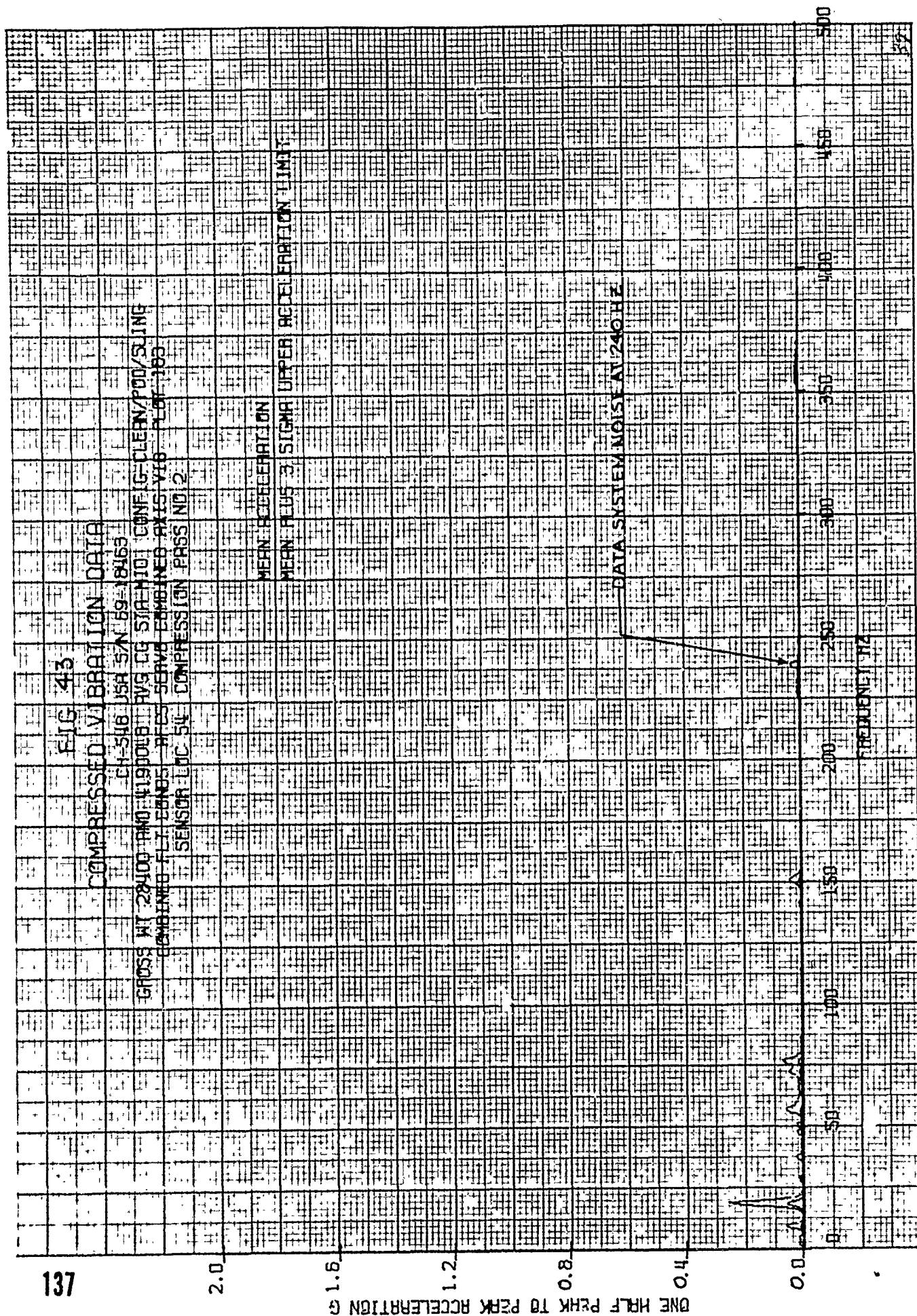




FIG. 44

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH-54B USA S/N 59-18463  
 GROSS WT 28400 AND 41900 LB AVG CG STR MID CONFIG CLEAN/POD/SLING  
 COMBINED FLT BONDS APP MOUNT AND CLUTCH COMBINED AXIS PLAT 184  
 SENSOR LOC 57.58 COMPRESSION PASS NO. 2

CONDITIONS OF MAXIMUM ACCELERATIONS				COMPRESSION 184	
FREQUENCY ~ HZ	FLT COND	CONFIG	AXIS	LOCATION NUMBER	VIB AMPL ~ g
1322.0	T/O	CLEAN	VERT	57	28.82
1880.0	VCRUISE R/C	POD	LONG	57	89.36
1892.0	VCRUISE R/C	POD	LAT	57	86.47
1912.0	OGE	POD	LAT	57	395.94
1932.0	OGE	SLING LOAD	VERT	57	281.92
1940.0	T/O	SLING LOAD	VERT	57	260.00
1968.0	LDG A	SLING LOAD	LAT	57	41.94

ONE HALF PEAK TO PEAK ACCELERATION

500

400

300

200

100

0.0

2000

1000

500

300

1000

1200

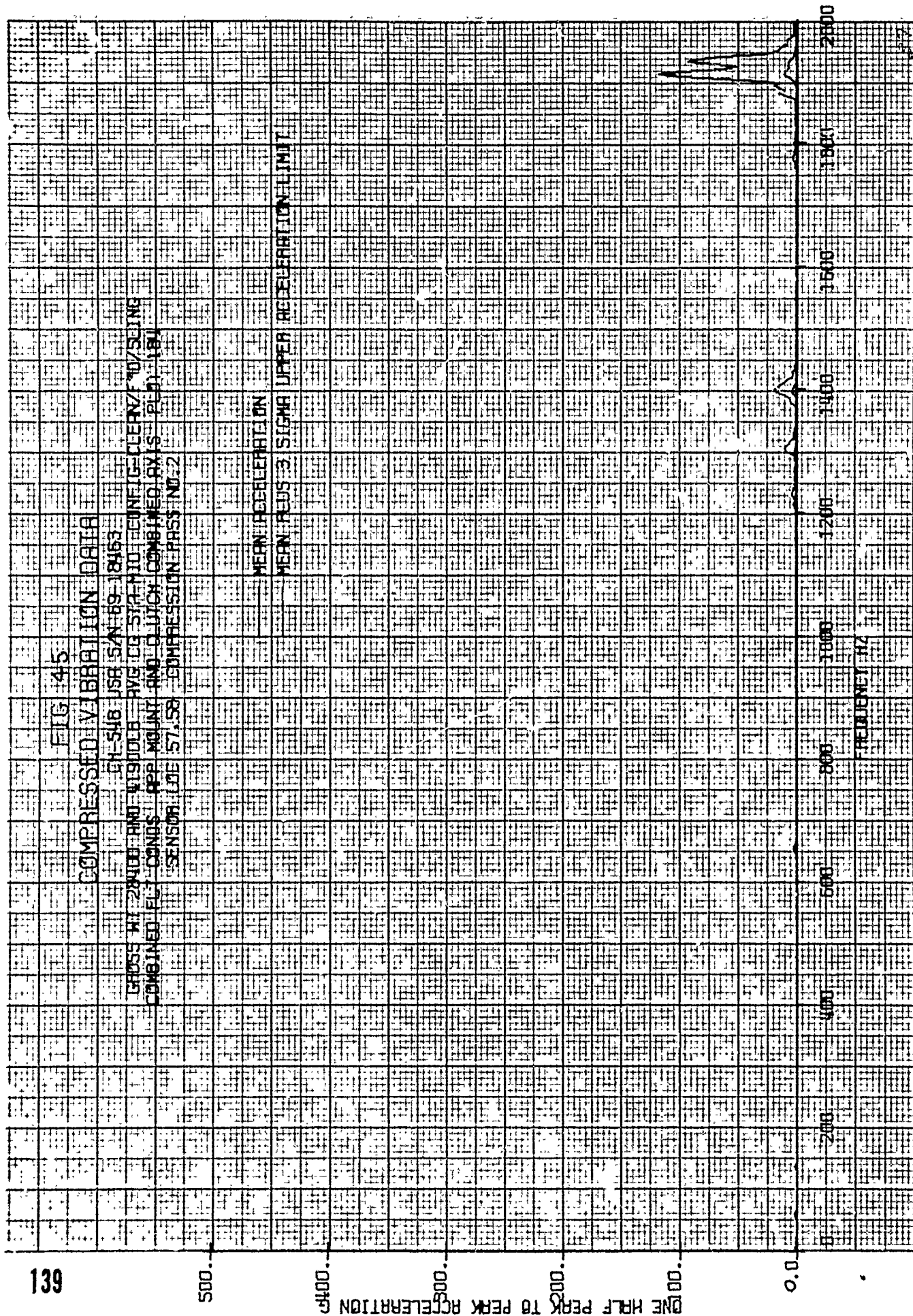
1400

1600

1800

2000

FREQUENCY HZ



140

20

ONE HALF PEAK TO PEAK ACCELERATION G

16

12

8

4

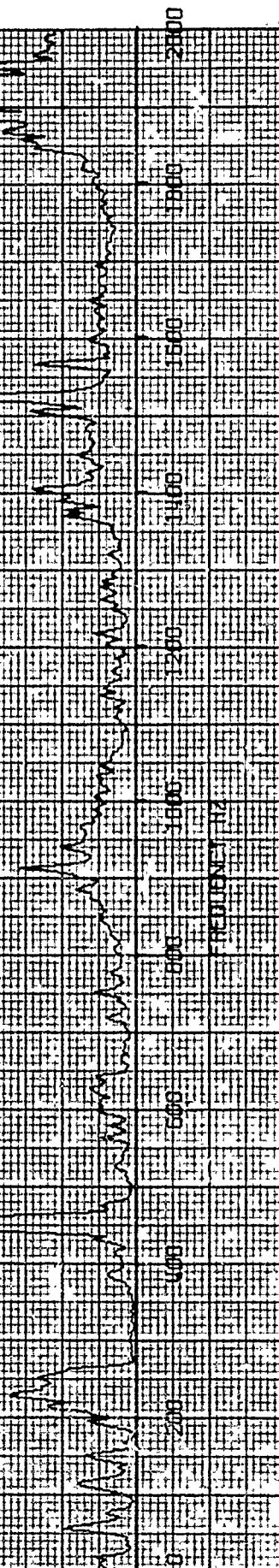
0

FIG 4-6

COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH-54B J58 S/N 59-18463  
 GROSS WT 28400 AND 41900LB AVG CG STR-MID COMFIG-CLEAN/POD/SLING  
 COMBINED FLT ENGINE MOUNTS COMBINED AXIS VIB PLAT 185  
 SENSOR LOC 60/61/62/63/64 COMPRESSION PHSS MD-2

CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION 185
FREQUENCY ~ Hz	FLT COND	CONFIG	AXIS	LOCATION NUMBER	VIB AMPL ~ g
228	LF(.8V)	POD	LAT	64	3.49
448	GND RUN	FLT IDLE	LAT	61	7.32
912	T/O A	SLING LOAD	LAT	61	3.19
1524	GND RUN	GND IDLE	LAT	60	6.32
1888	VCRUISE RC	POD	VERT	62	5.94
1912	OGE	POD	VERT	64	9.19
1928	OGE	SLING LOAD	LAT	60	8.23
1952	VCRUISE RC	POD	LAT	60	5.36





141

ONE HALF PEAK TO PEAK ACCELERATION G

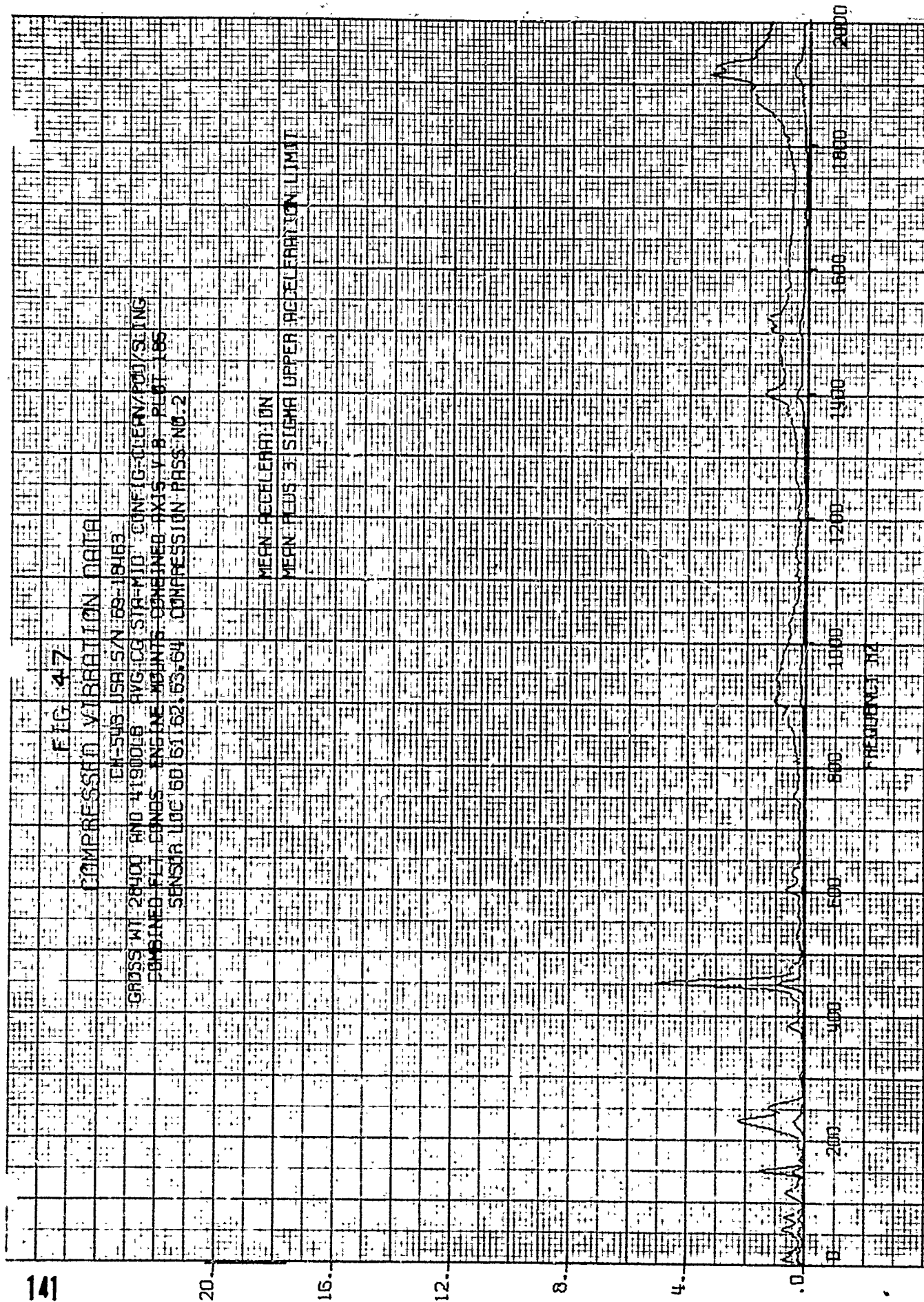


FIG 48

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH-54B USAF/N 189-18163  
 GROSS WT 28400 LBS AVG CG STR MID CONFIG CLEAN/POD/SLING  
 COMBINED FLT COND ENGINE COMBINED AXIS VIB PLT 186  
 SENSOR LOC 65.66.67.68.69.70 COMPRESSION PHSS NO 2

CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION 186	
FREQUENCY ~ HZ	FLT COND	CONFIG	AXIS	LOCATION NUMBER	VIB AMPL ~ g	
264.0	VERUISE R/C	POD	LAT	68	3.88	
520.0	VBEST R/C	POD	LAT	68	14.64	
564.0	T/O	SLING LOAD	VERT	67	12.11	
668.0	VERUISE R/C	SLING LOAD	LAT	68	16.53	
780.0	VBEST R/C	POD	LAT	68	3.83	
868.0	OGE	SLING LOAD	LAT	66	4.37	
1040.0	VBEST R/C	POD	LAT	68	6.90	
1136.0	FLT IDLE	GND RUN	LAT	70	5.26	
1256.0	OGE	SLING LOAD	VERT	67	3.76	
1308.0	VERUISE R/C	POD	VERT	69	4.27	

0.5

2000

4000

6000

8000

10000

12000

14000

16000

18000

20000

FREQUENCY HZ

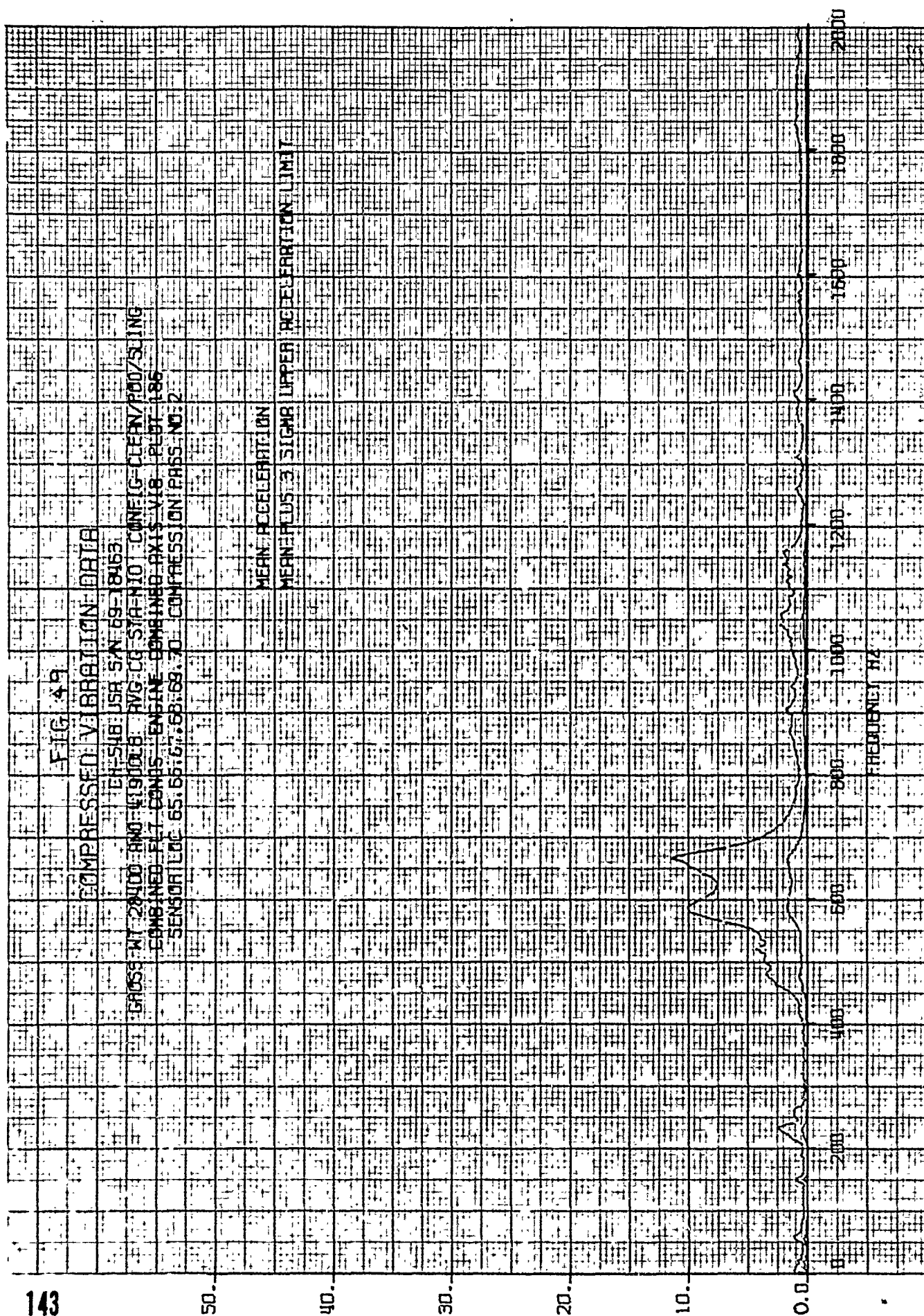




FIG 50

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CM-540-ISA-57N-69-18463

GRCS AT 28000LB AVG CG STAR-HID CONE10-CLEAN

END TEST APP PLAN ONLY RPP ABOUT AND CLUTCH COMBINED AXIS VIB PLY 153

SENSOR LOC 57.58 COMPRESSION PASS NO.1

20

16

12

8

4

0.0

ONE HALF PEAK TO PEAK ACCELERATION G

0 200 400 600 800 1000 1200 1400 1600 1800 2000

TIME IN SECS



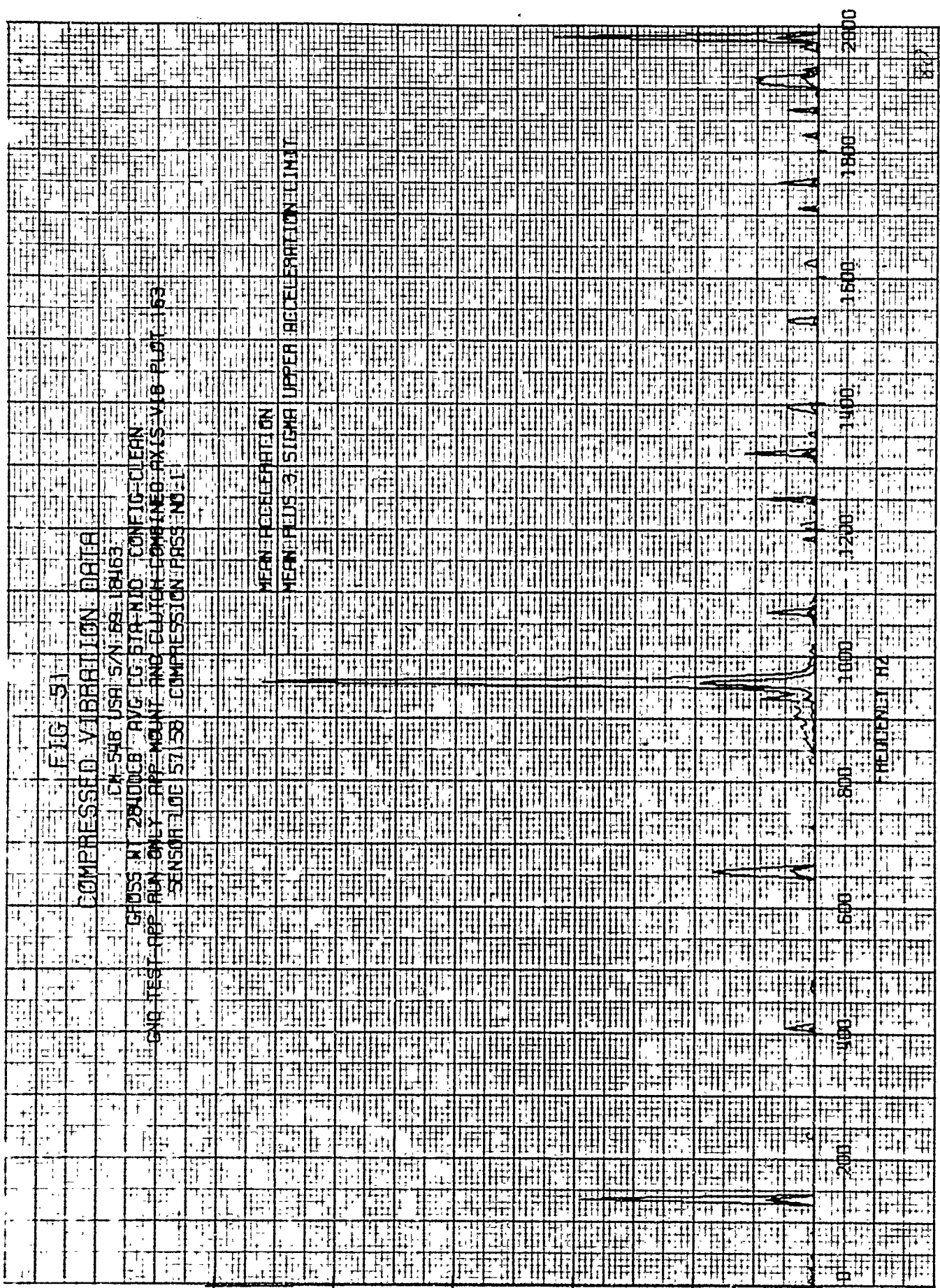


FIG 52

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH 548 USA S/N 89-18463  
 GROSS WT 28400 LB AVG CG 67A-M30 CONFIG CLEAN  
 GND TEST DRP RUN ONLY DRP FUEL PRESS SH COMBINED AXIS Y18 PLOT 152  
 SENSOR LOC 4U COMPRESSION PASS NO 11

NOTE: NO STATISTICAL ANALYSIS WAS PERFORMED  
 ON THIS DATA SINCE THERE IS ONLY ONE  
 DATA RECORD AT THIS CONDITION

ONE HALF PEAK TO PEAK ACCELERATION G



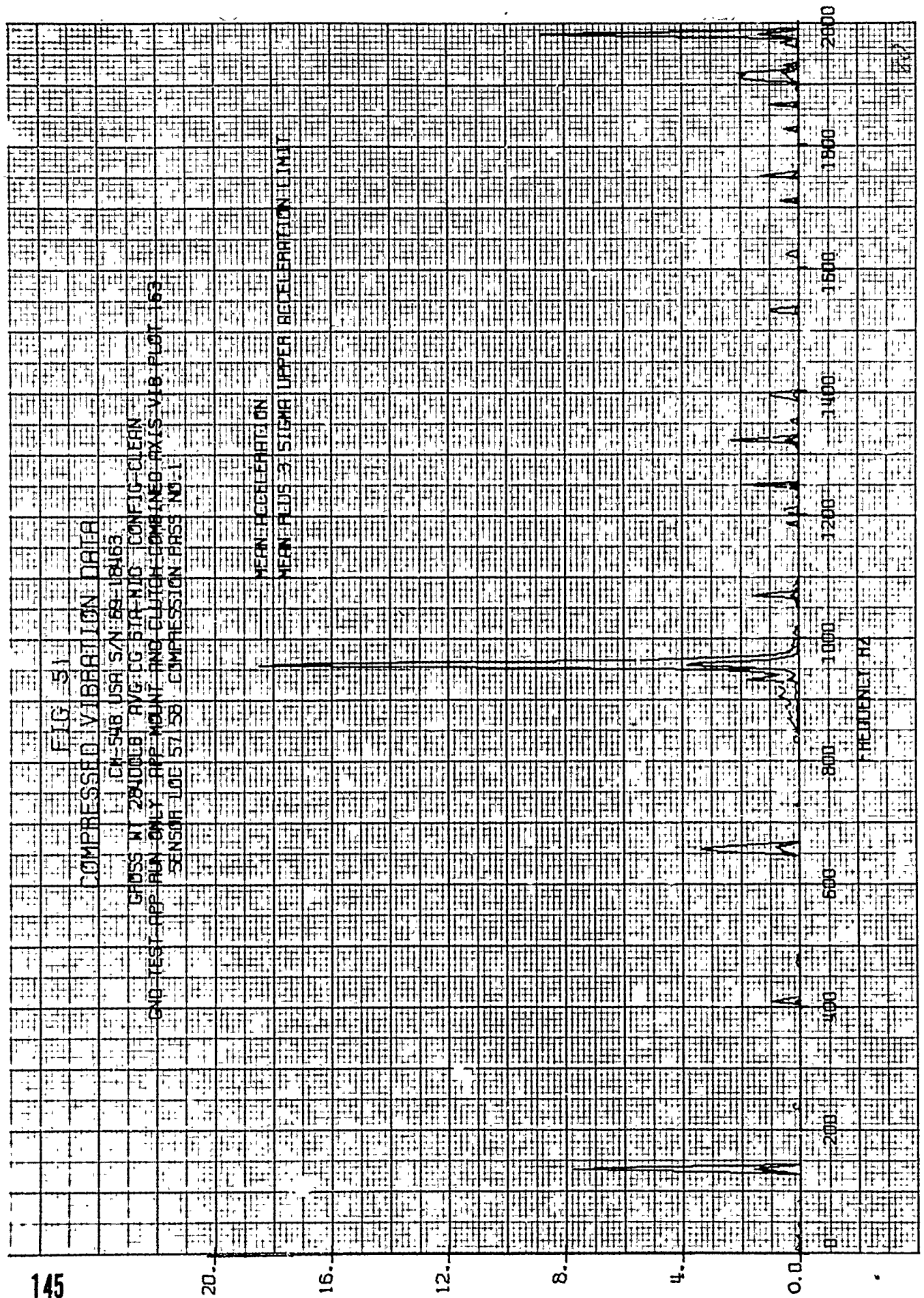


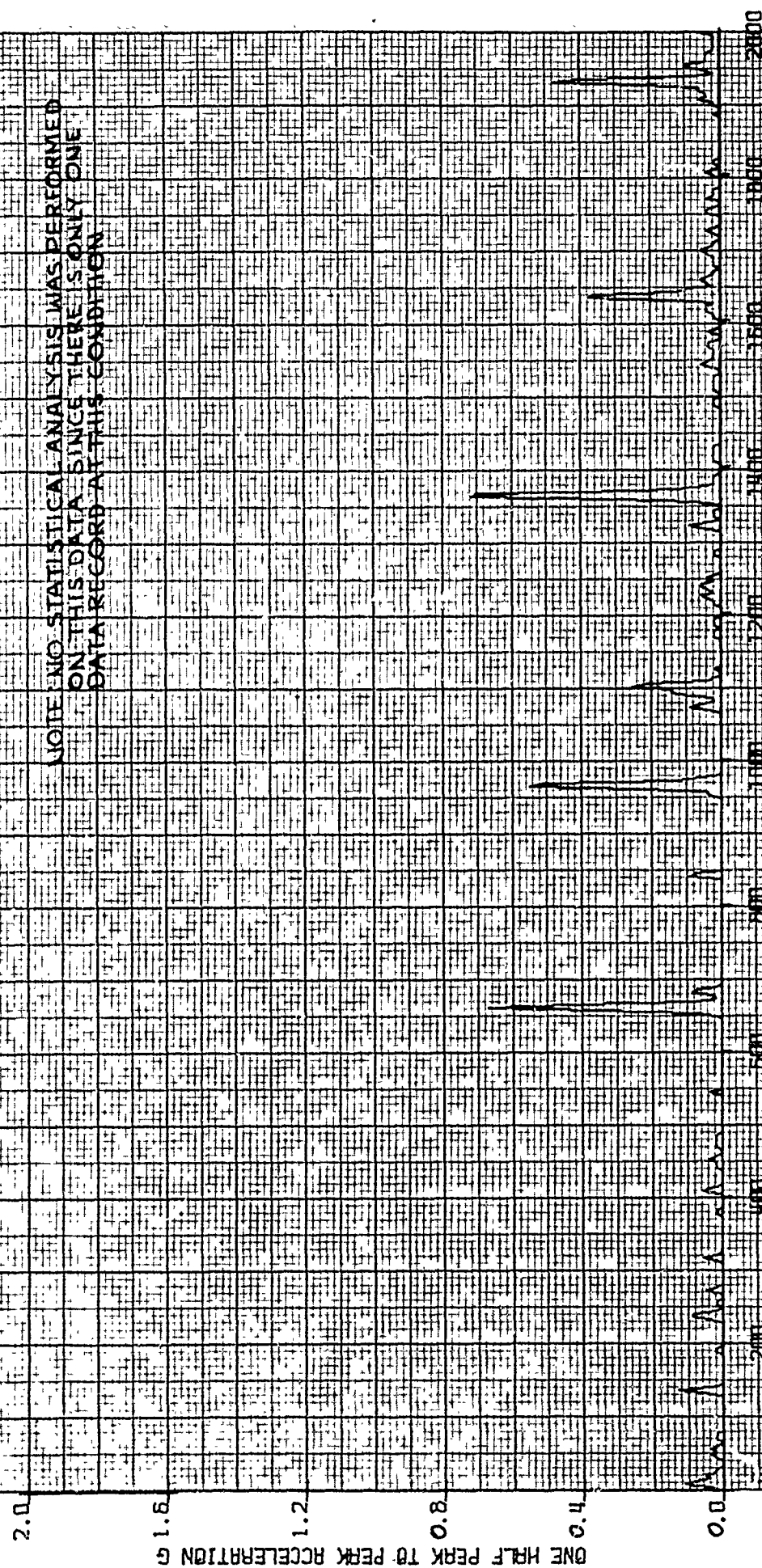


FIG 52

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH-54B USA S/N 69-18453  
 GROSS WT 28100 LB AVG CG STA NO 0 CONFIG CLEAN  
 GND TEST APP RUN ONLY APP FUEL PRESS SH COMBINED AXIS VIB PLOT 152  
 SENSOR LOC WW COMPRESSION PASS NO 1

NOTE: NO STATISTICAL ANALYSIS WAS PERFORMED  
 ON THIS DATA SINCE THERE IS ONLY ONE  
 DATA RECORD AT THIS CONDITION



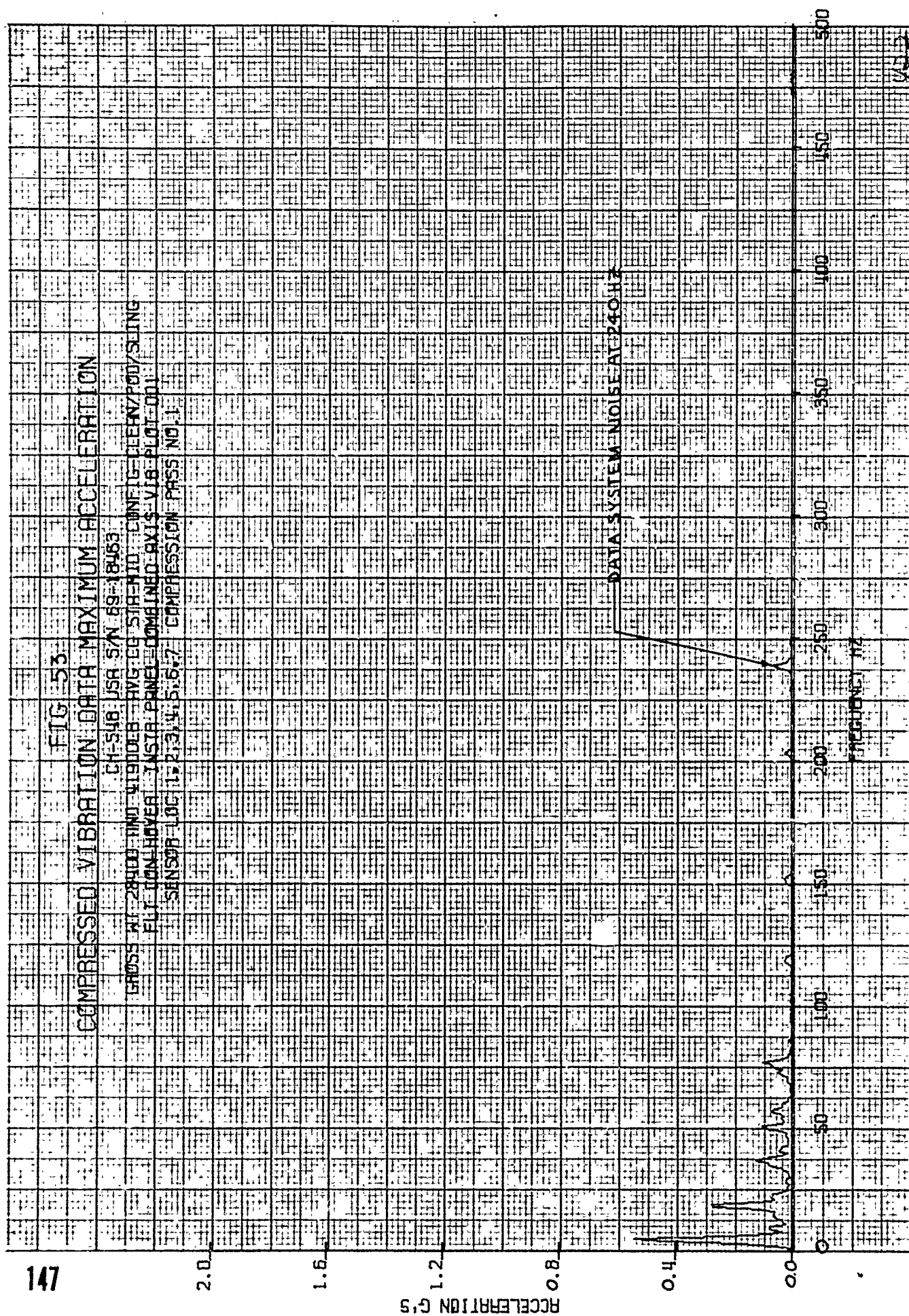


FIG 54

## COMPRESSED VIBRATION DATA

CH-546 USA S/N 69-18163  
GROSS WT 28400 AND WINDLER AVG CG STR-MID CONFIG-DEERY/30D/SLING  
FLT CON-LIVER INSTR PANEL COMBINED AXIS VIB PLOT 001  
SENSOR LOC 1, 2, 3, 4, 5, 6, 7 COMPRESSION PASS NO. 1

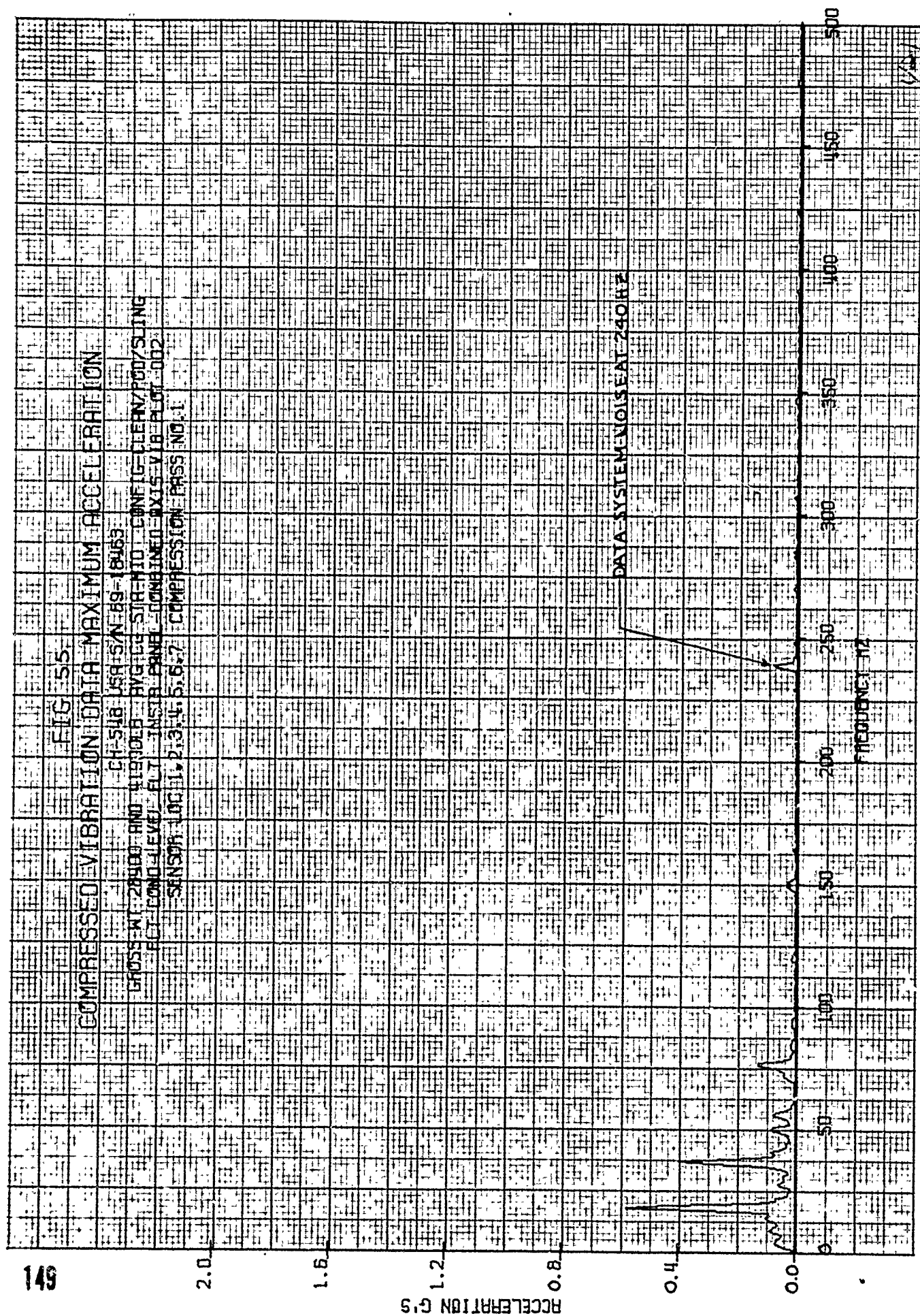
MEAN ACCELERATION  
MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

DATA SYSTEM NOISE AT 240 Hz

FREQUENCY Hz

7/2/68







150

2.0

1.6

1.2

0.8

0.4

0.0

ACCELERATION G'S

FIG 56

COMPRESSED VIBRATION DATA

CH 508 USA S/N 69-18463  
 CROSS AT 28900 RPM VIB 10.8 AVG CG STATION ID1 CONFIG ELEV/PD/S/LING  
 ALT COND LEVEL FLT INSTR PANEL COMBINED AXIS VIB PLT 002  
 SENSORS LOG 1, 2, 3, 4, 5, 6, 7 COMPRESSION PASS NO. 1

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

DATA SYSTEM NO SE AT 240112

FREQUENCY Hz

500

450

400

350

300

250

200

150

100

50

0

500

450

400

350

300

250

200

150

100

50

0

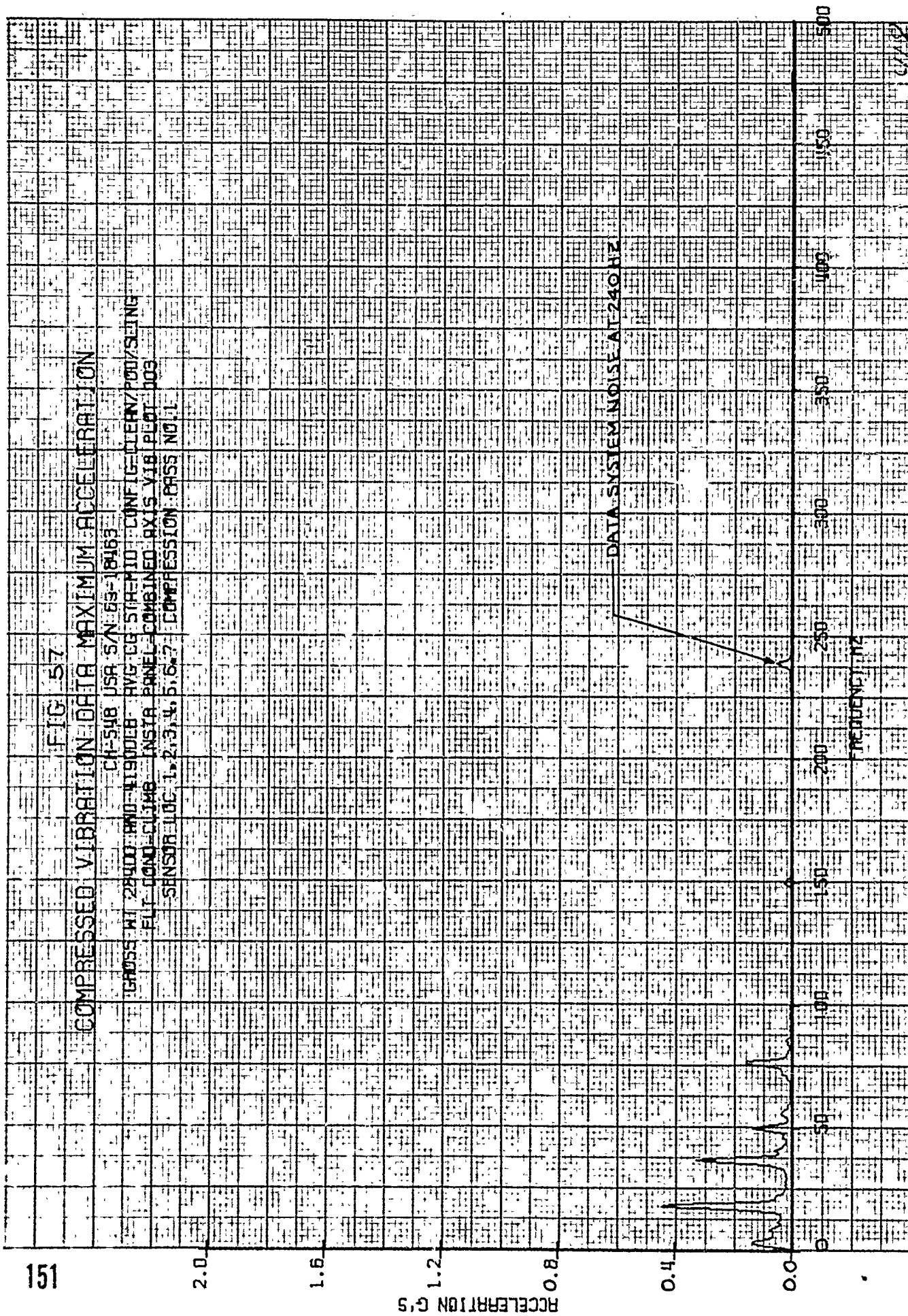


FIG 58

## COMPRESSED VIBRATION DATA

GROSS WT 28400 RND 41900LBS  
 CH-540 USA S/N 69-18463  
 AVG LG SJR-F111 CONE LG MEERN/POU/SLING  
 FLT 0000-CL106 INSTA PANEL COMBINED RX'S-V18 PLAT 103  
 SENSOR LOC 1, 2, 3, 4, 5, 6, 7 COMPRESSION PASS NO. 1

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

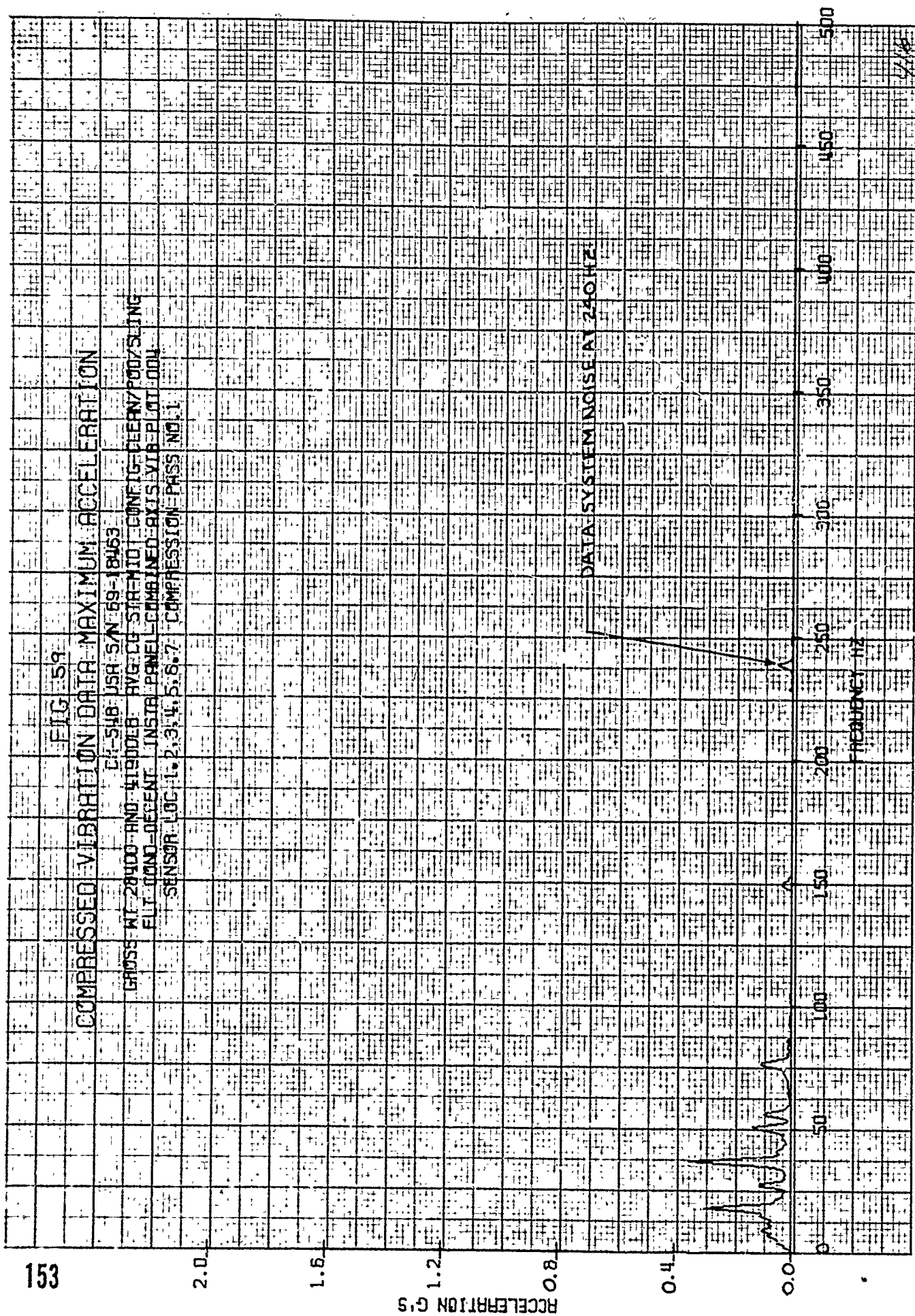
ACCELERATION G'S

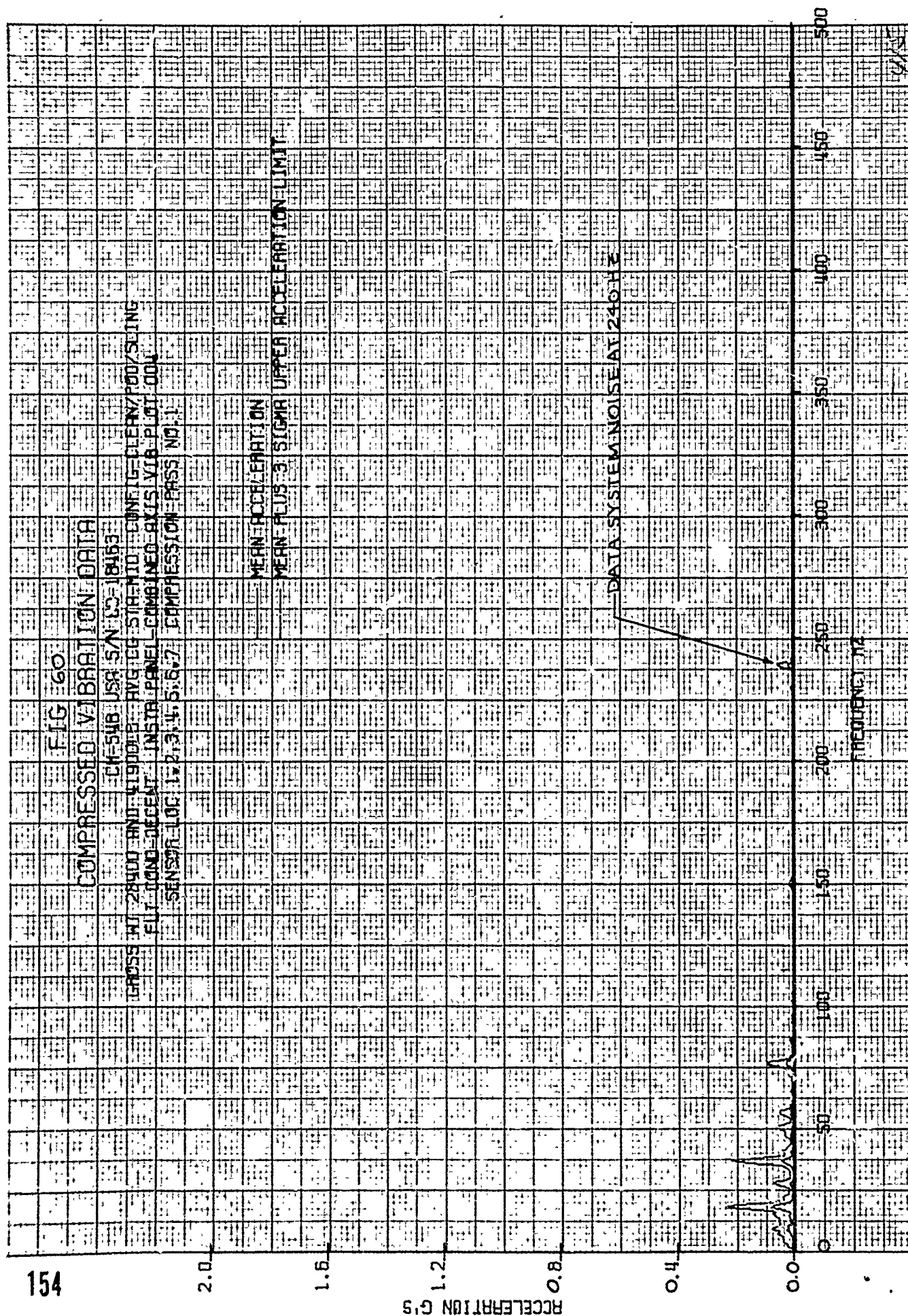
DATA SYSTEM NOISE AT 240 HZ

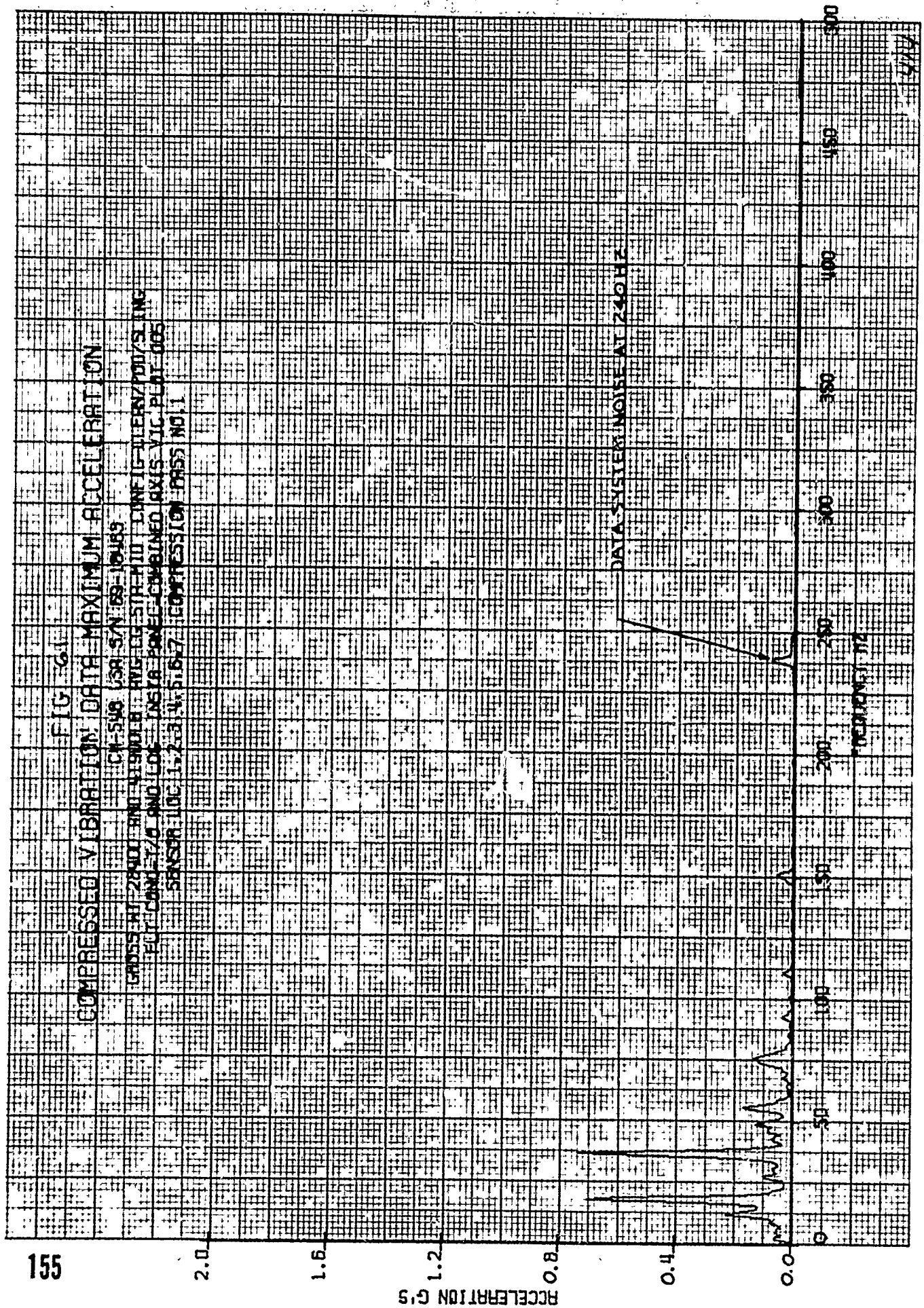
FREQUENCY HZ

1917















KIT G3

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

14-500 USB SAN 68-10053  
 GROSS WT 28000 AND VIBRODOL KIT CG STR-110 CON-IG-STER/100/SLING  
 FLT COND MEASUREMENTS MASTER PANEL COMBINED AXIS 118 PLAT 005  
 SENSOR LOC 1.2.3 V. 5.6.7 COMPRESSION PRESS NO. 1

2.0

1.6

1.2

0.8

0.4

0.0

ACCELERATION G'S

DATA SYSTEM NOISE AT 240 HZ

FREQUENCY HZ

500

450

400

350

300

250

200

150

100

50

0

4/13

FIG. 64

## COMPRESSED VIBRATION DATA

CM-548 USA SN 69-10453  
 CROSS HT 20000 AND USM01B HVG EG STRIPD LCONF G-LEARN/100/SLING  
 FLT COND-MANUEVERING INGER-PANEL-COMBINED AXIS-1/8-PLAT-005  
 SENSOR-LDC 11-213-V-5-6-7 COMPRESSION PASS NO.1

MEAN ACCELERATION  
 MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

DATA SYSTEM NOISE AT 200HZ

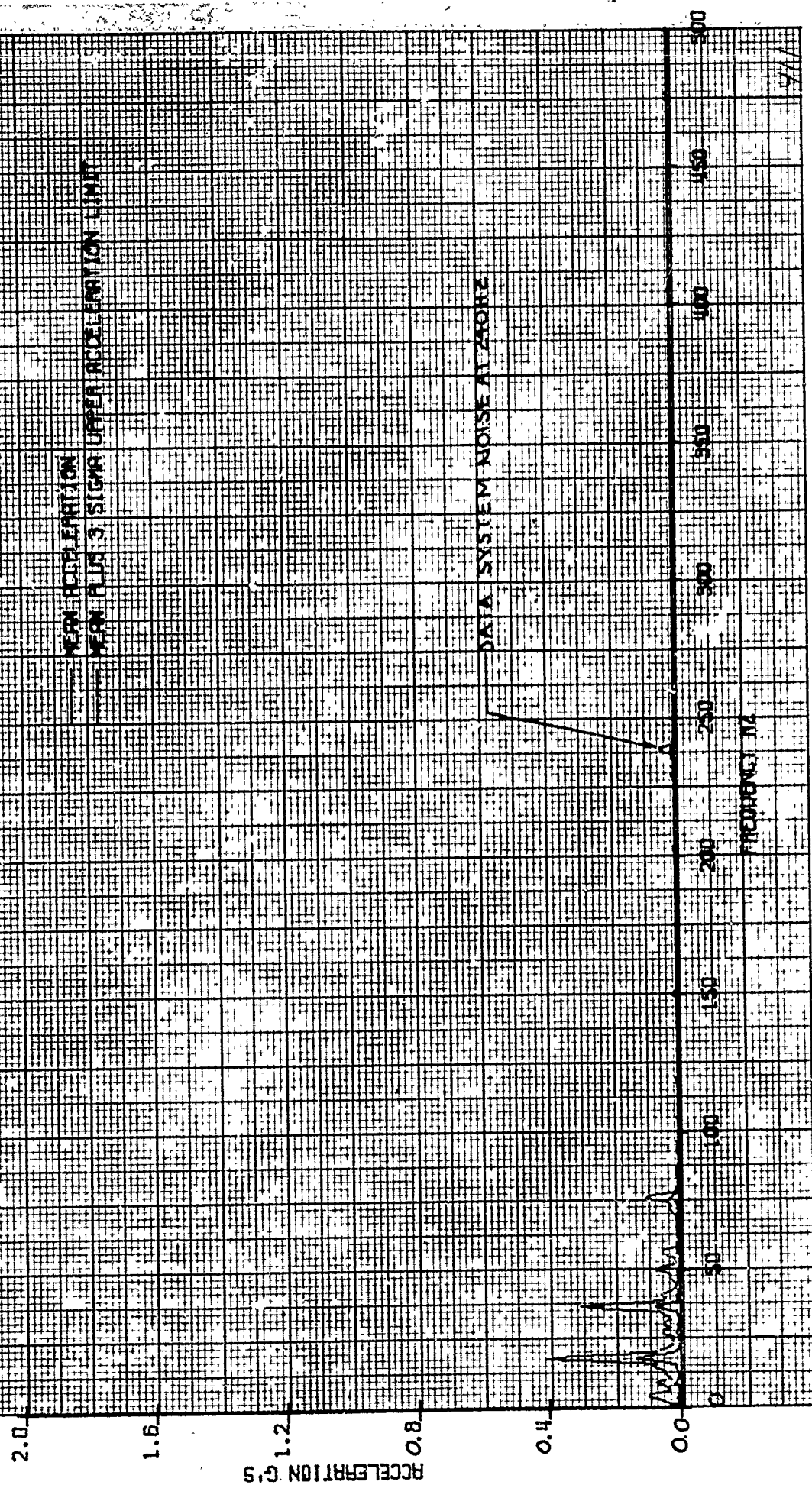


FIG. 65

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH 518 J58 S/N 59-18463

GROSS W 2600 LB AVG EG STR N/D CONFIG CLEAN

END TEST COND G40/FLT 10 LE INSER PANEL COMBINED AXIS PLAT 2

SENSOR LOC 1.2 3.6 5.6 7 COMPRESSION PASS NO. 1

2.0

1.6

1.2

0.8

0.4

0.0

ACCELERATION G'S

DATA SYSTEM NOISE AT 1250 Hz

FREQUENCY Hz

50 100 150 200 250 300 350 400 450 500

0.0

0.4

0.8

1.2

1.6

2.0

2.4

2.8

3.2

3.6

4.0

4.4

4.8

5.2

5.6

6.0

6.4

6.8

7.2

7.6

8.0

8.4

8.8

9.2

9.6

10.0



FIG 66

## COMPRESSED VIBRATION DATA

CM-548 USA 5/4/68-18463  
 GROSS WT 28.00 LB RVS 10 BTX INHD CONF-JP-CLEAN  
 PND TEST-0000-040/ALT 10LE INSTA PANEL COMBINED AXIS PLAT-002  
 SENSOR LOC 1-2-3 1-5-5-5-7 COMPRESSION PASS NO. 11

2.0

1.6

1.2

0.8

0.4

0.0

ACCELERATION G'S

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

DATA SYSTEM NOISE AT 240 HZ

FREQUENCY HZ

500

450

400

350

300

250

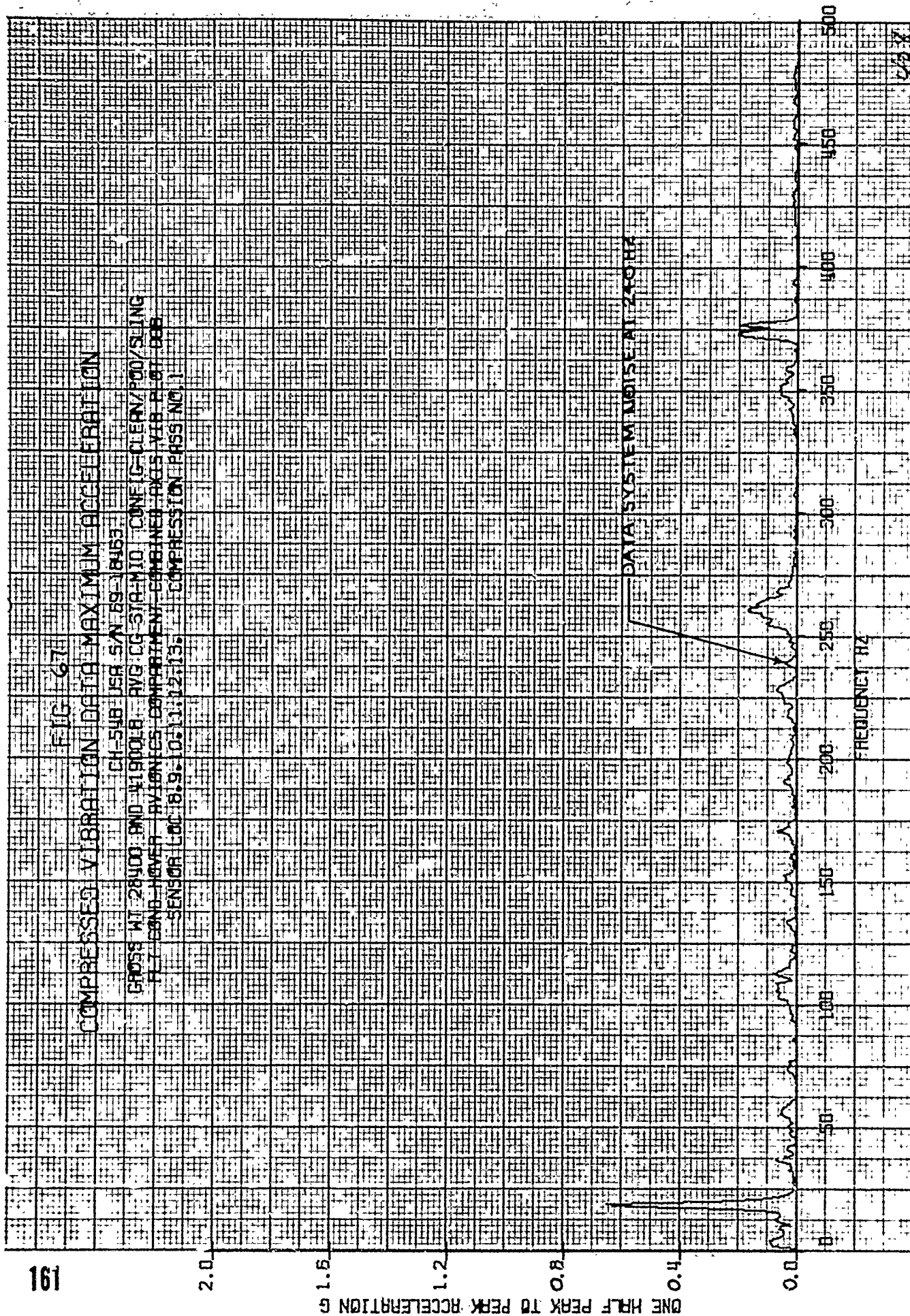
200

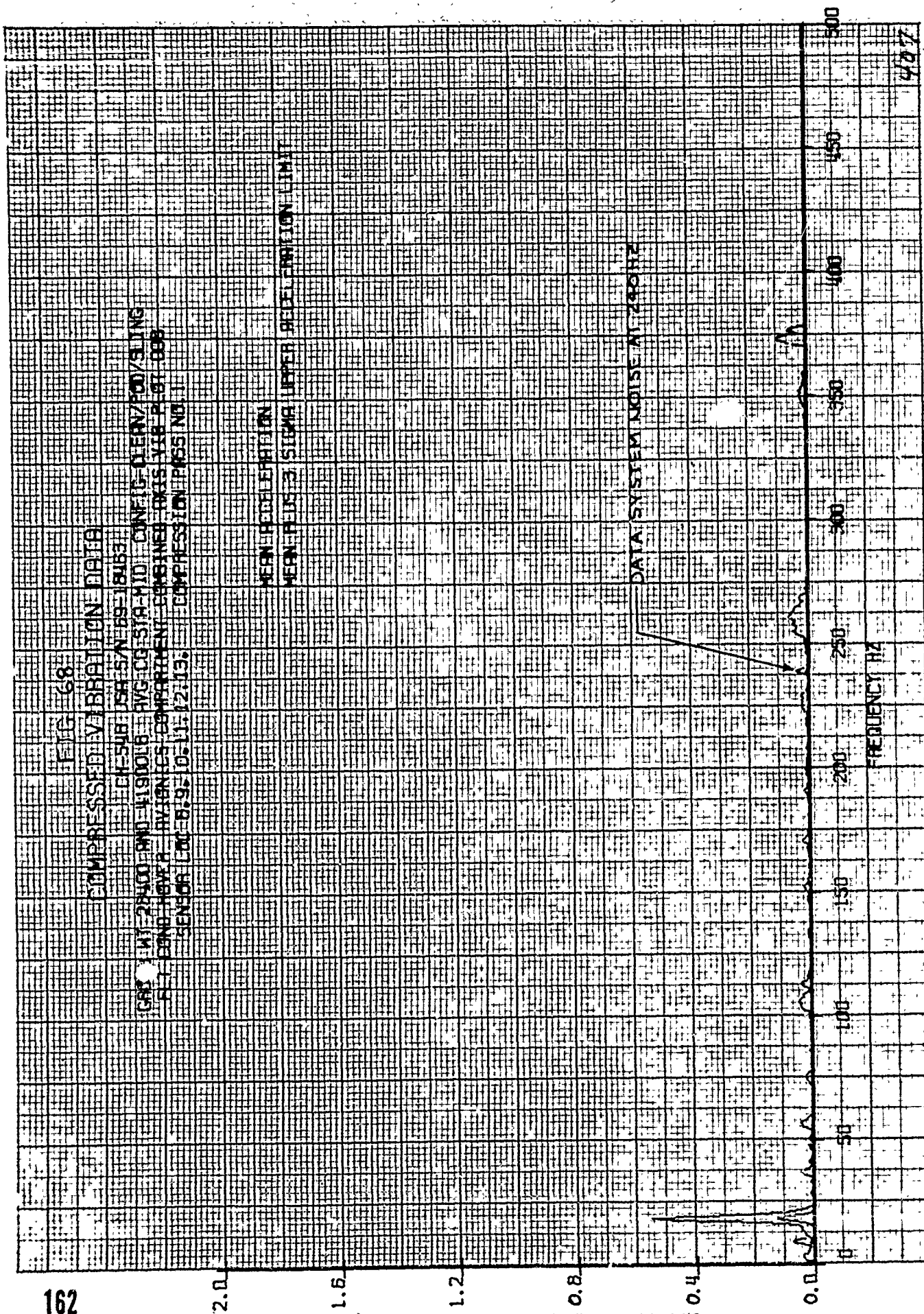
150

100

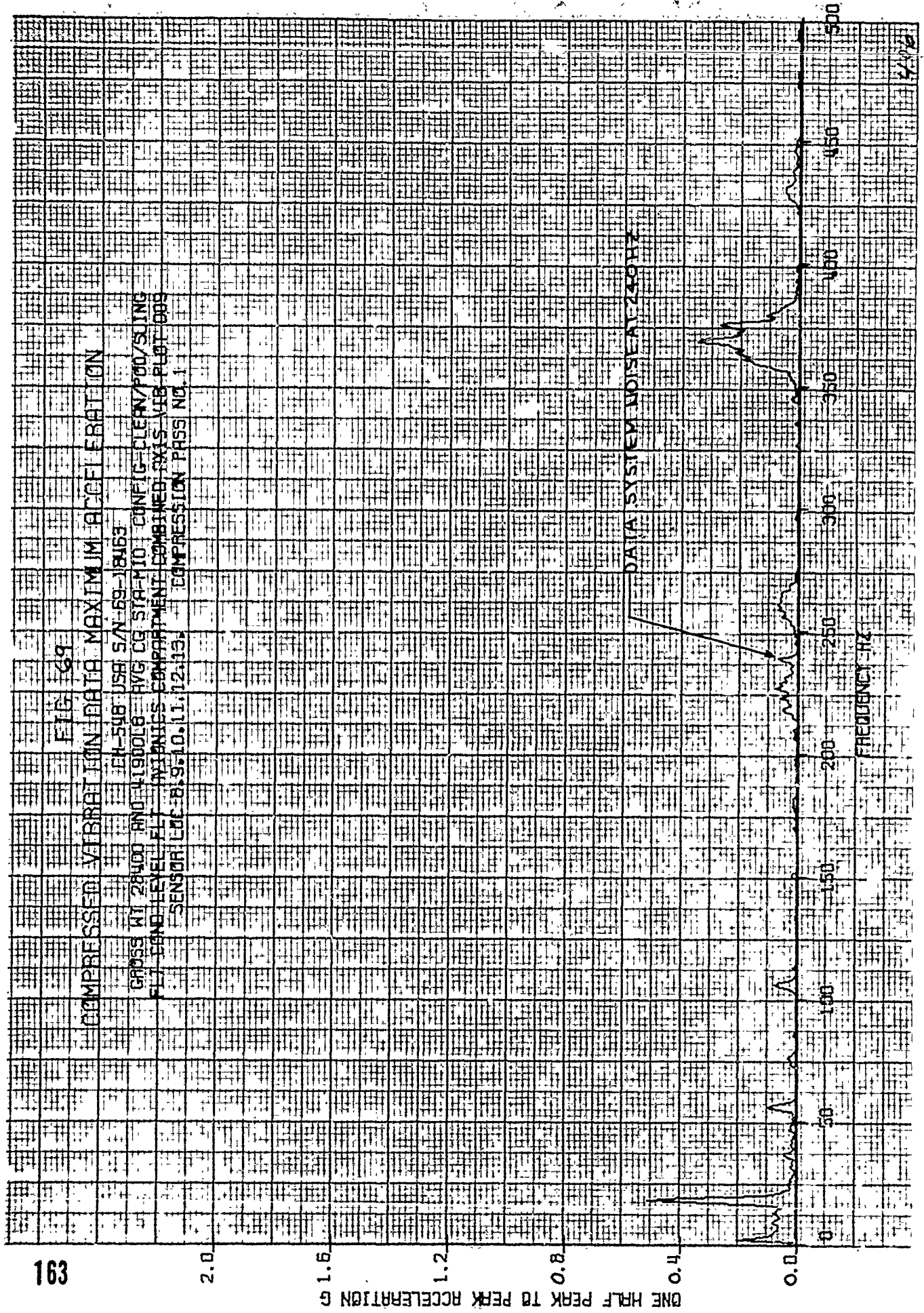
50

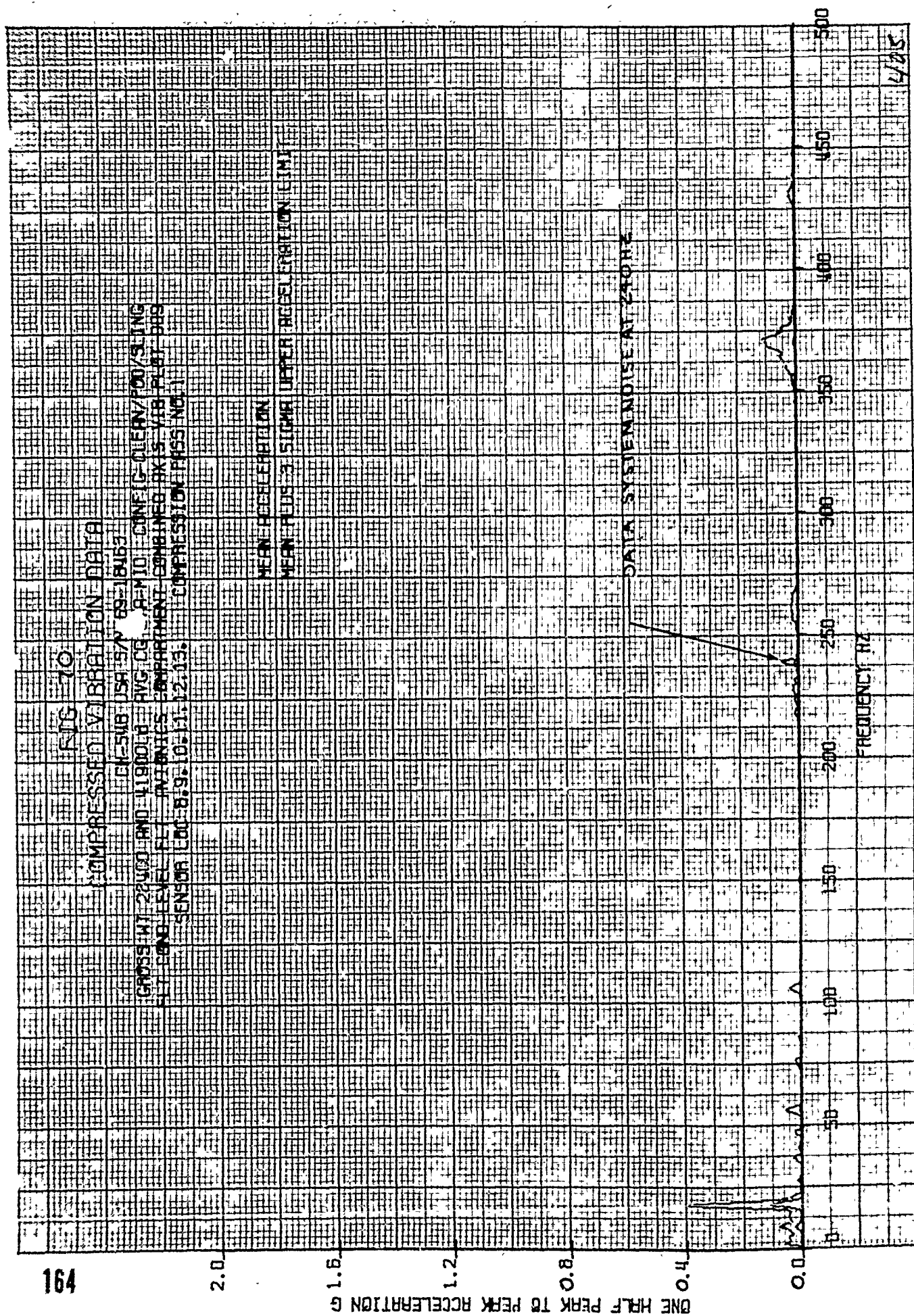
U-459







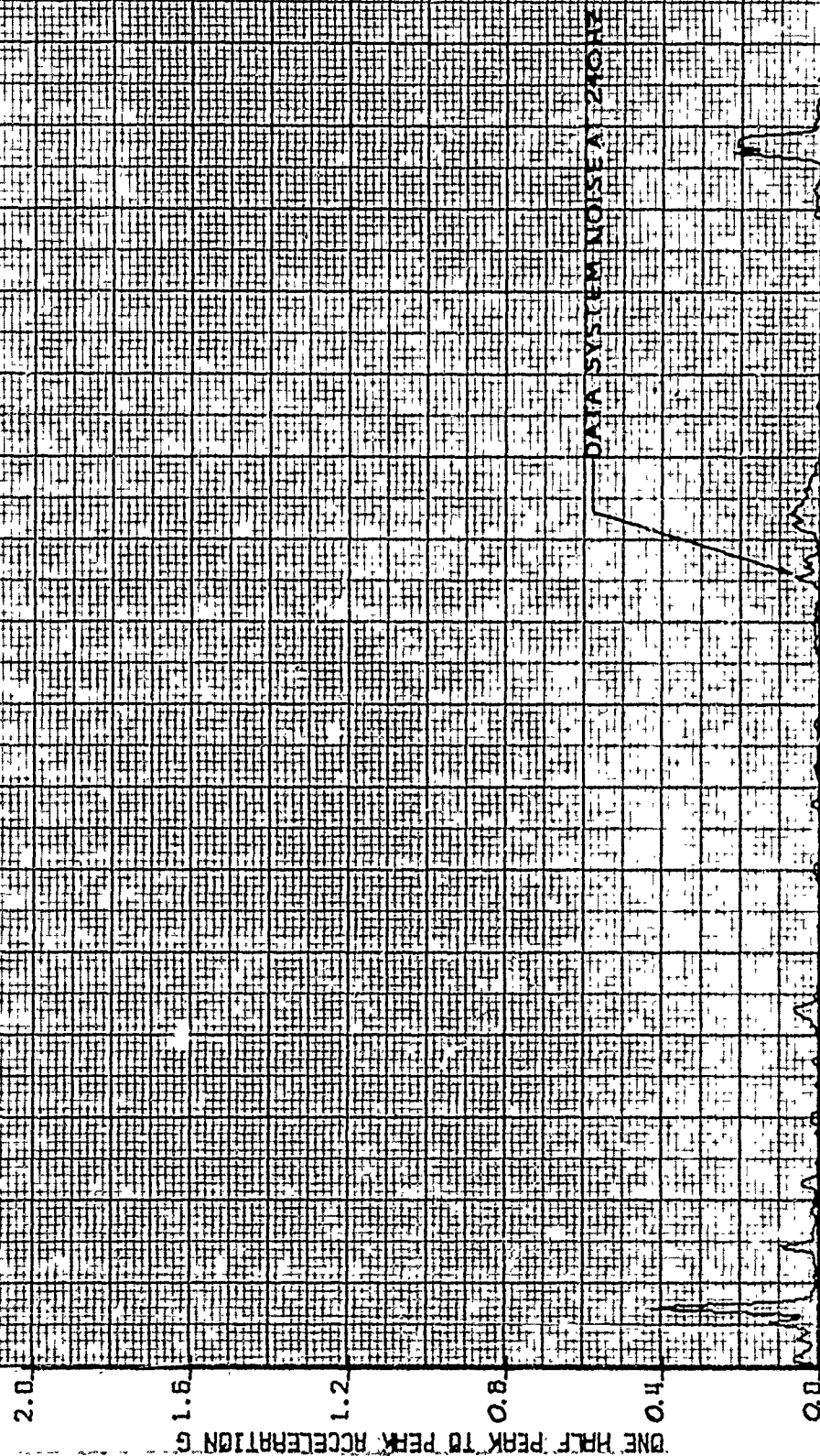




165

# COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

FIG. 17  
 CR-506 USA 57N 69-18463  
 GROSS WT 28.000 AND 119.0018 AVG CG STR-M10 CONE G-CLEEN/POD/SLING  
 FLT COND-ACMB RVLONCES COMPARTMENT COMBINED DATA VER PLOT 818  
 SENSOR LOC 819.0.11-12/13. COMPRESSION PASS NO. 1



0.0

0.4

0.8

1.2

1.6

2.0

0

50

100

150

200

250

300

350

400

450

500



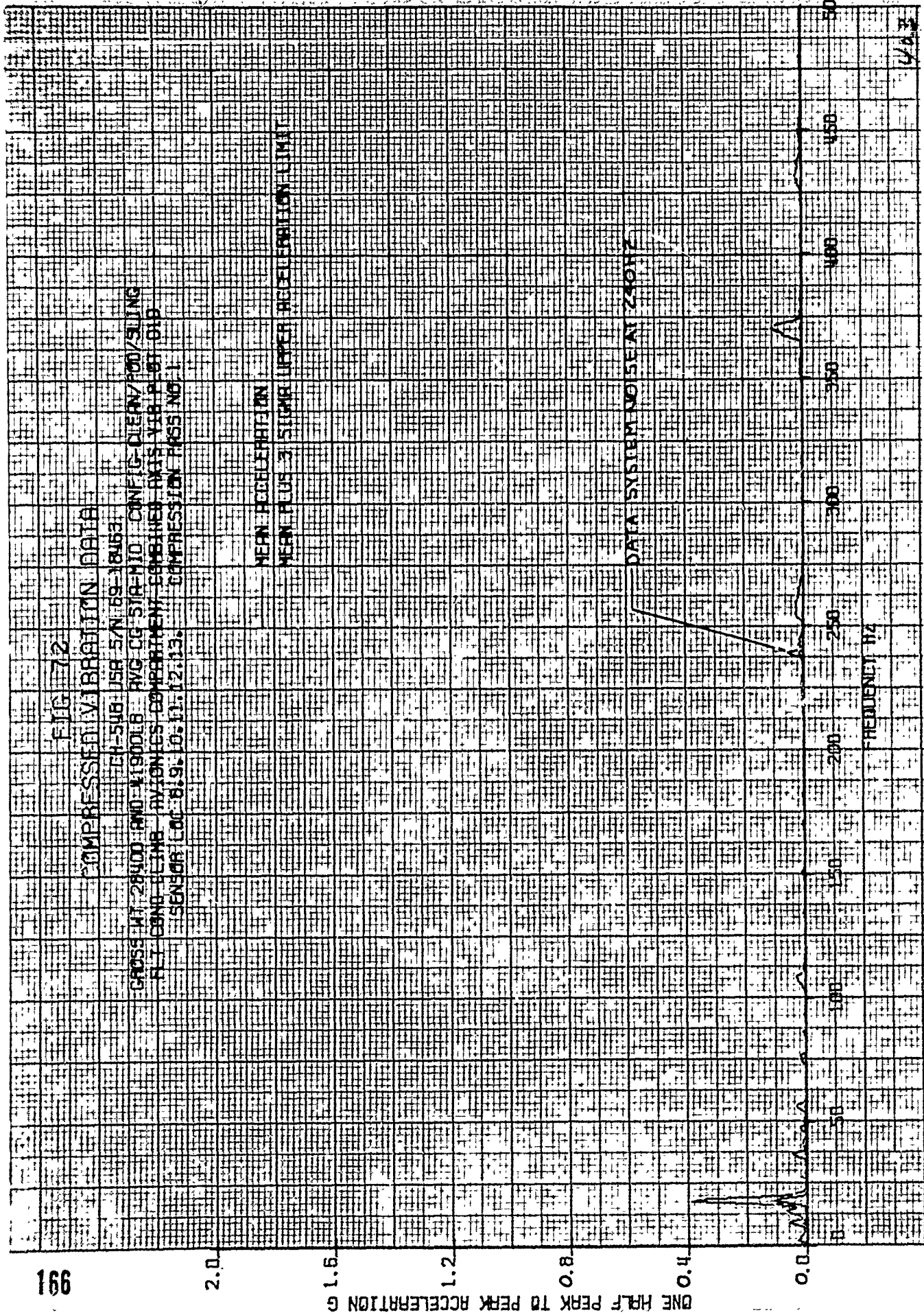


FIG 73

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

ICH-54B USA 5/N 89-18U63

GROSS WT 28.00 AND 11.90 LB AVG CG STA-MID CONF (G-DUEN/POD/S/ING  
 FLT END-DESCENT AVIONICS COMPARTMENT SUBMERGED AXES VIB PLAT BEL  
 SENSOR LOC 8.9.10-11.12.13. COMPRESS (ON PASSING NO 1

2.0

1.6

1.2

0.8

0.4

0.0

ONE HALF PEAK TO PEAK ACCELERATION G

0

100

150

200

250

300

350

400

450

500

FREQUENCY HZ

DATA SYSTEM NOISEA 24012

600

FIG 7-4

COMPRESSED VIBRATION DATA

CH-508 DES 5/N 89-18163  
 CROSS INT 28400 TWO 1130018 AVG OF STR-M10 CM 1G CLEN/PMS/SLING  
 FLT-608 RESIDENT AVIATION-CONTRACTOR ENGINEER PMS VIB-8-1-811  
 SENSOR L/C 0.9.10.13.12.13 COMPRESSION PRESSING 1

WEN MEASUREMENT

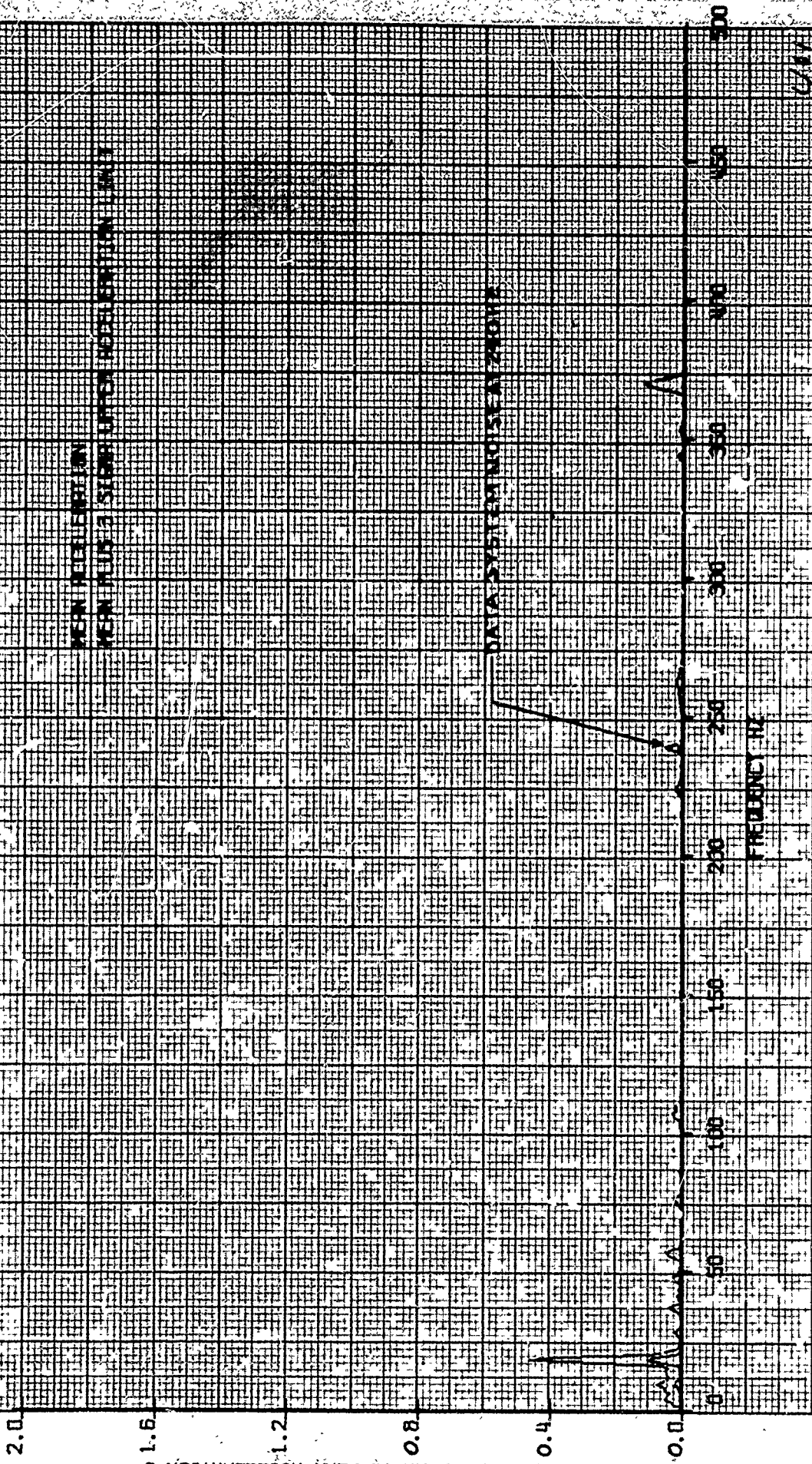
WEN M1013 STONE UPPER NOISE/STATION 1 M11

ONE HALF PEAK TO PEAK ACCELERATION G

DATA SYSTEM NOISE FLOOR

FREQUENCY HZ

CMV





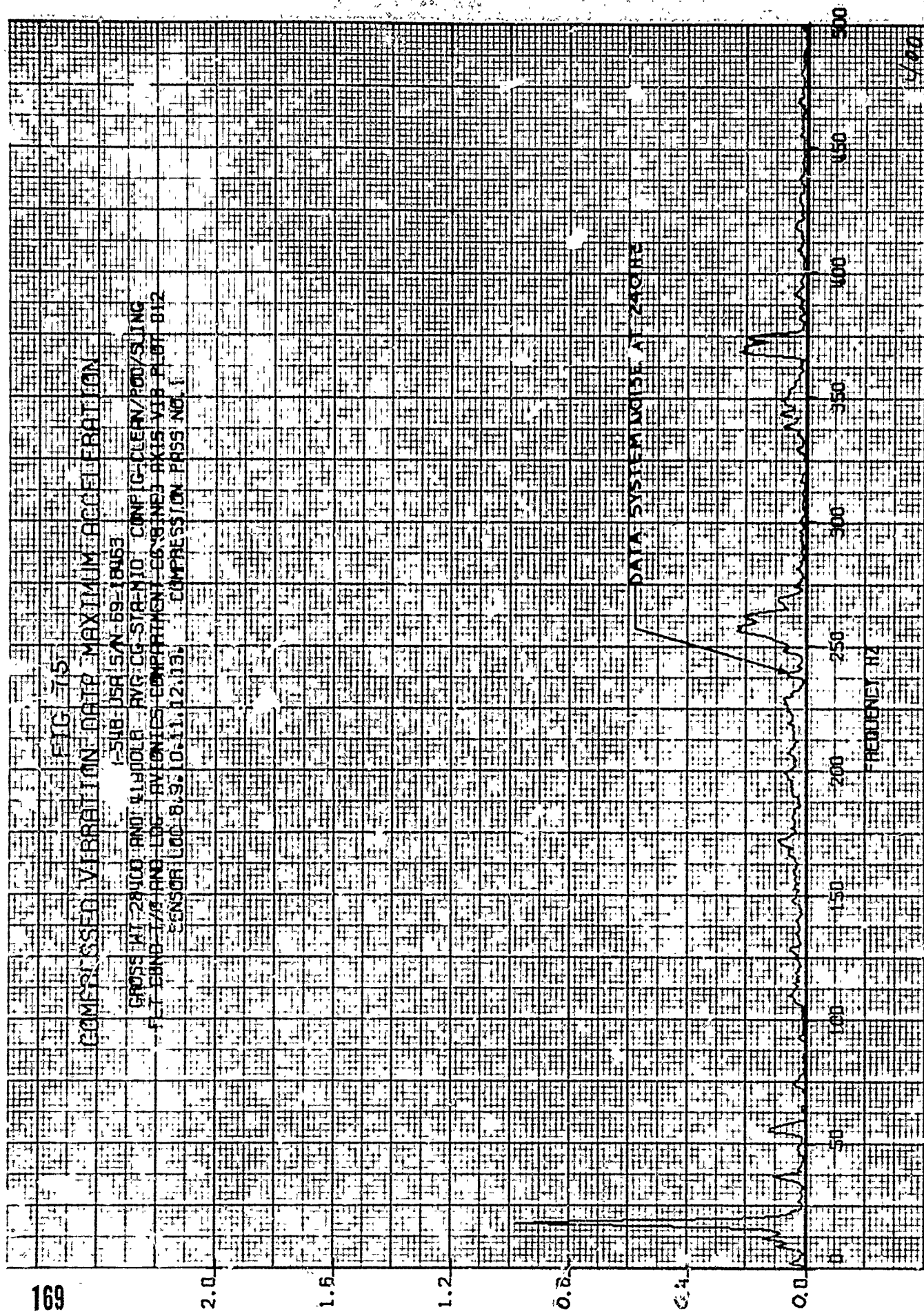


FIG 76

## COMPRESSED VIBRATION DATA

CH 508 USR 5/M 89-18063

GROSS WT 28400 AND 41900 LB  
 NET WT 178 AND 185 LBS  
 SENSORS 100 8.5 10.1 12.15  
 COMPRESSION PRESS 100 PSI

NEAR ROTATION

NEAR ROTATION UPPER ROTATION LIMIT

DATA SYSTEM NOISE AT 2.012

FREQUENCY Hz

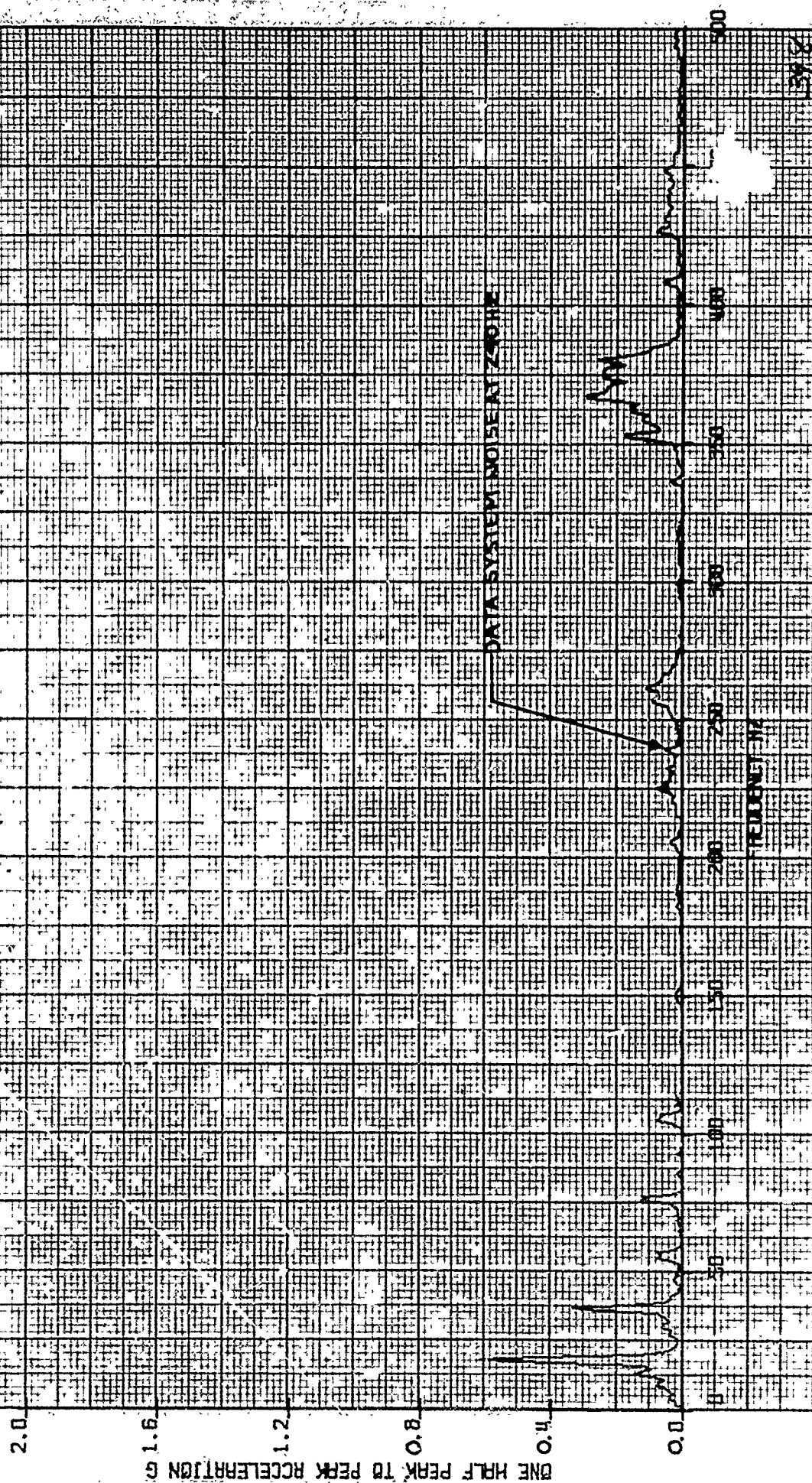
FREQUENCY Hz

207

FIG. 77

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

GROSS WT 28400 LBS. 11900 LBS. AVG CG STA 110 CONFIG-CLEAN/POD/SLING  
 FLT COND-HANDLING-RMS-AVENUES-ENVRNMENT-COMBINED-AXIS-VIB-PLT-B13  
 SENSOR LOC 8,9,10,11,12,13. COMPRESSION PASS NO. 1





# COMPRESSED VIBRATION DATA

FIG 78

CH-SUB-USA S/N 69-18463

GROSS WT 28100 AND 41900LB AVG CG STA-M10. CONFIC-CLEAN/100/SLING  
 FLT CRAB HANDELWING. PYLONES COMPARTMENT-COMBINED AXIS VIB. PLOT B13  
 SENSOR L00-8-9-10-11-12-13. COMPRESSION PASS NO

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER REJECTION LIMIT

DATA SYSTEM NOISE AT 200 Hz

FREQUENCY Hz

59.9

FIG. 79

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH-54B USA 3/A 89-18463

GROSS WT 28400 LB AVG CG STR MID CONFIG-CLEAN

CMB TEST CMB-CMB/FLT 18EC AVIONICS COMPARTMENT COMBINED DATA VIB-PLAT DAY

SENSOR LOC 8.9.10.11.12.13 COMPRESSION PASS NO. 1

2.0

1.6

1.2

0.8

0.4

0.0

CMB HALF PEAK TO PEAK ACCELERATION G

DATA SYSTEM NOISE AT 2400 Hz

0 50 100 150 200 250 300 350 400 450 500

FREQUENCY Hz

345

FIG 80

## COMPRESSED VIBRATION DATA

CM-548 USA S/N 63-18463

GROSS WT 28400LB AVG CG STR MID CONFIG-CLEAN

CAB TEST 23ND GND/FLT 1BLE RV-ONES-COMPARTMENT-COMBINED-AXIS VIB-PLAT-BIN

SENSOR LOC 849.10-1.12.13. COMPRESSION PASS NO 1

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

ONE HALF PEAK TO PEAK ACCELERATION G

2.0

1.6

1.2

0.8

0.4

0.0

0.0

0 50 100 150 200 250 300 350 400 450 500

FREQUENCY HZ

306

DATA SYSTEM NOISE AT 240HZ



FIG 81

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CP-5168 USA S/N 69-18483  
 CROSS HT 28000 AND 10300.8 AVG CG STP-MID CNF LG-DERN/100/SLING  
 FLT CEND-HOVER PAYLOADS-RFT FUEL/PZL-GEM/AND-AXIS-VIB-PLST-SP18  
 SENSOR 100 10.00.56 SPECIAL PURPOSE COMPRESSION

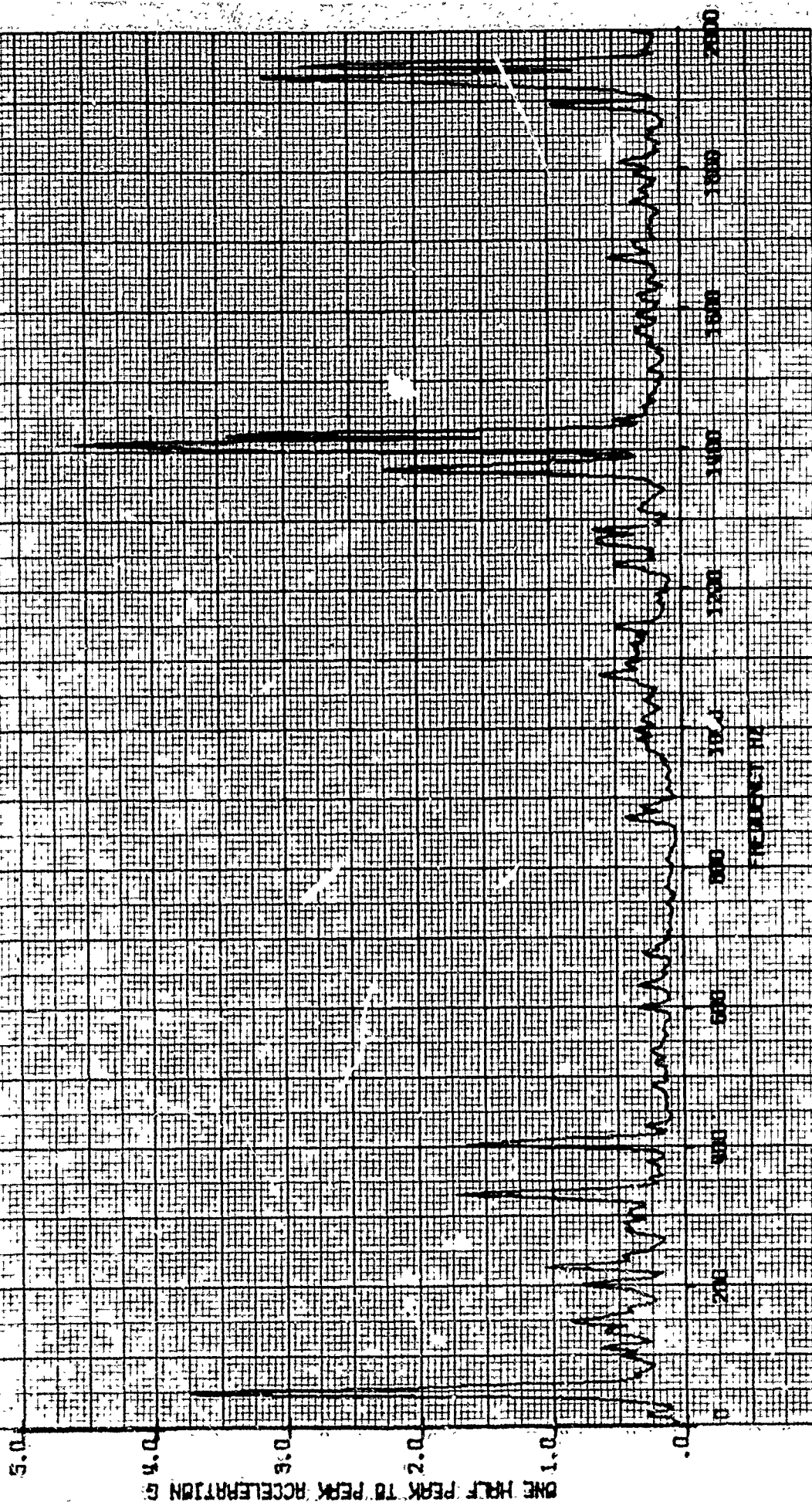


FIG 8.2

## COMPRESSED VIBRATION DATA

EN-508 USH 5/N 69-18463  
 GROSS WT 28400 AND 41500 LB AVG CG STR-MID CONFIG-CLERY/ROUSLING  
 FLT-BOMB-MISSILE PYROGENICS-PT FUSELAGE COMBINED AXIS Y18-PLAT 5015  
 SENSOR LOC 14.48.56 SPECIAL PURPOSE COMPRESSION



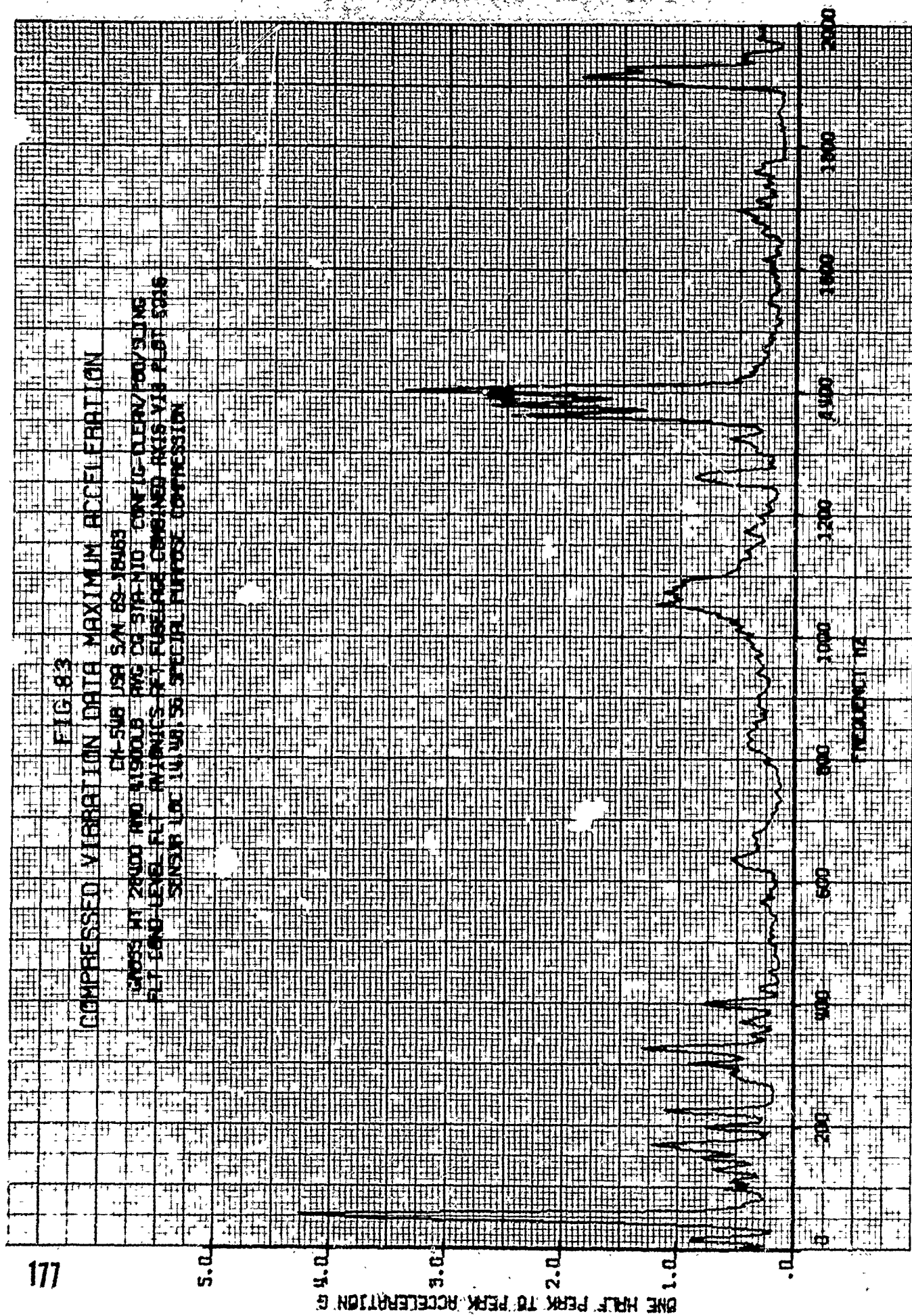




FIG 84

## COMPRESSED VIBRATION DATA

GROSS WT 2400 AND 11500LB. AVE CG STA MID CONF LG-CLEAN/PO/SUNG  
 FLT COND LEVEL FLT. ANALOGICS OFT RELEASED COMBINED AXIS VIB. PLOT 5046  
 SENSOR LOC 14, 143, 55 SPECIAL PURPOSE COMPRESSION

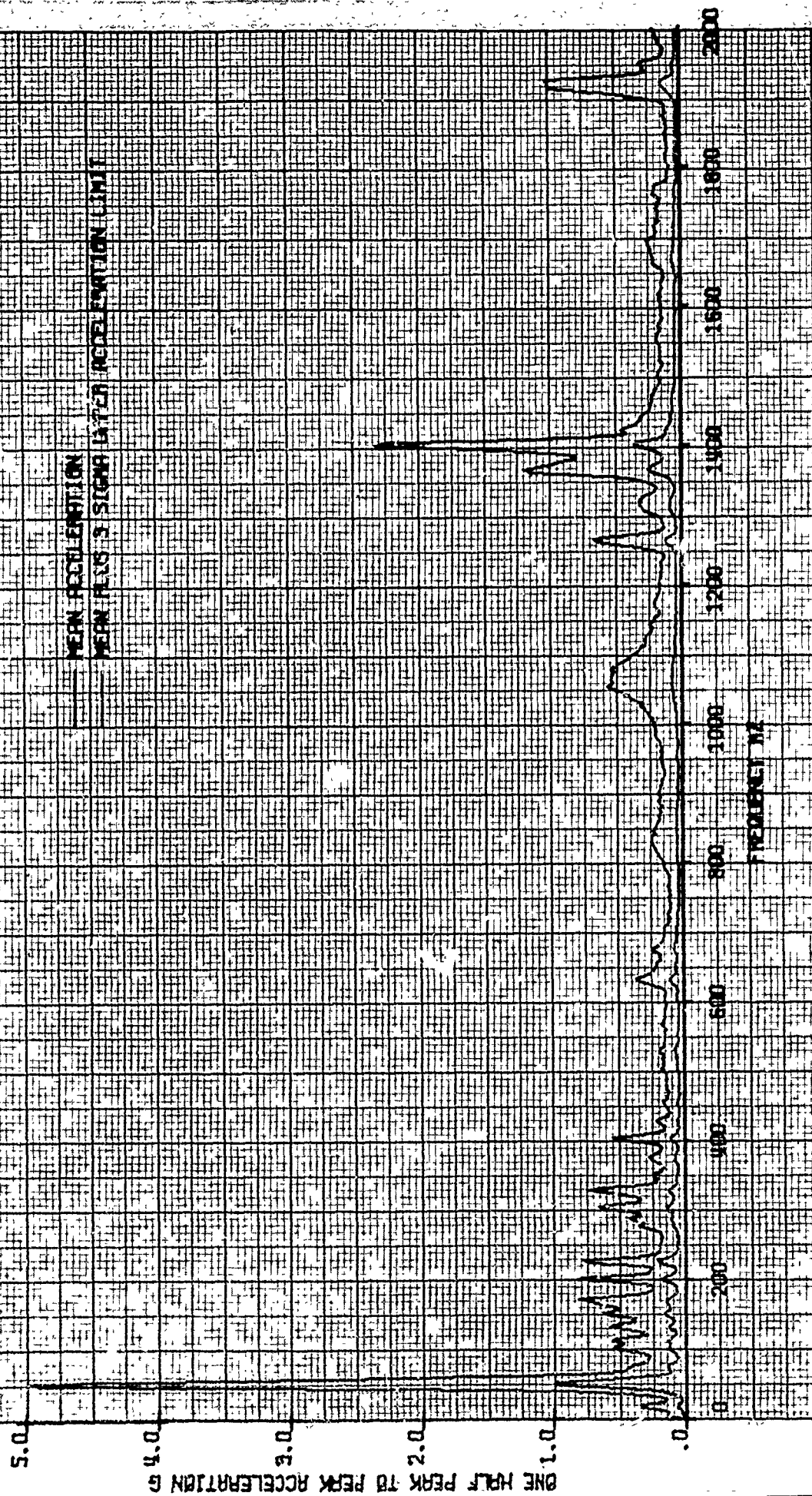


FIG 85

## COMPRESSED VIBRATION DATA MAXIMUM RECELFATION

CH-54B USA 3/A 85-18453  
 CROSS AT 28400 AND 41900LB AVG OF 37A-HIO CONF/G-CLEAN/POO/SLING  
 FLT COND-CLING AVIATIONCS REF-FUSelage-BOMBARDIER AXIS-VIB-1/4G-SD12  
 SENSOR LOC 14, 40, 56 SPECIAL PURPOSE COMPRESSION

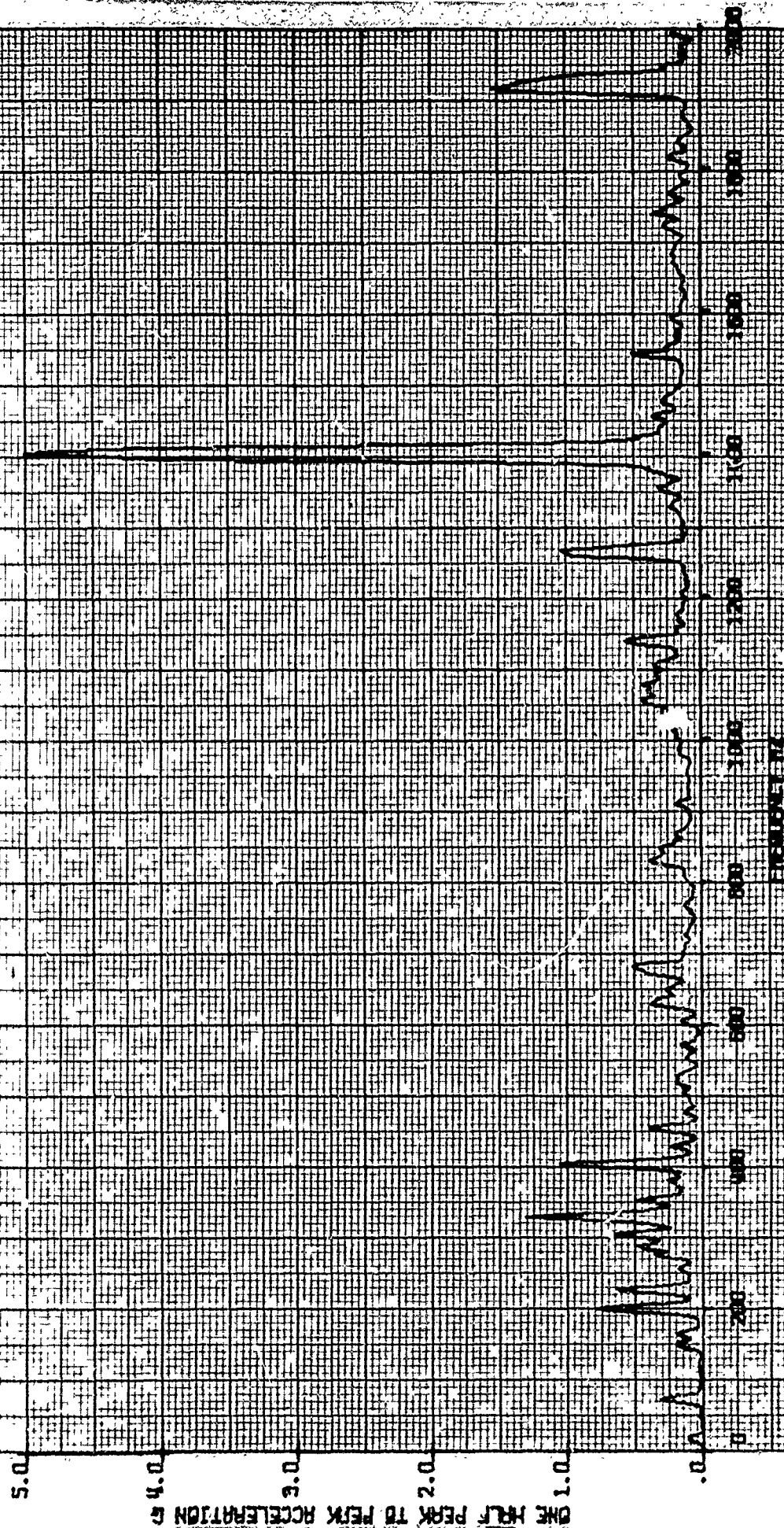


FIG 186

## COMPRESSED VIBRATION DATA

CROSS AT 2000 AND 11500 Hz. AVG OF STR-110 CONF/G-TOEN/POD/SLING  
 FLT 3000-0 TIME AVERAGE REF FUSELAGE COMBINED AXES Y18 FLT 501.2  
 SENSOR LOC 11410156 SPECIAL PURPOSE COMPRESSION

5.0

4.0

3.0

2.0

1.0

0.1

ONE HALF PEAK TO PEAK ACCELERATION G

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

0

100

200

300

400

500

600

700

800

900

1000

TIME (SECONDS)



FIG. 87

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

E4-5UB USA S/N 89-18483

GROSS WT 20400 LBS AVG CA 572-H10 CONFIG-DL2AV/DO/LINE

FET COND-BESENT - RIVETES-FLASHER-BOUNDED-8X15 VIB-R37-5318

SENSOR LOC 10.00.56 SPECIAL PURPOSE COMPRESSION

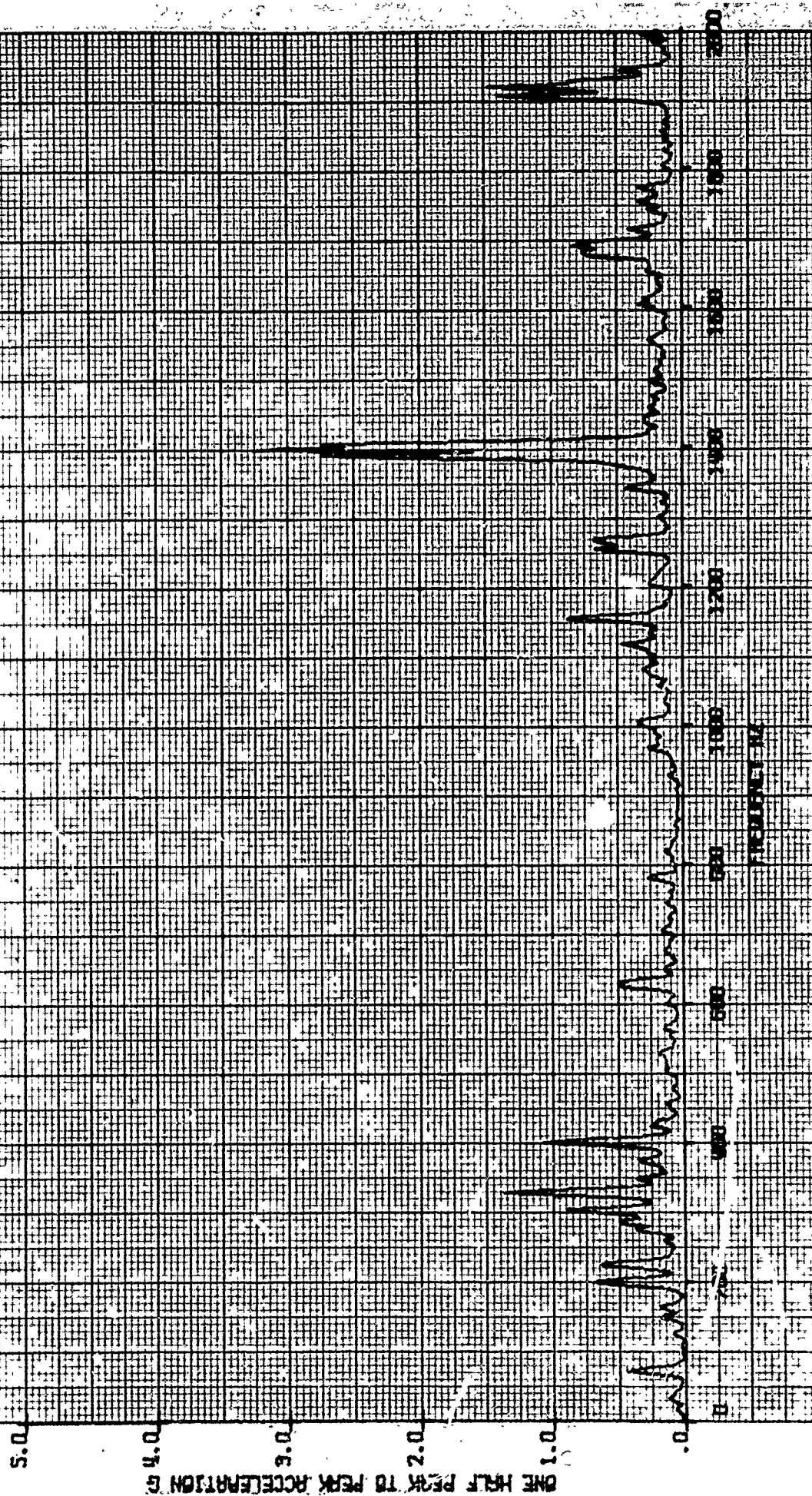


FIG 88

## COMPRESSED VIBRATION DATA

CH-53B USN SN 29-10463

GROSS WT 24000 LBS 41000 LB AVG CG STR-110 CMFG-CLEW/TOW/LINE

FLT COND-DESENT AVIATION FUEL/RE CONSUMED 3000 YIB FLT 5018

SENSOR LOC IN W. 56 SPECIAL PURPOSE COMPRESSION

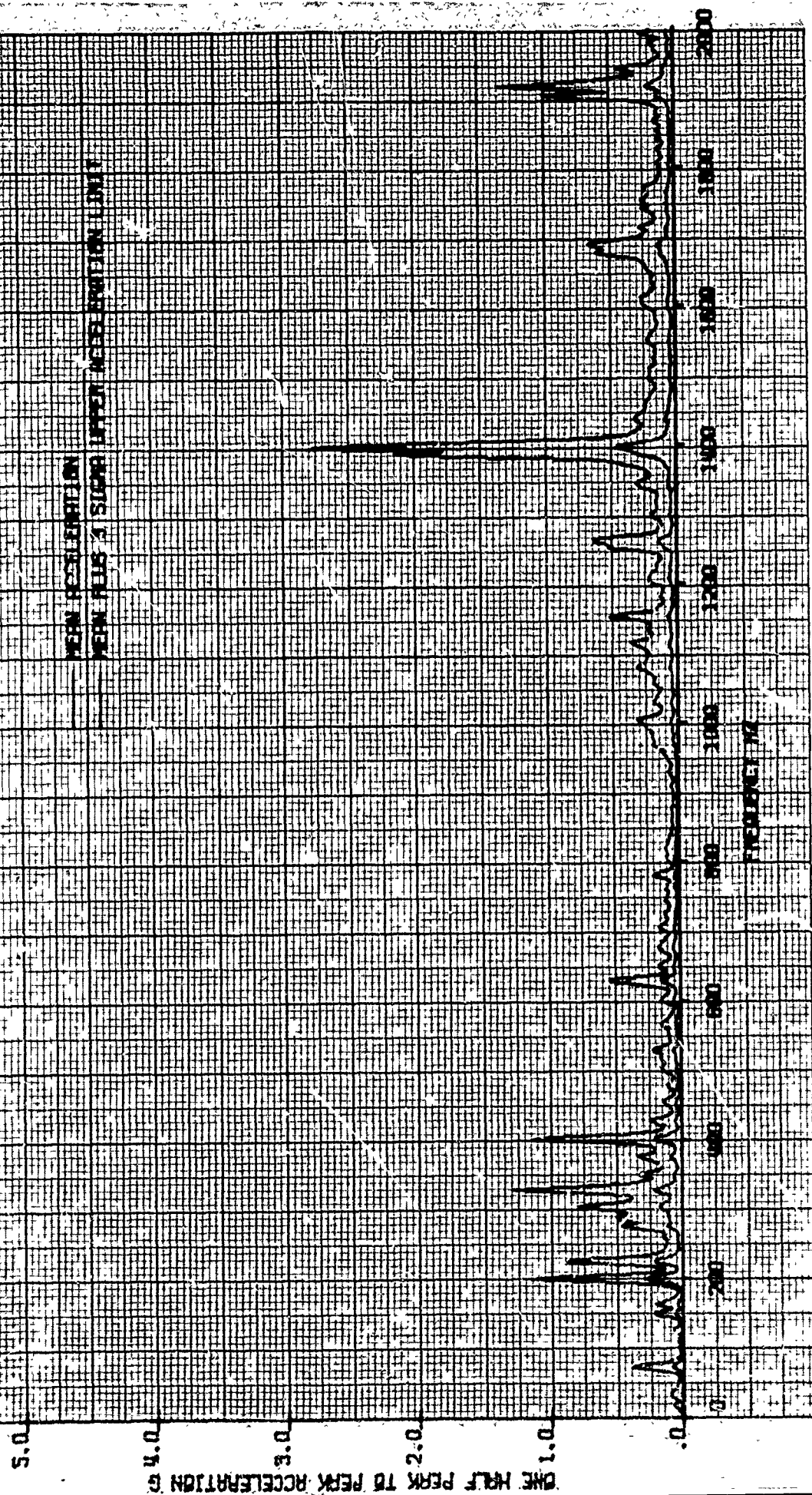
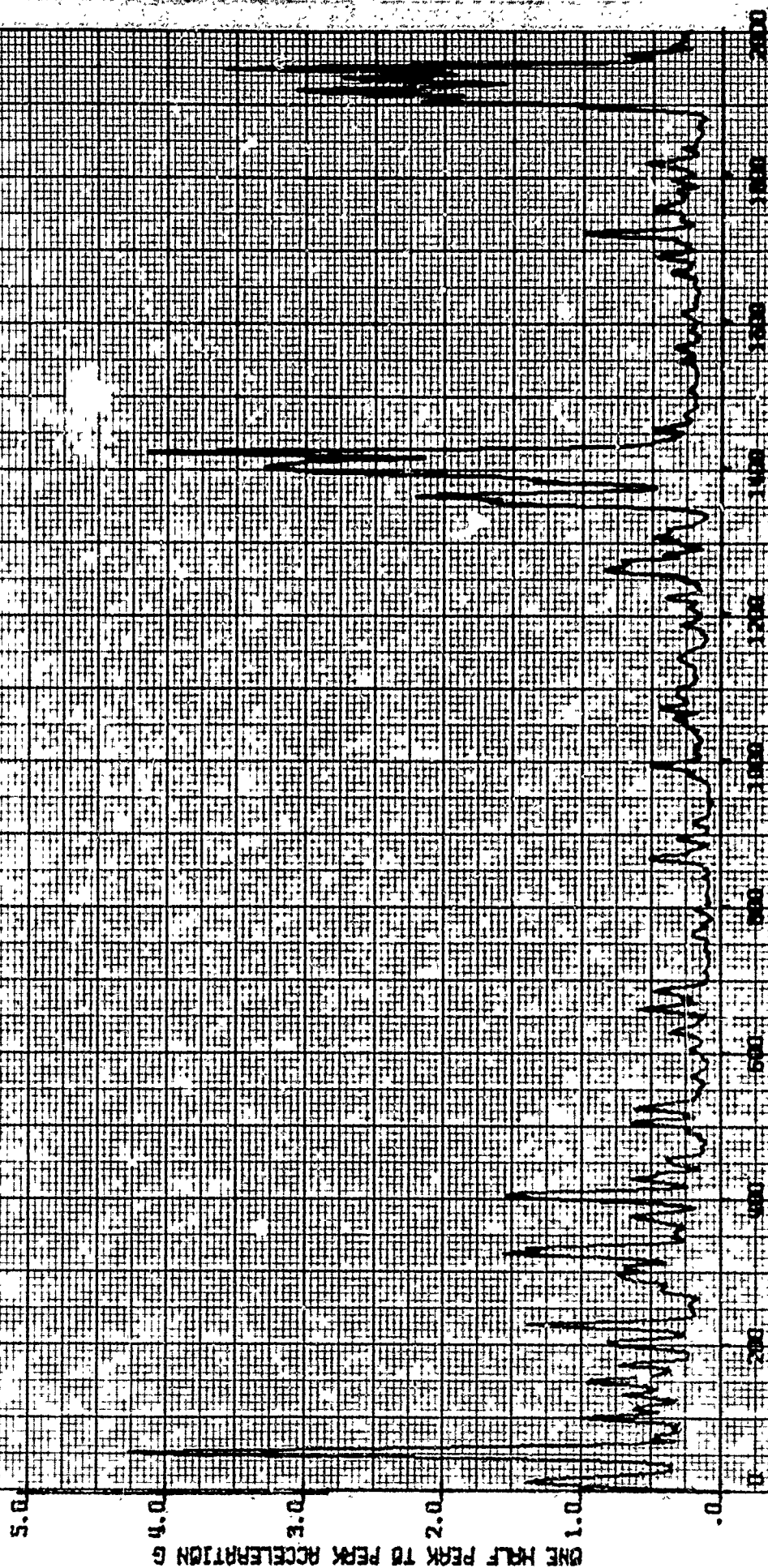


FIG 89

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CP-508 USA 5N 68-10653

GROSS WT 28400 AND 41900.0 AVG CG STA-110 CONF (G-OBSERVATIONS) LING  
 FET 2000-179 ONE LRG ANALOGIES AFT FUSE ARE COMBINED IN L5-VIB PLATE 5019  
 SENSOR LOC IN LUG 56 SPECIAL PURPOSE COMPRESSION





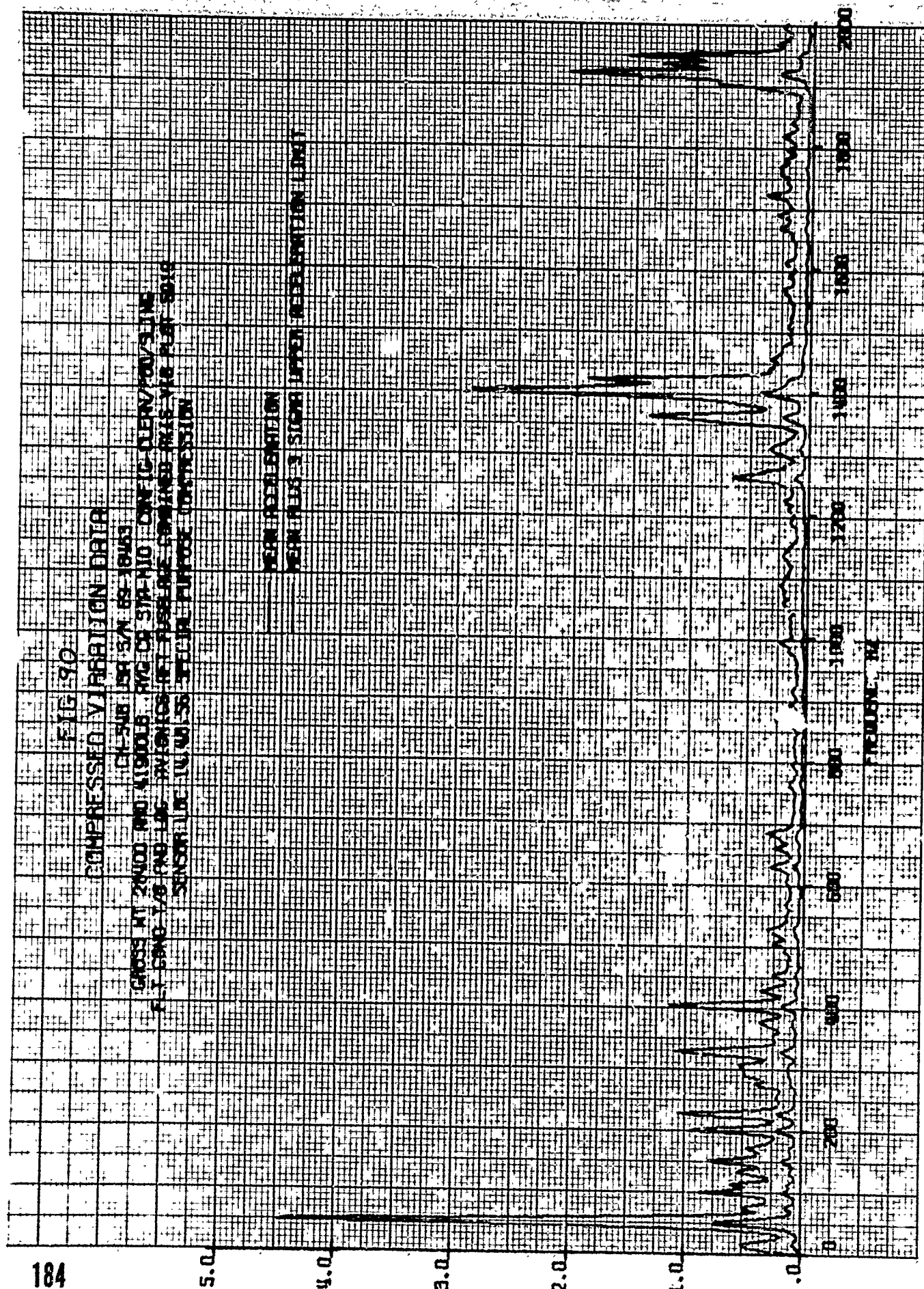


FIG. 91

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH-548 JSA SA 89-18463  
 GROSS WT 2000 LBS VISUAL AVG DE STR-HIG LINE-IG-BURN/TOUSLING  
 P.T. CONO-MEASURING ANALYSIS RET FUSE-AGE COMBINED THIS WAS FOR 3000  
 SENSOR LOG-ILL-40.55 SPECIAL PURPOSE COMPRESSION

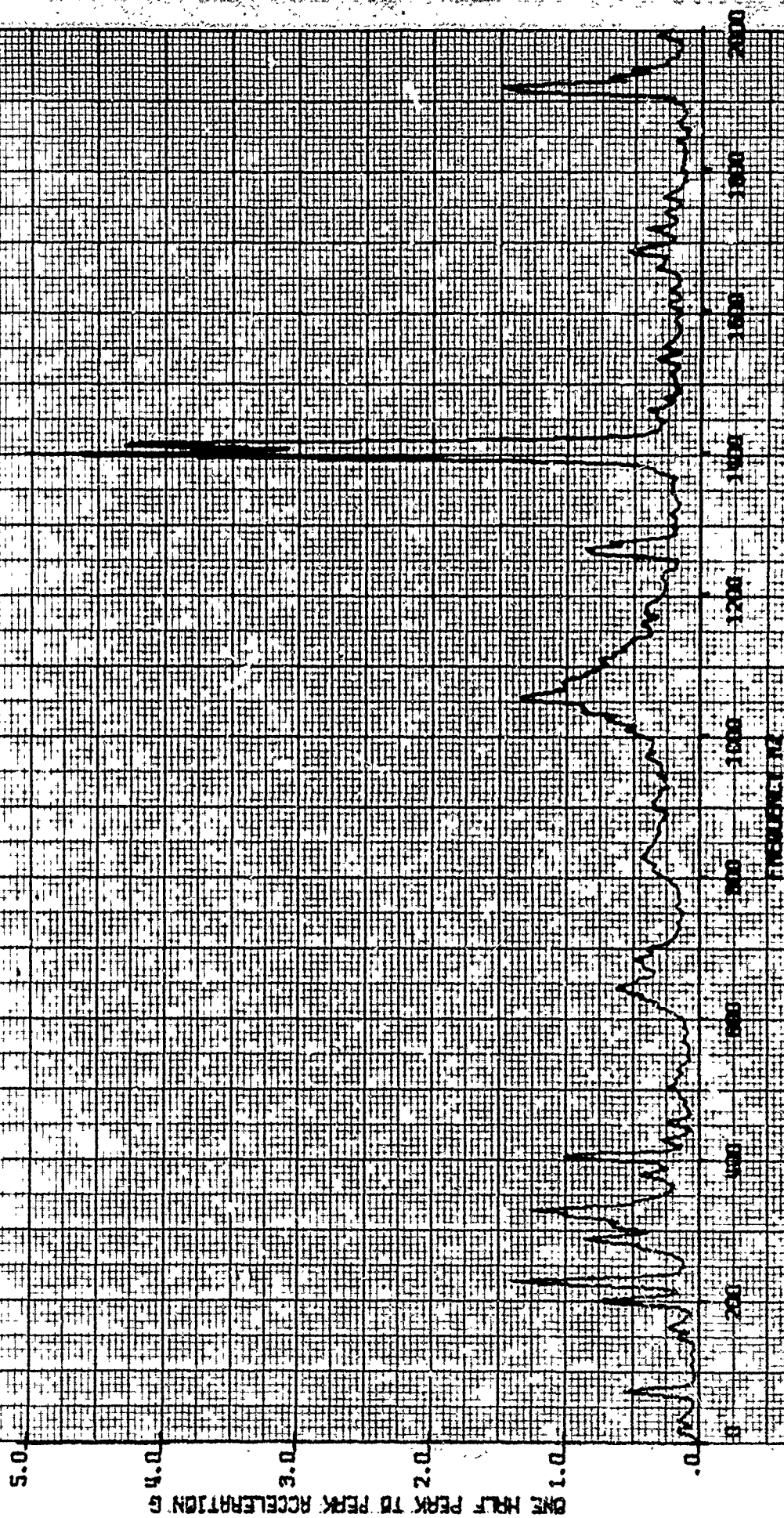


FIG 92

## COMPRESSED VIBRATION DATA

CR-500 FOR 5/1/69-10/69/3  
 CROSS MT 28000 AND 110000.8 AVG OF 5/1/69-10/69/3  
 FLT END-MANAGEMENT HYDRAULICS RET-FUSelage-ENGINEED-JETS-VIB-FLAT-5000  
 SENSOR LOC 10/10/56 SPECIAL PURPOSE COMPRESSION

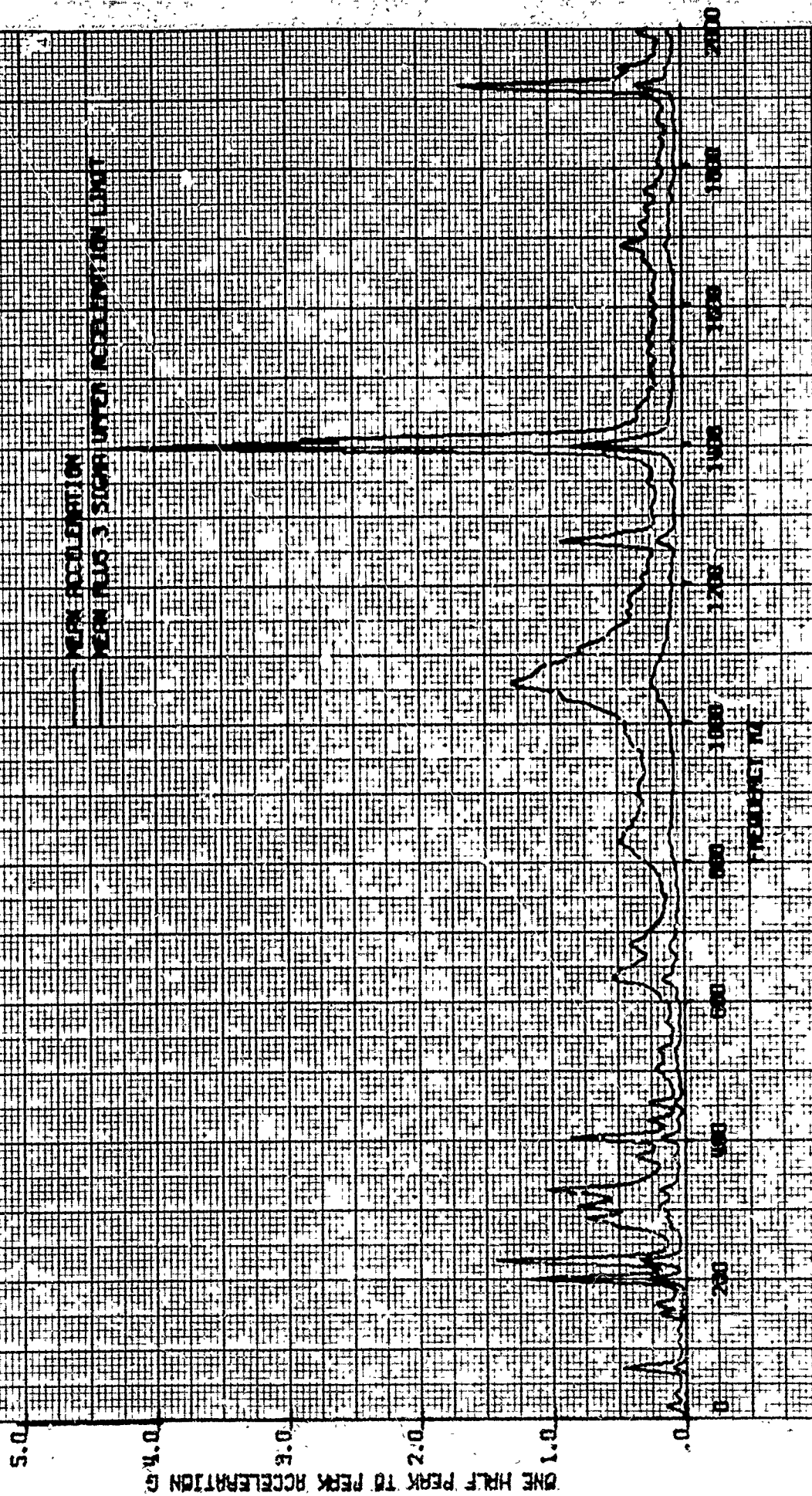




FIG 93

## COMPRESSED VIBRATION DATA MAXIMUM RECELERATION

CP-548 USA S/N 60-10463

GROSS WT 2800 LB AVE LG 51 IN HCU CONFIG-CLERM

CNO TEST CNO-CNO/FLT 10.5 INCHES-PT FLARE-AGE COMBINED 10.15 VIB 6.00-5000

SENSOR LOC 10.48.55 SPECIAL PURPOSE COMPRESSION

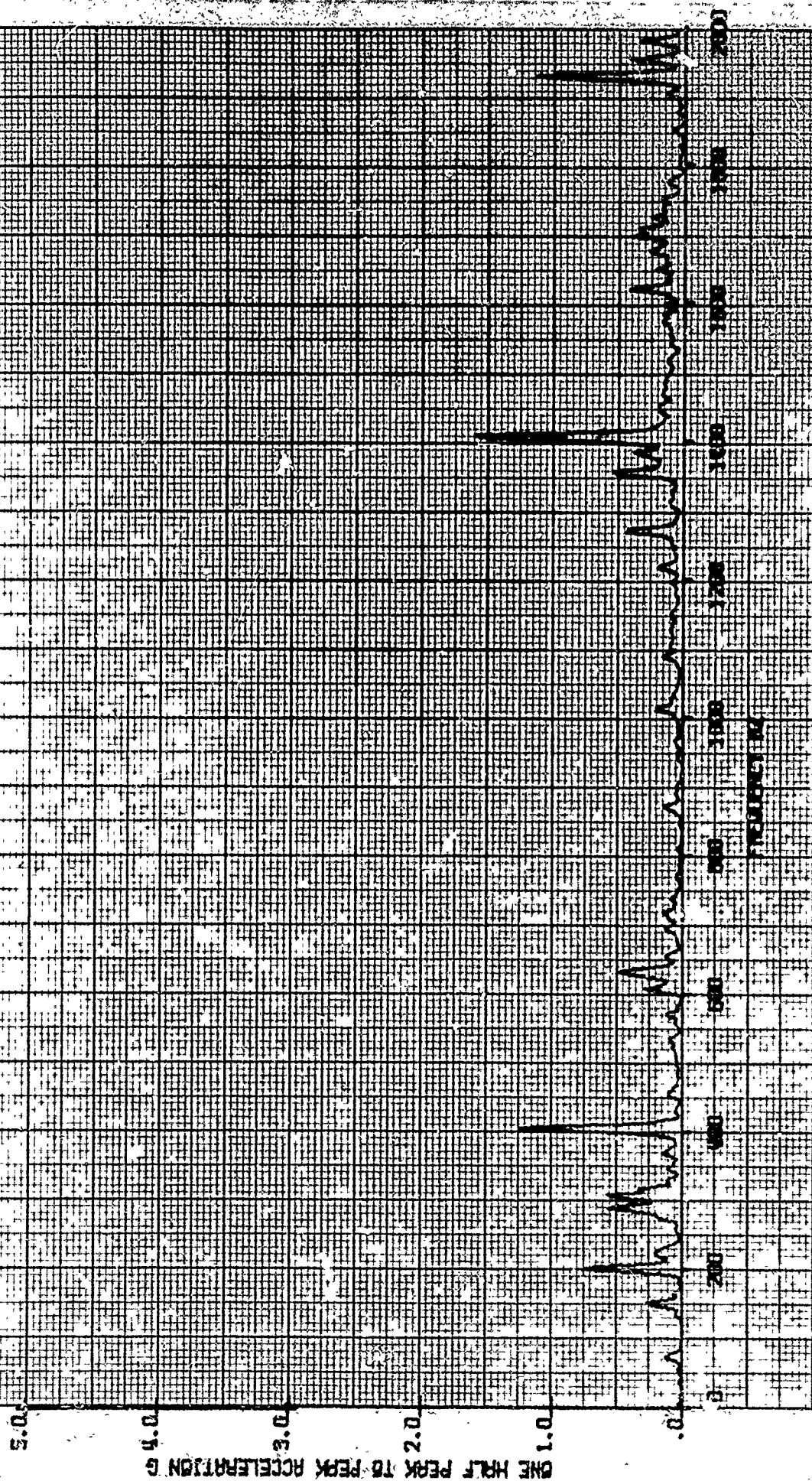


FIG 94

## COMPRESSED VIBRATION DATA

CA-500 100 SA 80 DEWES

CROSS 77 2000000 HVE DC 510 AND DOWSIC-CLERK

CAO TEST COND-CAO/AL 7-100E RULONICS-DET FIBER ARE COMBINED 0213 VIB ALON 302A

SENSOR 110C 100/500 SYSTEM PURPOSE COMPRESSION

5.0

4.0

3.0

2.0

1.0

0

ONE HALF PEAK TO PEAK ACCELERATION G

RAW ACCELERATION

RAW PLUS 3 SIGMA UPPER ACCELERATION LIMIT

0

200

400

600

800

1000

1200

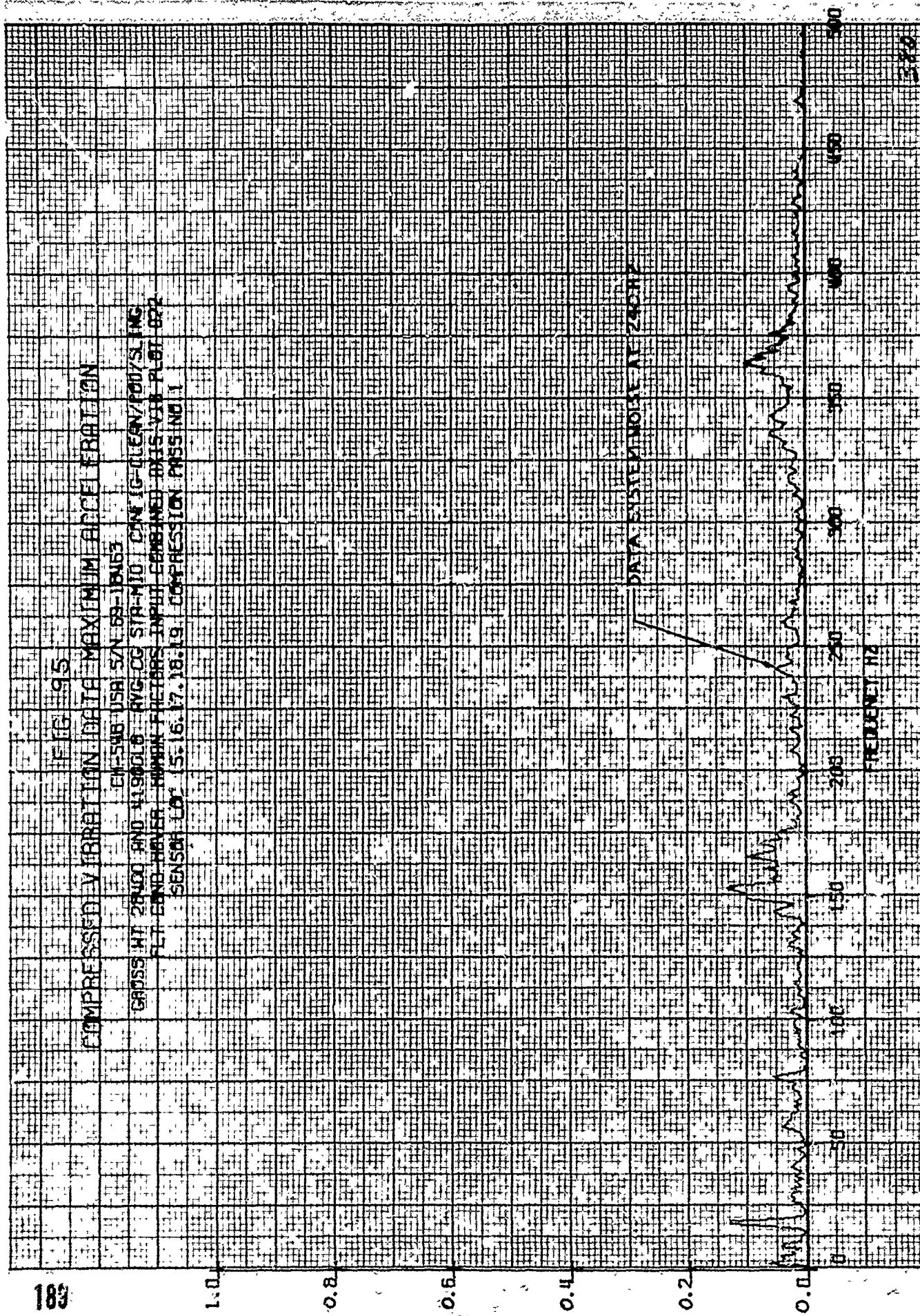
1400

1600

1800

2000

FREQUENCY Hz





**REVIEW**

CONF-IG-CLEAN/900/SLING

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5.16.17.18.19	COP REC	IN 285 NO 1
SENSOR LOC		

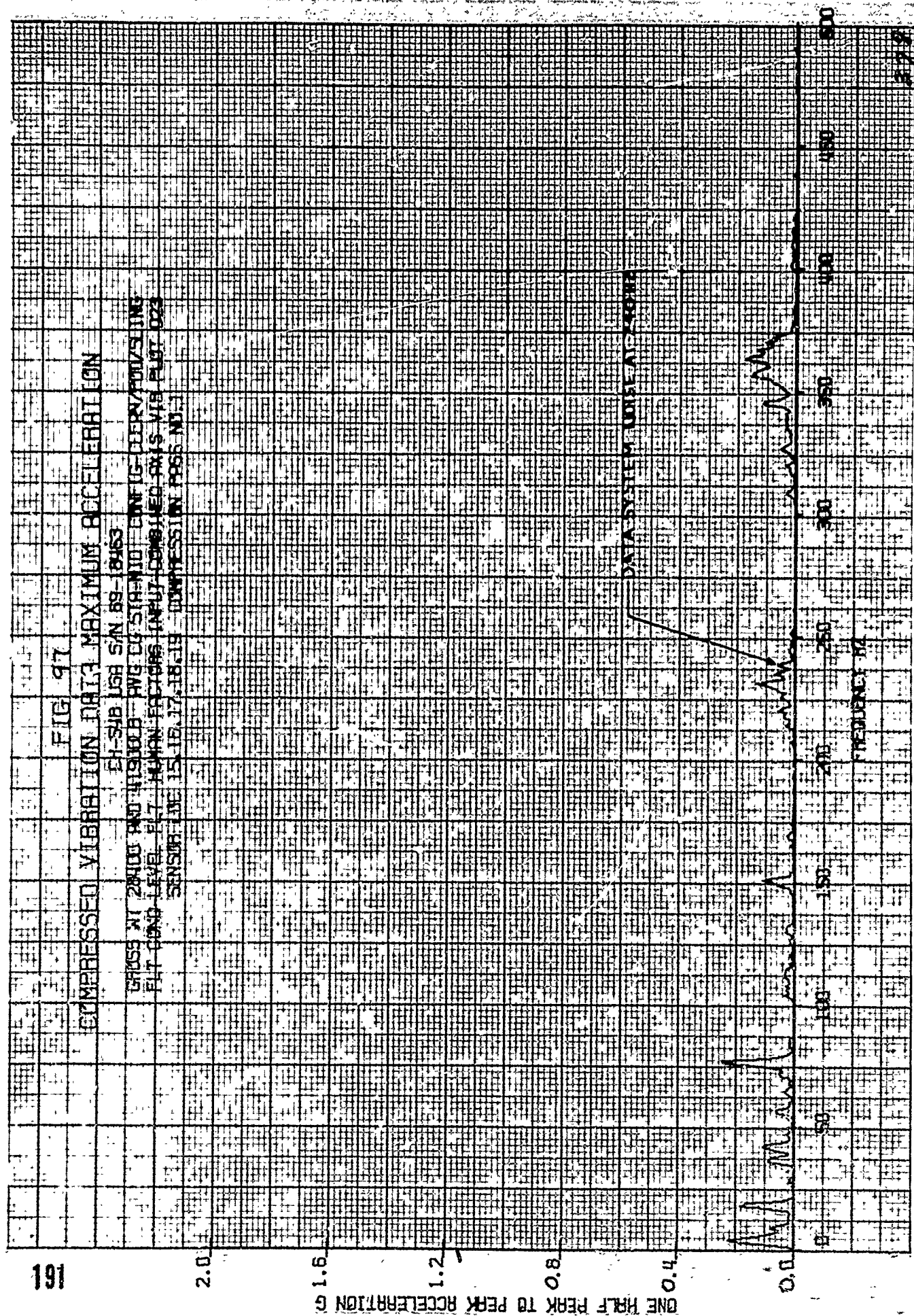
**G**

74	2	59	6	2	72	5	57	7
75	3	60	7	3	73	6	58	8
76	4	61	8	4	74	7	59	9
77	5	62	9	5	75	8	60	10
78	6	63	10	6	76	9	61	11
79	7	64	11	7	77	10	62	12
80	8	65	12	8	78	11	63	13
81	9	66	13	9	79	12	64	14
82	10	67	14	10	80	13	65	15
83	11	68	15	11	81	14	66	16
84	12	69	16	12	82	15	67	17
85	13	70	17	13	83	16	68	18
86	14	71	18	14	84	17	69	19
87	15	72	19	15	85	18	70	20
88	16	73	20	16	86	19	71	21
89	17	74	21	17	87	20	72	22
90	18	75	22	18	88	21	73	23
91	19	76	23	19	89	22	74	24
92	20	77	24	20	90	23	75	25
93	21	78	25	21	91	24	76	26
94	22	79	26	22	92	25	77	27
95	23	80	27	23	93	26	78	28
96	24	81	28	24	94	27	79	29
97	25	82	29	25	95	28	80	30
98	26	83	30	26	96	29	81	31
99	27	84	31	27	97	30	82	32
100	28	85	32	28	98	31	83	33
101	29	86	33	29	99	32	84	34
102	30	87	34	30	100	33	85	35

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# IDENTIFICATION OF COMBINED VIBRATION DATA

CH	S	B	USA	5	A	68	1	8453							
BRASS	WT	2400	AND	4190	LB	WGT	CG	STAR	NO	CONF	IS	LEAV	700	5	INC
FLT	COND	LEAD	FLT	MUN	FACTORS	NEWLY	COMBINED	EX	S	WIS	PLST	023			
SEN	30A	IN	15	16	17	18	19	EXPRESS	ON	PRE	MI				

FOR CASH IN  
NEW U.S. & SINGAPORE EXCHANGE

# STRENGTHEN YOUR EXERCISE



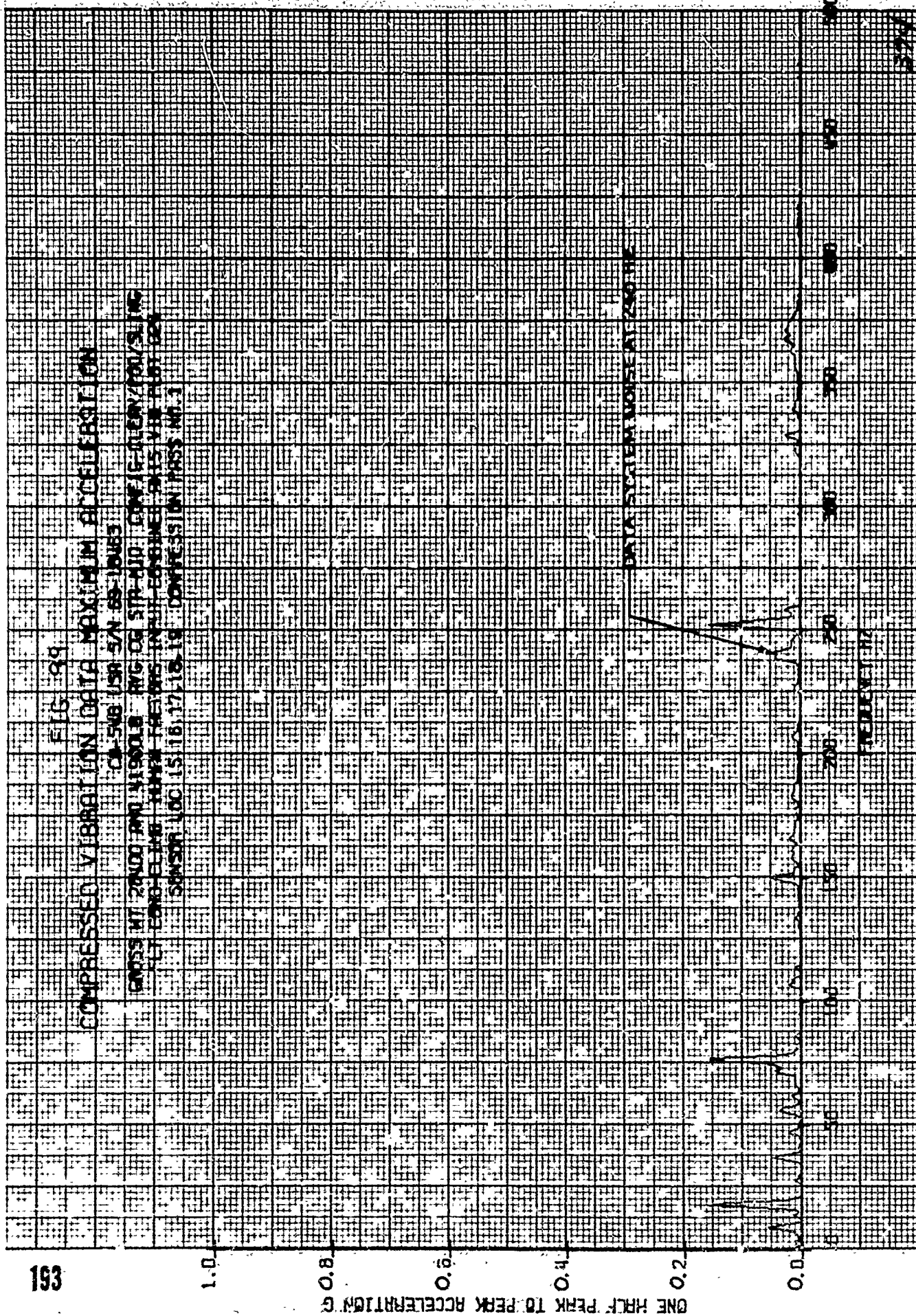


FIG. 100

## COMPRESSED VIBRATION DATA

CH-54B USR 5/4 89-18453  
 CROSS MT 204001 RND 4190013 AVG CG 570-N10 CONFIG-CLEAV/POO/SLINK  
 FLT EMBD-ELPHB HUMAN-FAITHRES-INDIA-EMB-MED-BRES-VIB-8-81-124  
 SENSOR JUL 15 16 17 18 19 COMPRESSION PRESS NO. 1

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER REGULATION LIMIT

ONE HALF PEAK TO PEAK ACCELERATION G

DATA SYSTEM NOISE AT 200 Hz

FREQUENCY IN

300



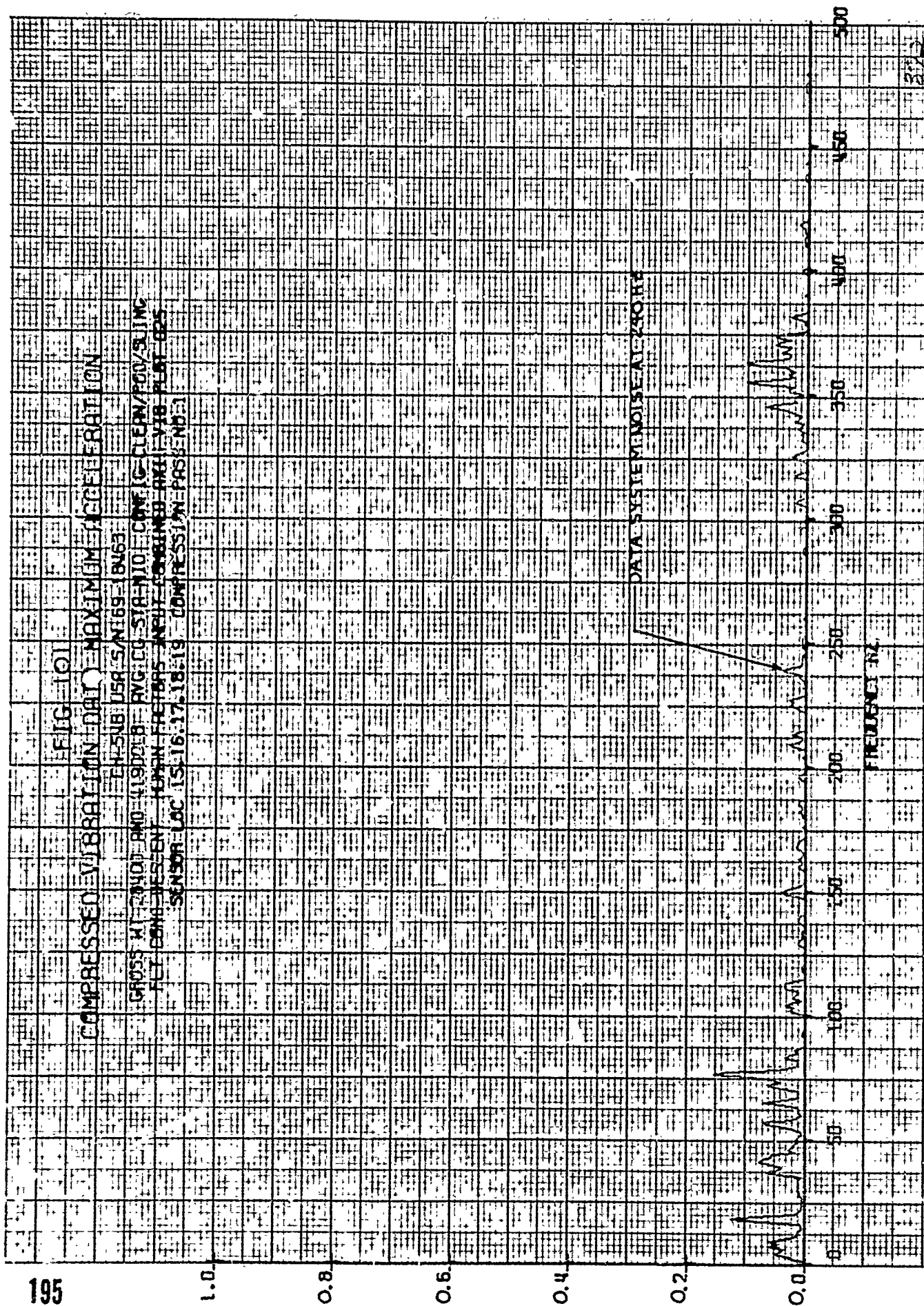


FIG 102

COMPRESSED VIBRATION DATA

GROSS AT 20400 AND 41900LB AVG CG STA-M10 CONF (G-CLEM/POD/S/LING  
 FLY COMB-DESECT TEMPN FRETORS INPHY-COMBINED-AXIS-VIB PLAT-025  
 SENSOR LOC 15 16 17 18 19 (CONF-SESSION-PASS-NO-1)

CH-SNB USH-S/N-69-18463

1.0

0.8

0.6

0.4

0.2

0.0

ONE HALF PEAK TO PEAK ACCELERATION G

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER REGENERATION LIMIT

DATA SYSTEM NOISE AT 220HZ

FREQUENCY HZ

500

450

400

350

300

250

200

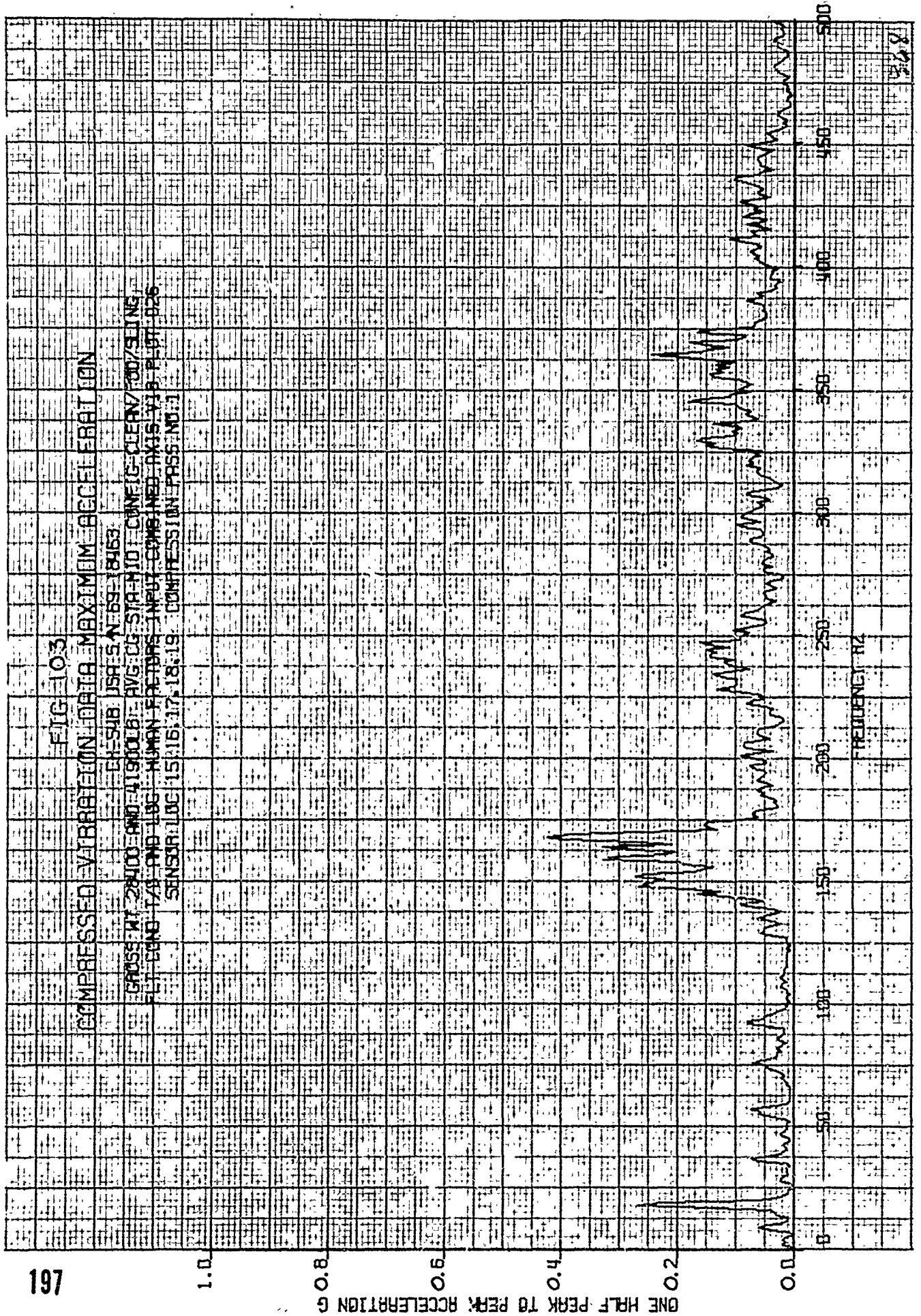
150

100

50

877





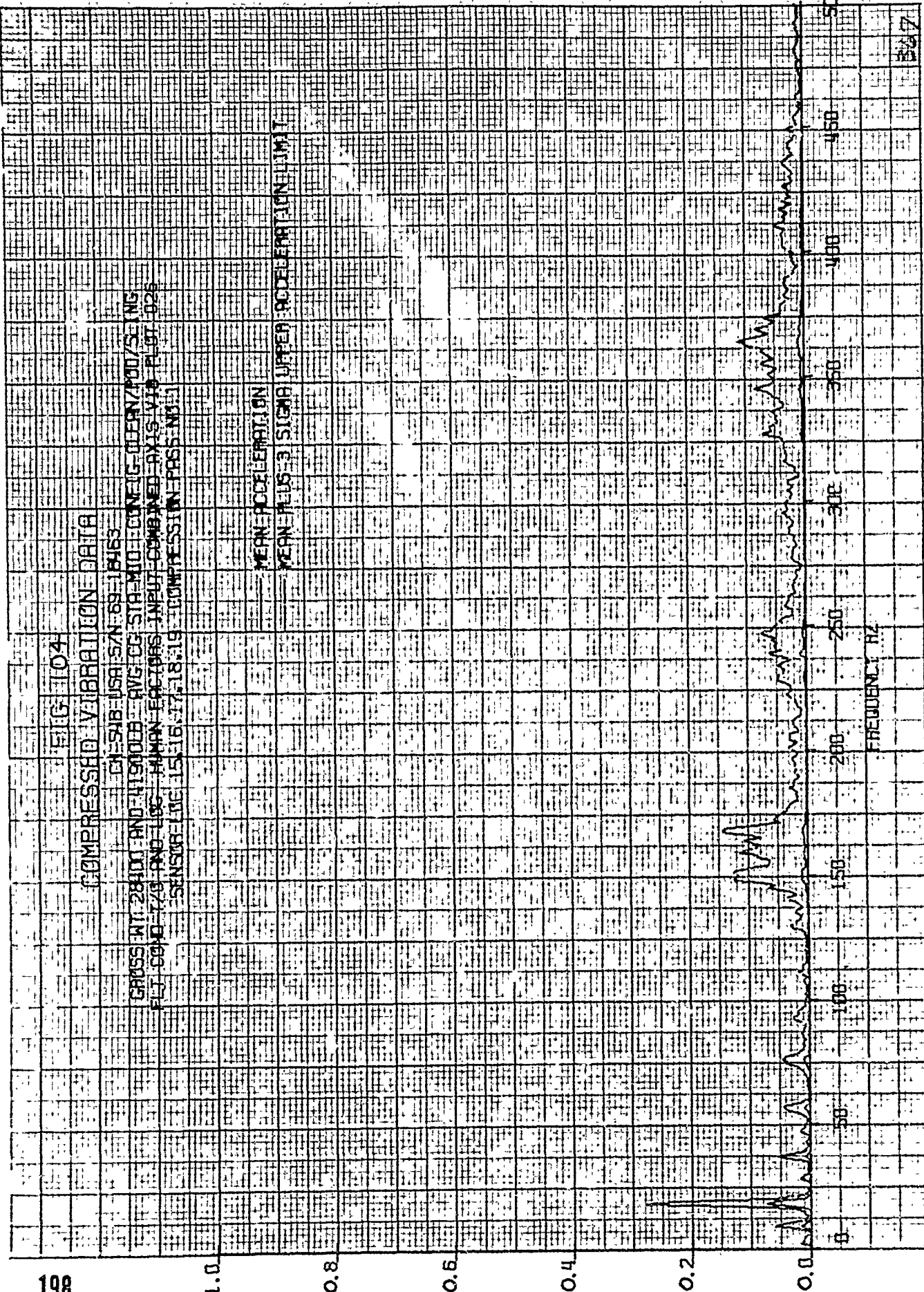
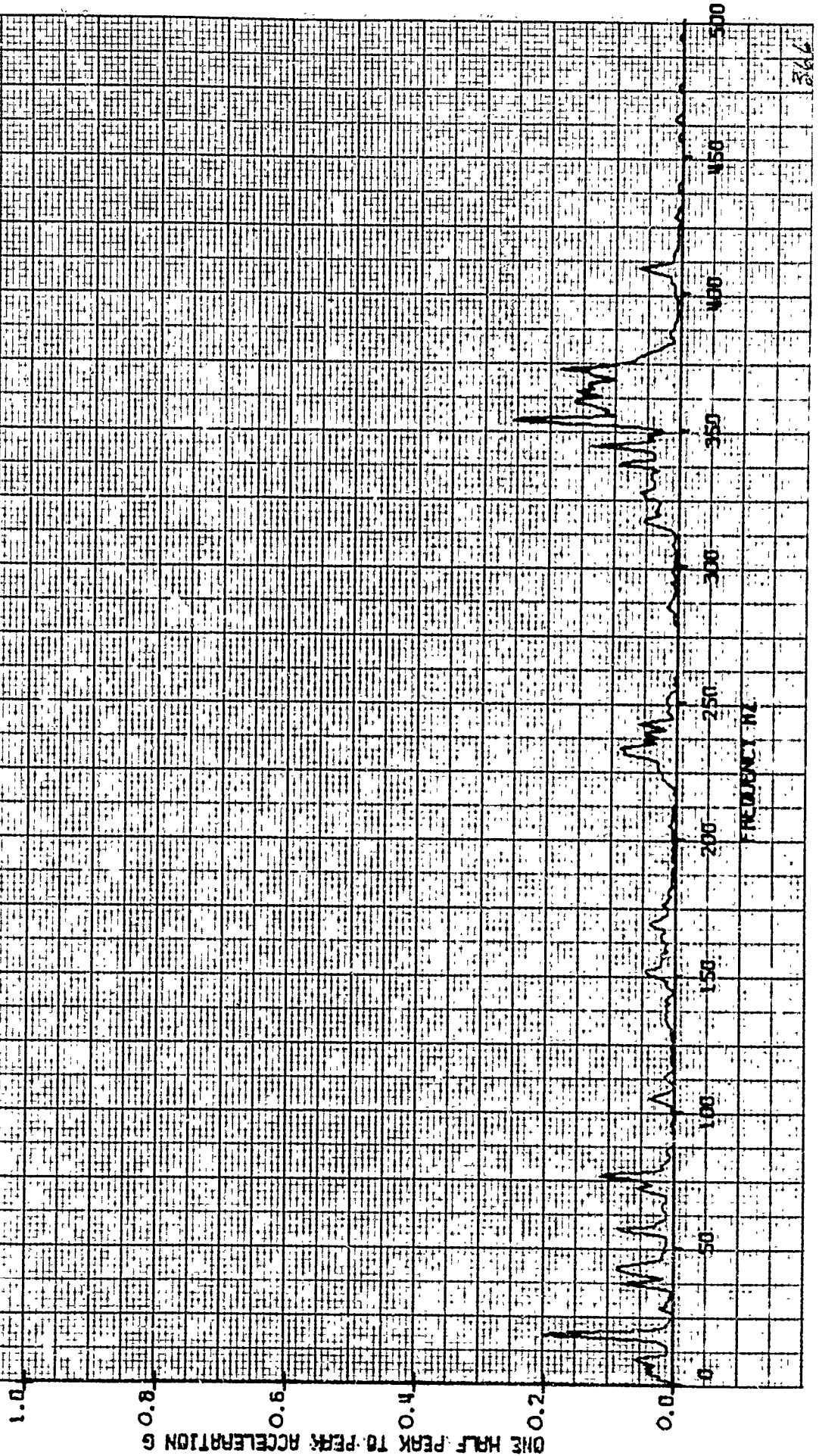


FIG 105  
COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

GROSS WT 2000 LBS. AVG CG STRAIN CONE 16-CLERN/POD/SLING  
FLY EMB-MEWELEVERING HUMAN FREPPS INPUT COMBINED AXIS VIB PLAT 027  
SENSOR LOC 15,16,17,18,19 COMPRESSION PASS NO. 1





200

1.0

0.8

0.6

0.4

0.2

ONE HALF PEAK TO PEAK ACCELERATION G

FIG 106

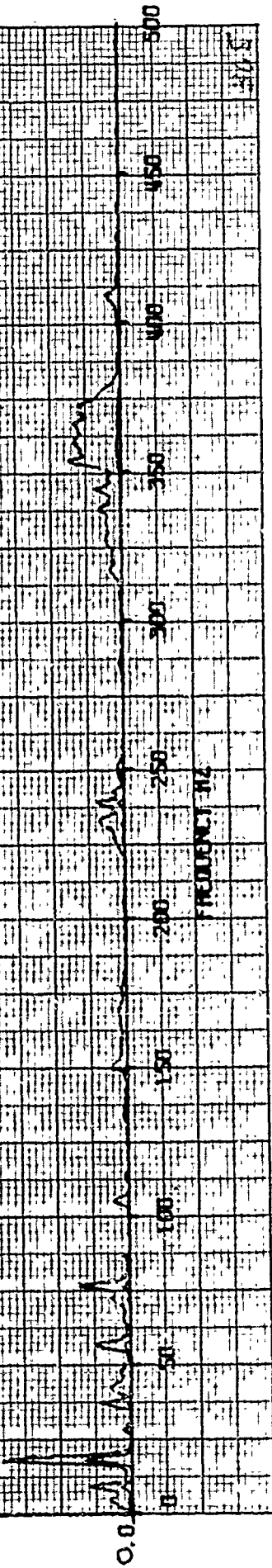
COMPRESSED VIBRATION DATA

GROSS WT 20400 LBS - 11900 LBS  
 CH-540 USA S/N 69-18463  
 AVG CG STA-N10 CME (G-CLEAN/F00/SLING)  
 FCT EONG NONSUSPENDING HUMAN FRETTING INPUT COMBINED AXIS-VIB PLOT 827  
 SENSOR LOC 15, 16, 17, 18, 19 COMPRESSION PASS NO. 1

MEAN ACCELERATION

MEAN PLUS 3 SIGMA

UPPER ACCELERATION LIMIT



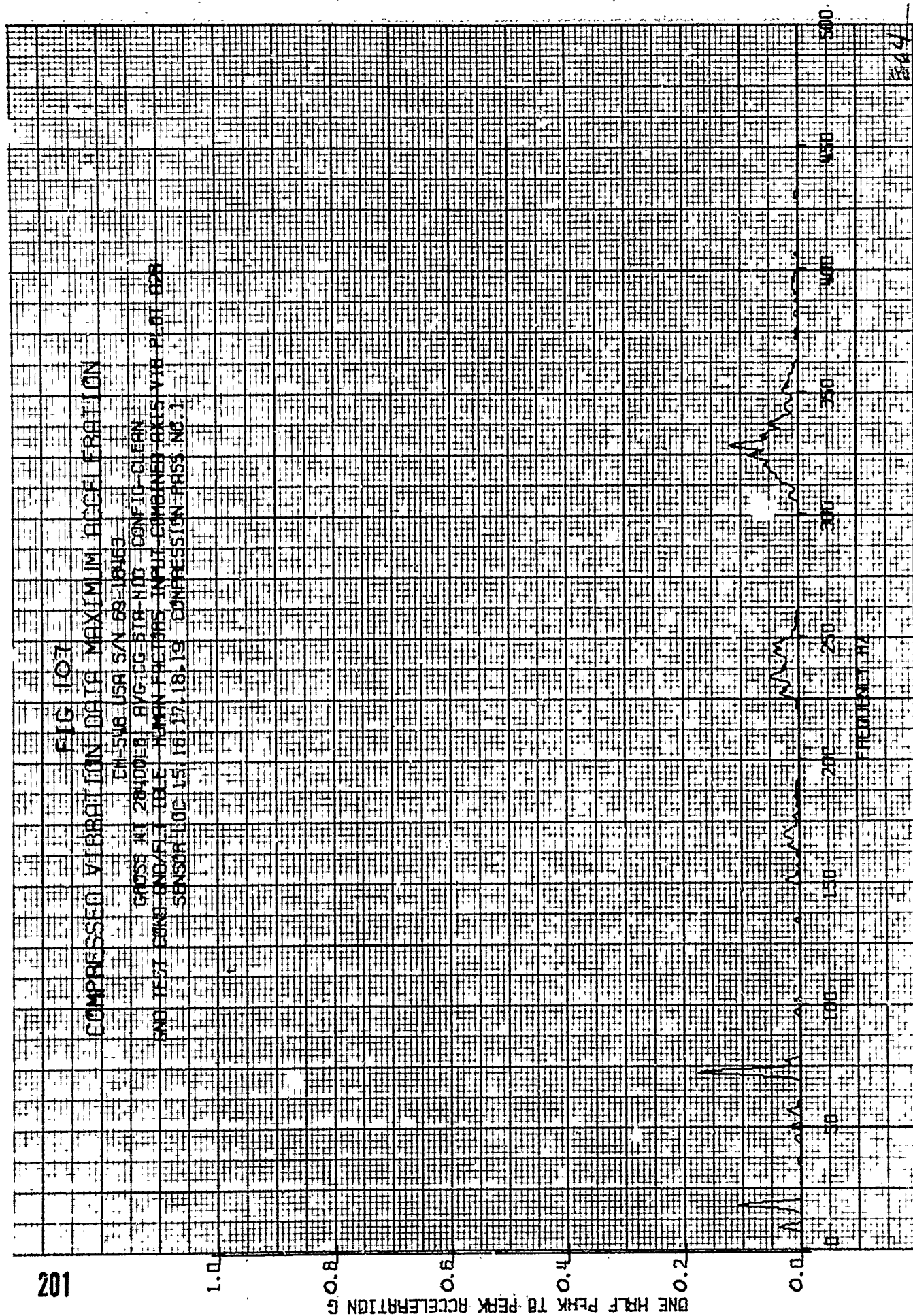




FIG 108

## COMPRESSED VIBRATION DATA

CH 546 USA S/N 69-18463

GROSS WT 28400 LB AVG CG 379-M.D. COMF 10-C-CLON

SMB TEST COMB ENG/EL 1-BLE HUMAN FACTORS IMPUL COMBINED AXES VIB-PLAT-DRG

SENSOR LOC 15-16, 17, 18, 19 COMPRESSION PASS NO 1

1.0

0.8

0.6

0.4

0.2

0.0

ONE HALF PEAK TO PEAK ACCELERATION G

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

0

50

100

150

200

250

300

350

400

450

500

FREQUENCY HZ

243

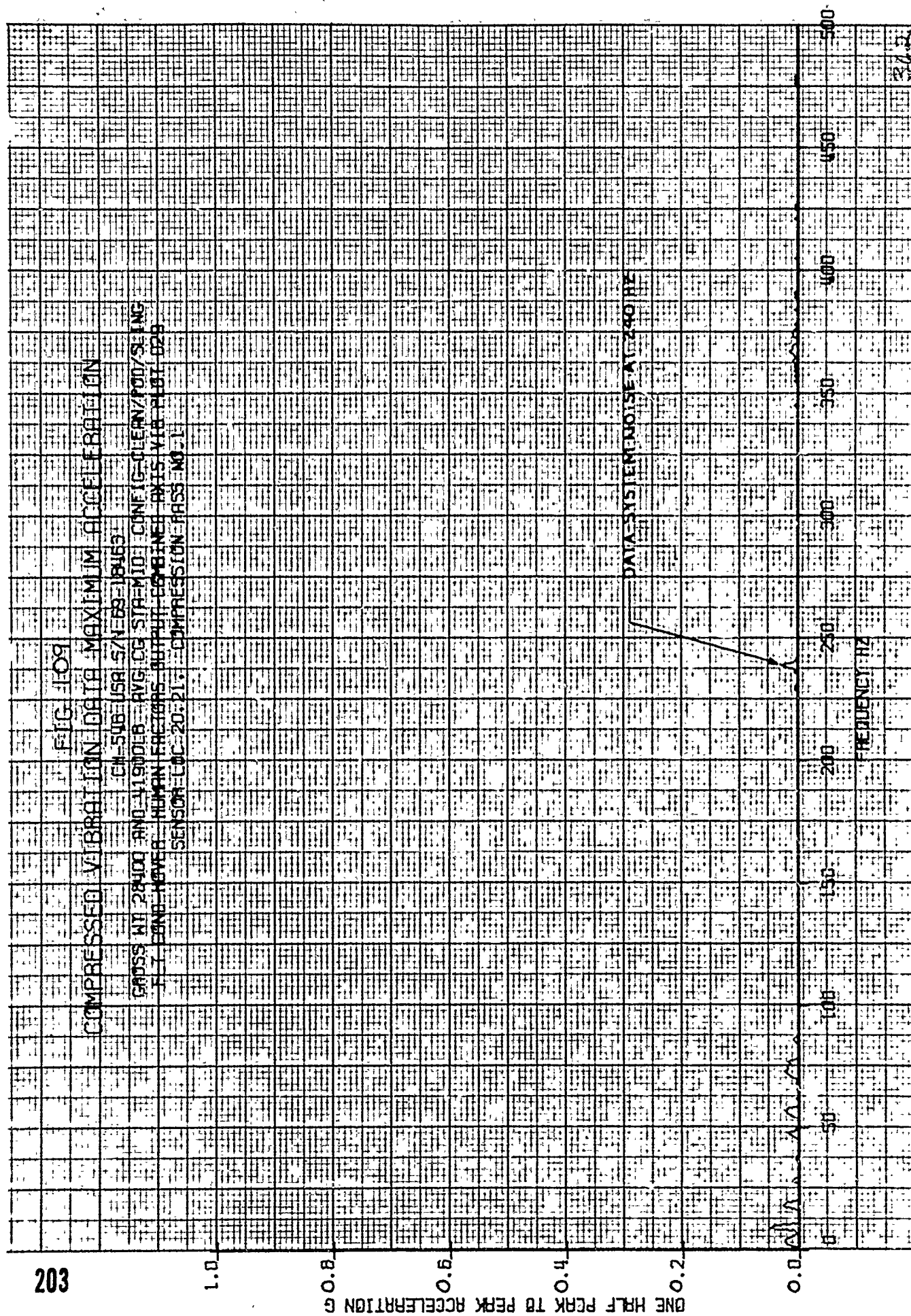


FIG 11.0

## COMPRESSED VIBRATION DATA

CR-546 USA S/N 69-18463

LG055 AT 28400 RPM VIBRO-B AVG LG STR-HIO CONFID-CLERY/100/SLING

FLY CONB-TOVER HUMAN FACTORS OUTPUT COMBINED AXIS Y10 P-01 029

SENSOR LOC-20-D11 COMPRESSION PASS NO-11

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

DATA SYSTEM NOISE AT 250 Hz

FREQUENCY Hz

0

50

100

150

200

250

300

350

400

450

500

550

600

650

700

750

800

850

900

950

1000



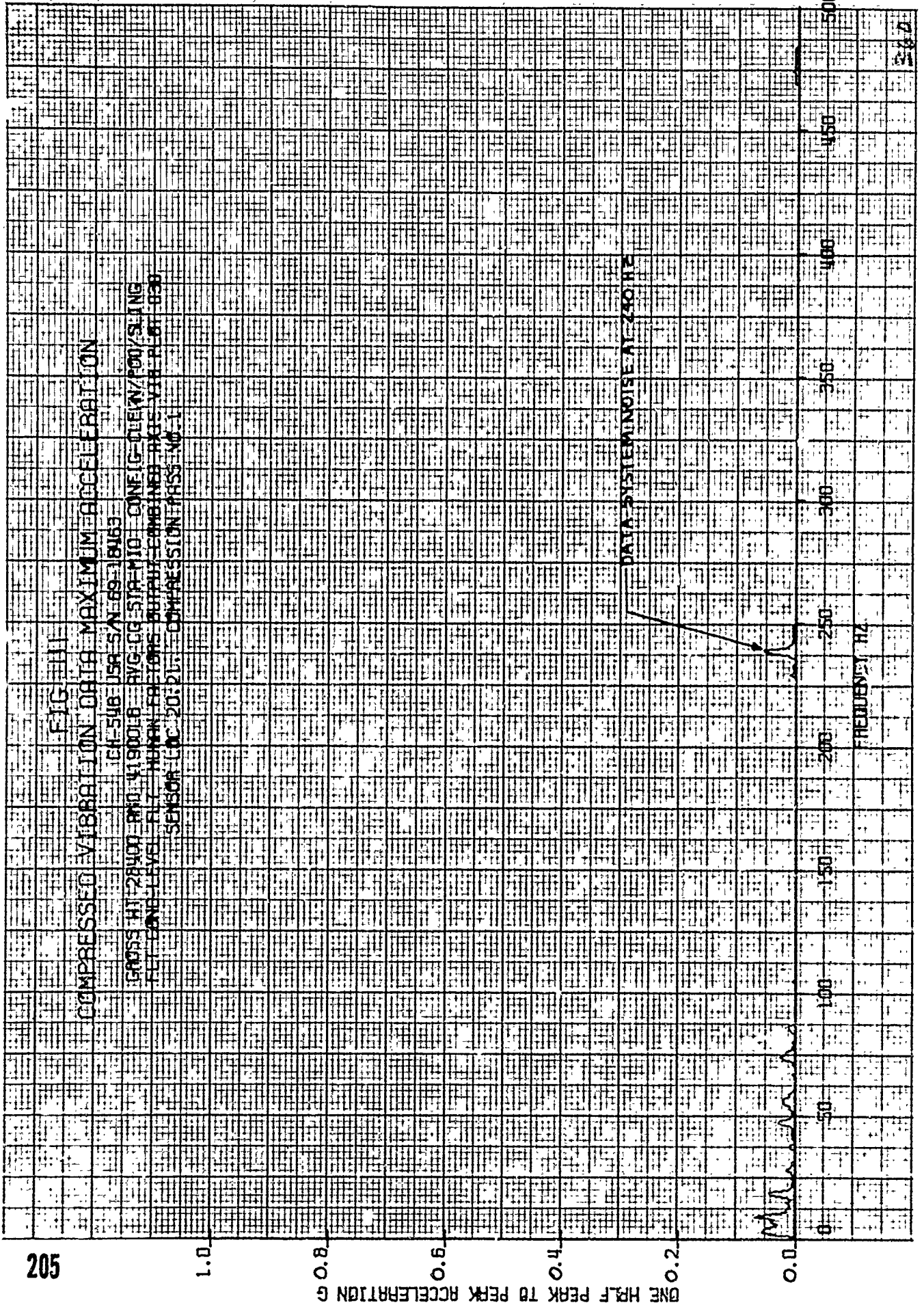
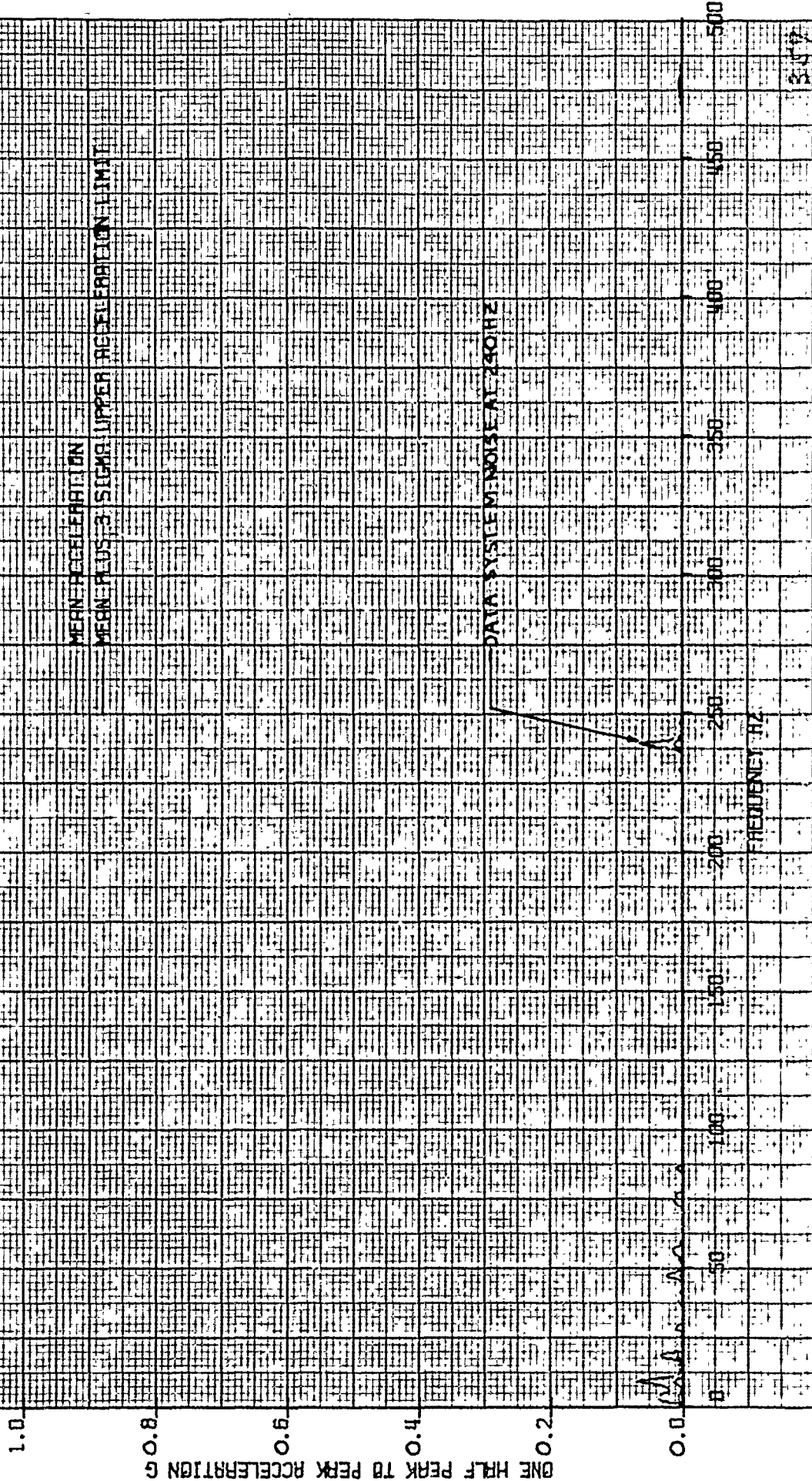


FIG. 112

## COMPRESSED VIBRATION DATA

CH-54B USA 57N 63-18463  
 GROSS INT 28400 AND 41900 LBS AVG CG STR MID CONE (G-DEERZ/POD/SLING  
 FLT DONG LEVEL FLT HUMAN FACTORS SUPPORT COMBINED AXIS VIB PLAT 833  
 SENSOR LOC 2D 2L COMPRESSION PASS NO 1





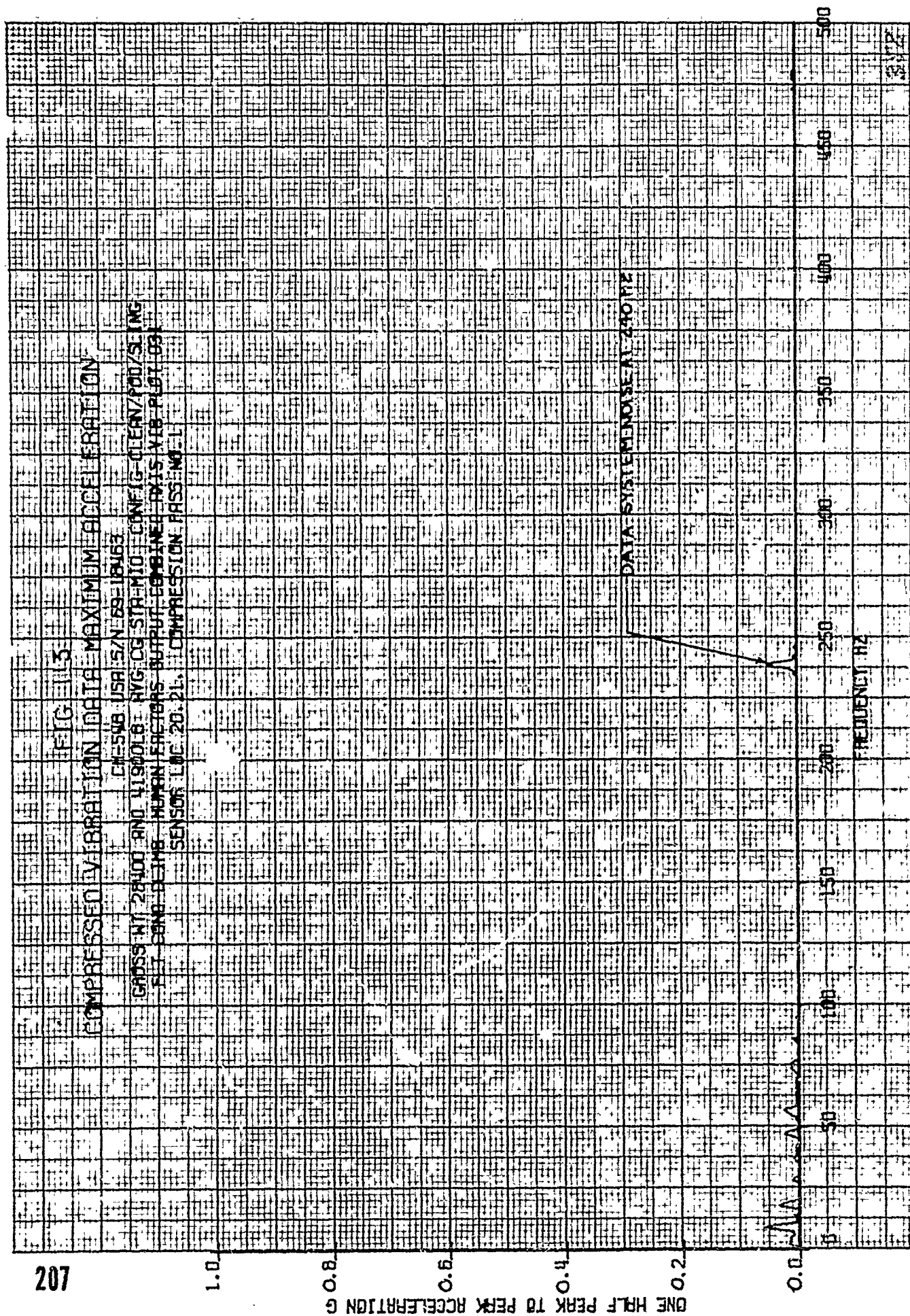


FIG 114

## COMPUTED VIBRATION DATA

GROSS WT 28400 LBS  
CH-54B USA S/N 69-18463  
AVG CG STR-NIO CONFIG-CLEAN/POD/SLING  
FLT COND-BE-RMB HUMAN FACTORS OUTPUT COMBINED AXIS Y-13 PLOT 033  
SENSOR LOC 20121 COMPRESSION PASS NO.1

1.0

0.8

0.6

0.4

0.2

0.0

ONE HALF PEAK TO PEAK ACCELERATION G

MEAN ACCELERATION

MEAN PLUS 3 SIGMA

UPPER RECELERATION LIMIT

DATA SYSTEM NOISE AT 240 HZ

0

50

100

150

200

250

300

350

400

450

500

FREQUENCY HZ

437

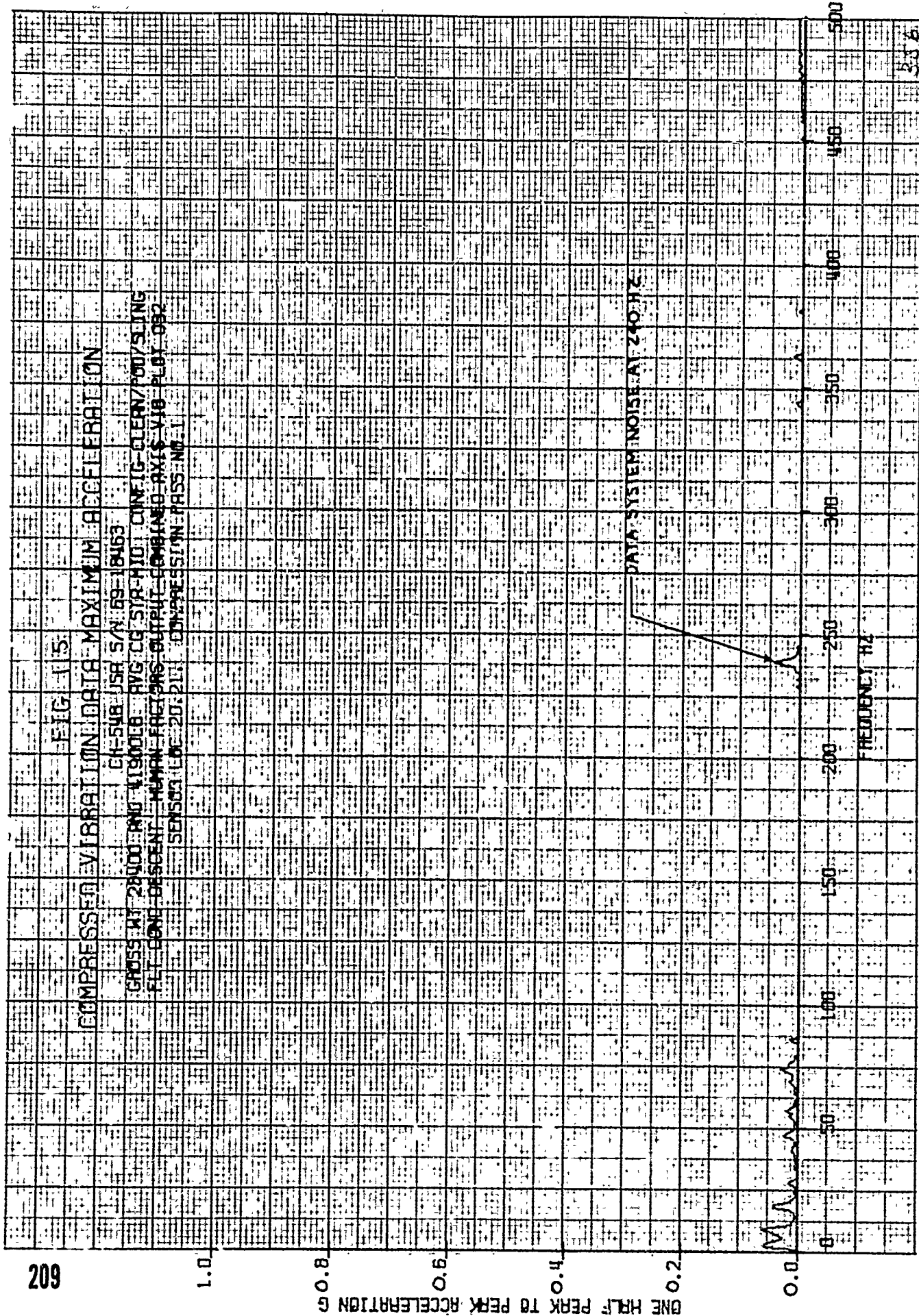




FIG. 116

## COMPRESSED VIBRATION DATA

GROSS WT 28400 LBS  
 CH-SUB USA 57N 69-18463  
 AVG CG STR-M10 CONFIG-CLEAN/POD/SLING  
 PLT-BOMB-BRESENT HUMAN FACTORS & TRAV COMBINED AXIS-VIB PLAT-092  
 SENSOR-LOC-20-21 COMPRESSION-PASS-NO-1

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

ONE HALF PEAK TO PEAK ACCELERATION G

DATA SYSTEM NOISE AT 240 HP

0.0

0.2

0.4

0.6

0.8

1.0

100

150

200

250

300

350

400

450

500

FREQUENCY HZ

500

450

400

350

300

250

200

150

100

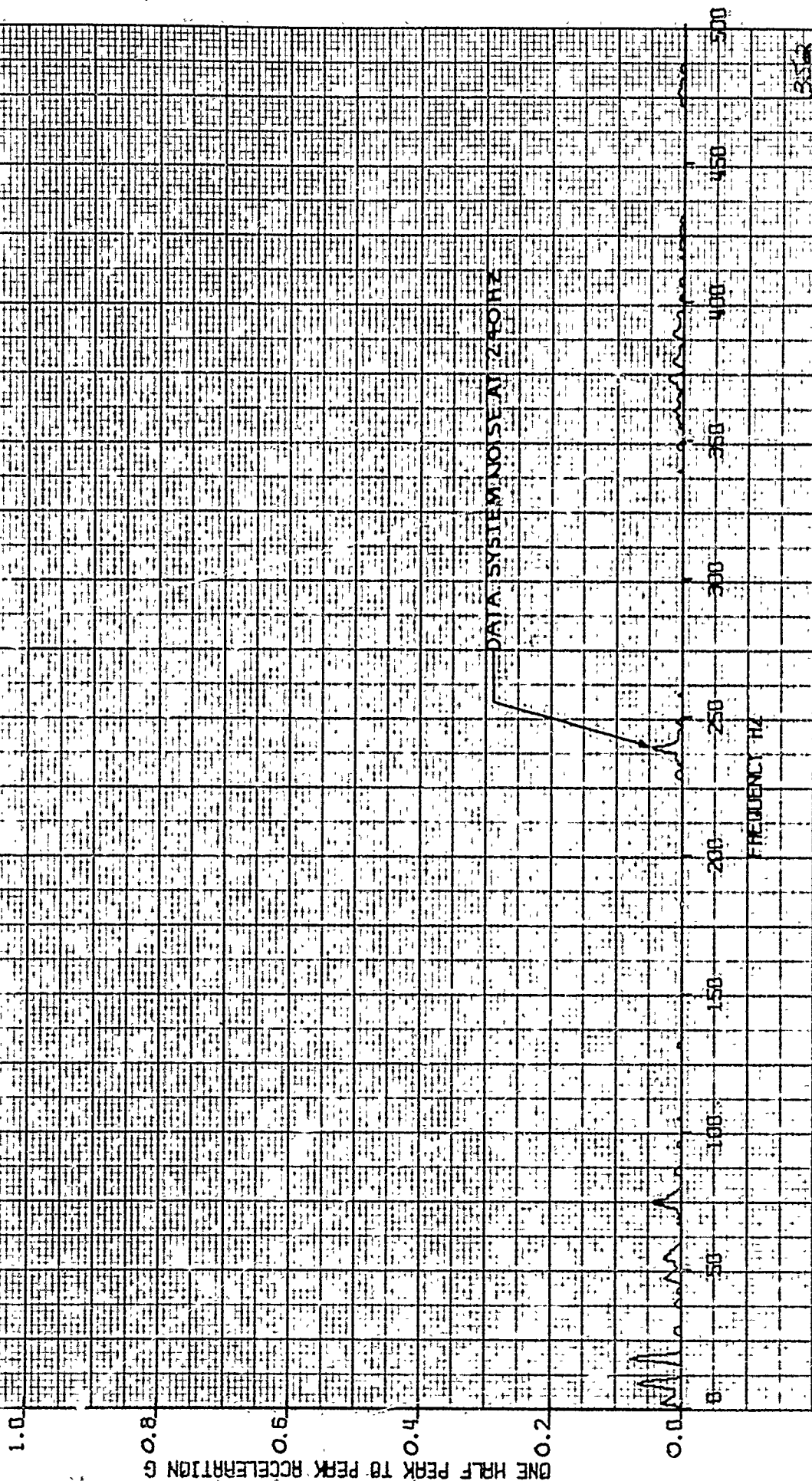
50

0

FIG. 117

## COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

CH-54B USA SN-69-13463  
 GROSS WT 28400 AND 41900 LB. AVG CG STA-HYD COME (G-CIERN/POD/SEING  
 PET COND-T/O AND LOG-HUMAN FACTORS OUTPUT-COMBINED-AXIS-VIB-PLT-033  
 SENSOR LOC 20.21, COMPRESSION PASS NO.1





RIG 118

## COMPRESSED VIBRATION DATA

CH-SUB-USA S/N 69-18463

GROSS WT 28400 AND 41500 LBS AVG CG STA MID CONE/C CLEAN/POD/SLING  
 PET COND 7.0 AND 1.0 HUMAN FACTORS OUTPUT COMBINED AXIS VIB-PLGT 033  
 SENSOR LOC 20121 COMPRESSION PASS NO 1

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

ONE HALF PEAK TO PEAK ACCELERATION G

DATA SYSTEM NOISE AT 220HZ

FREQUENCY HZ

500

500

450

400

350

300

250

200

150

100

50

0

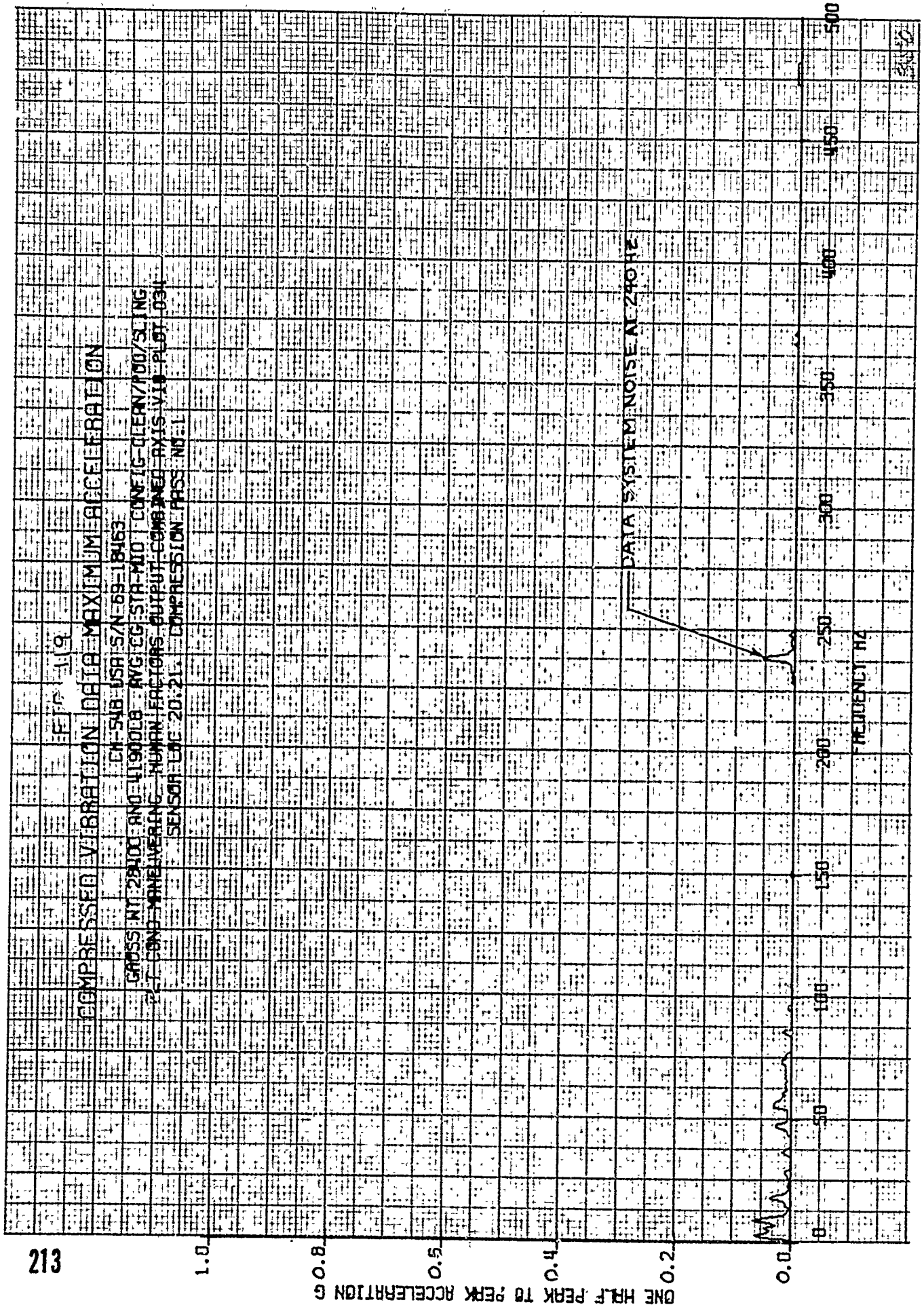


FIG 120

COMPRESSED VIBRATION DATA

CH SUB USA S/N 69-18463  
 GROSS WT 28400 AND 1900LB AVG CG STR-MID CONF G-CLERN/00/SLING  
 RET-COND-PANELVERING HUMAN FACTORS-OUTPUT COMBINED FXIS-VIB-PLAT 034  
 SENSOR LOC 20-21- COMPRESSION PASS NO 1

1.0

0.8

0.6

0.4

0.2

0.0

ONE HALF PEAK TO PEAK ACCELERATION G

MEAN ACCELERATION

MEAN PLUS 2 SIGMA UPPER ACCELERATION LIMIT

DATA SYSTEM NOISE AT 250 Hz

500

450

400

350

300

250

200

150

100

50

FREQUENCY HZ

349

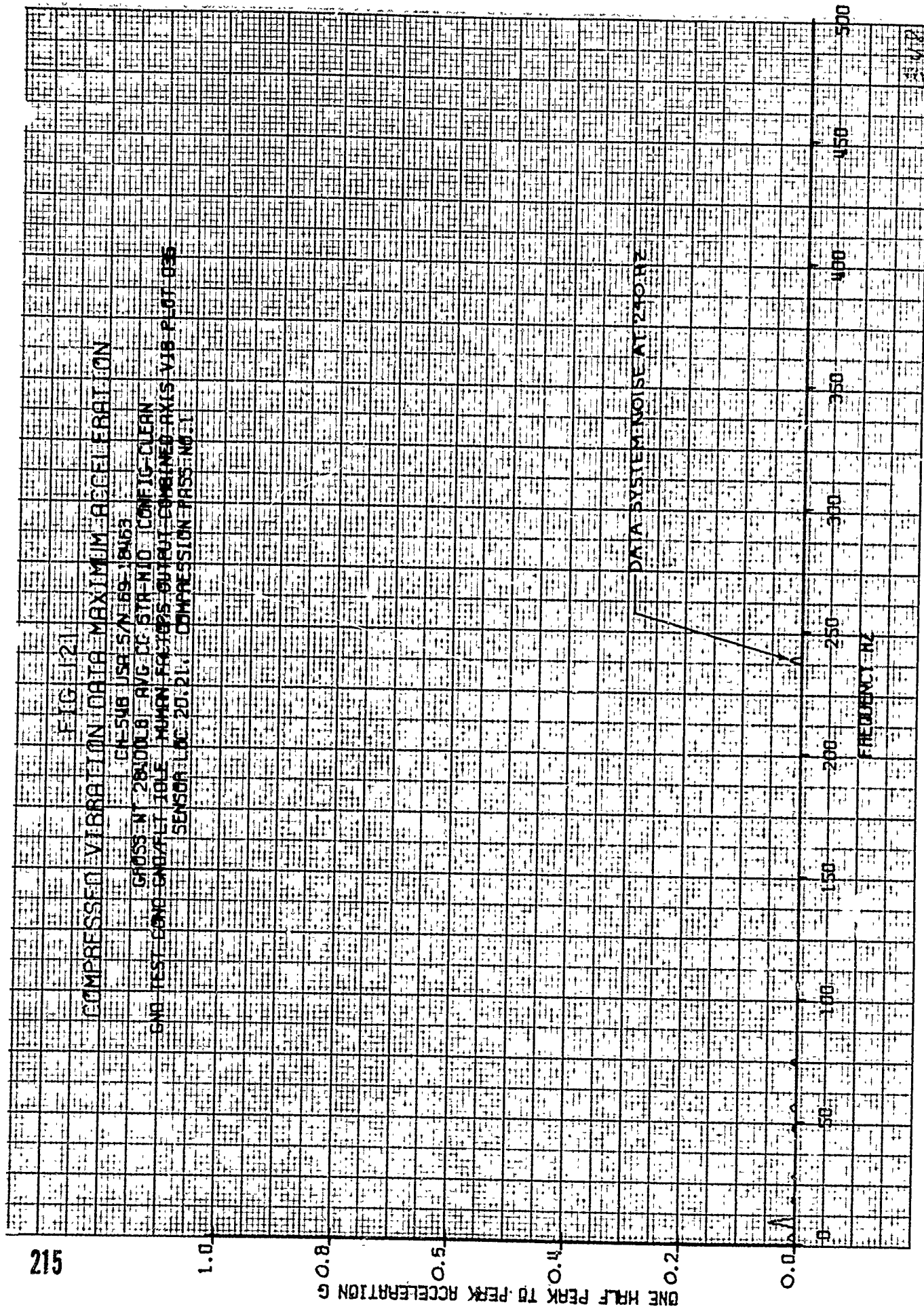




FIG. 1-22

## COMPRESSED VIBRATION DATA

CH-54B USA S/N 89-18463

GROSS WT 2840 LB AVG CG STA-MID CONF IG-CLEAN

CMB TEST CMB CMB/FET-10LE HUMAN FACTORS OUTPUT COMBINED AXIS VIB PLAT-B35

SENSOR LOC 20:21 COMPRESSION PASS NO:1

0.8

0.6

0.4

0.2

0.0

0.0

0.0

0.0

0.0

0.0

0.0

0.0

0.0

0.0

0.0

0.0

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

DATA SYSTEM NOISE AT 240 HZ

FREQUENCY HZ

500

450

400

350

300

250

200

150

100

50

0

347



FIGURE 123  
 STATIC INTERIOR TEMPERATURE  
 CH-54B USA MC9-18403  
 FRONT AVIONICS

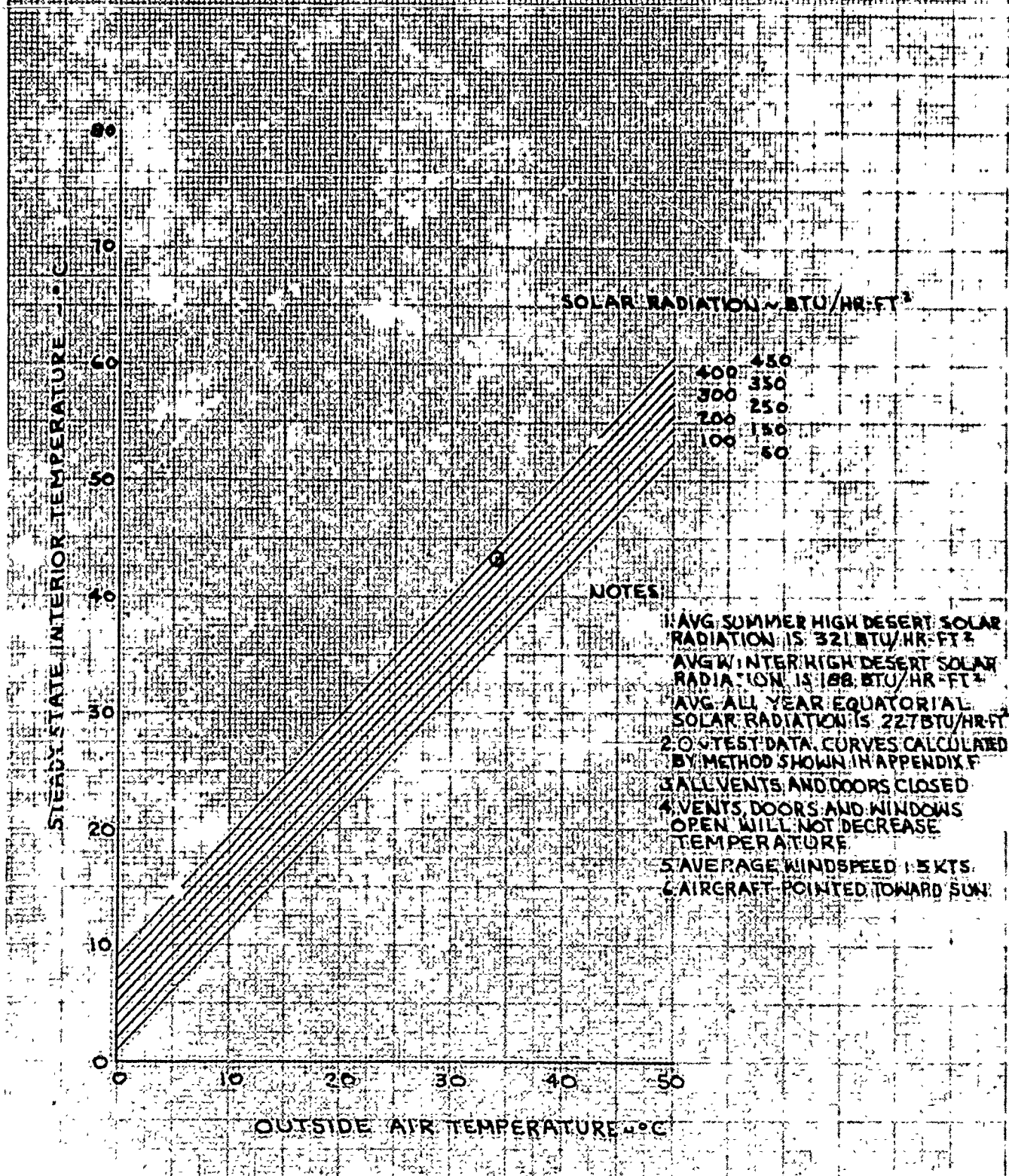


FIGURE 124  
 STATIC INTERIOR TEMPERATURE  
 CH-54B USA 1/469-18463  
 INSTRUMENT PANEL BACK

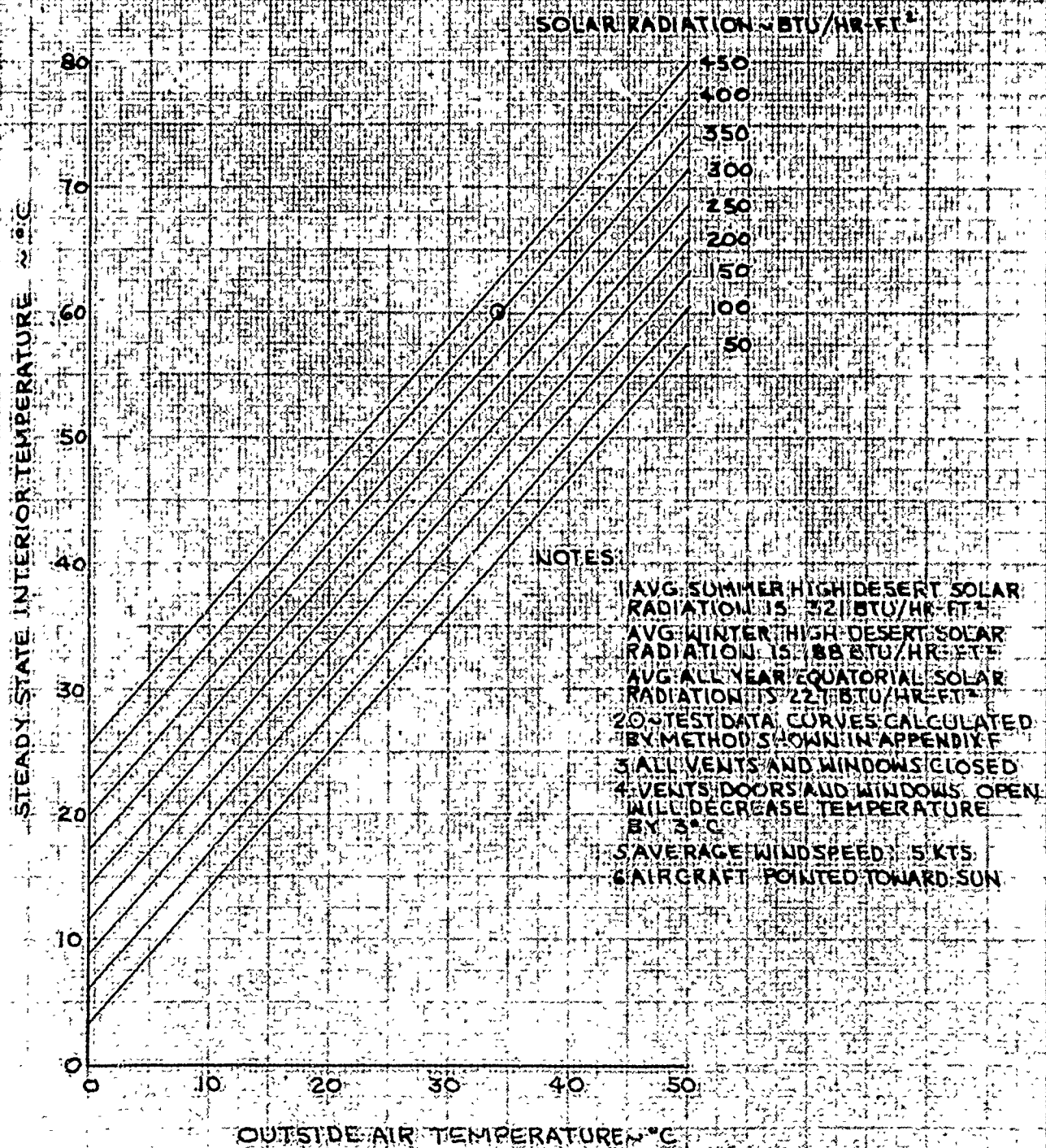


FIGURE 125  
 STATIC INTERIOR TEMPERATURE  
 CH-54B USAF C-9-18463  
 FRONT CABIN

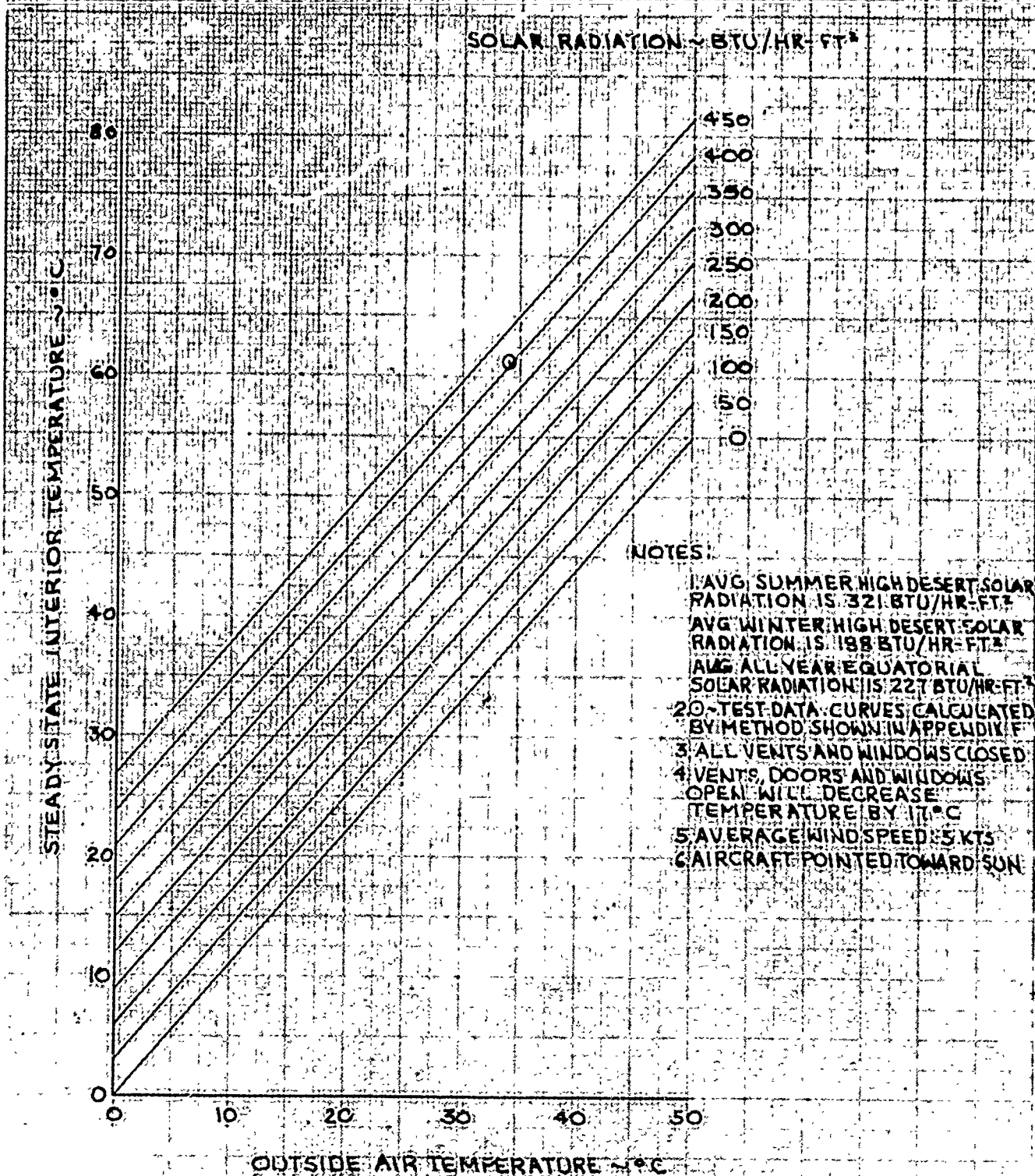
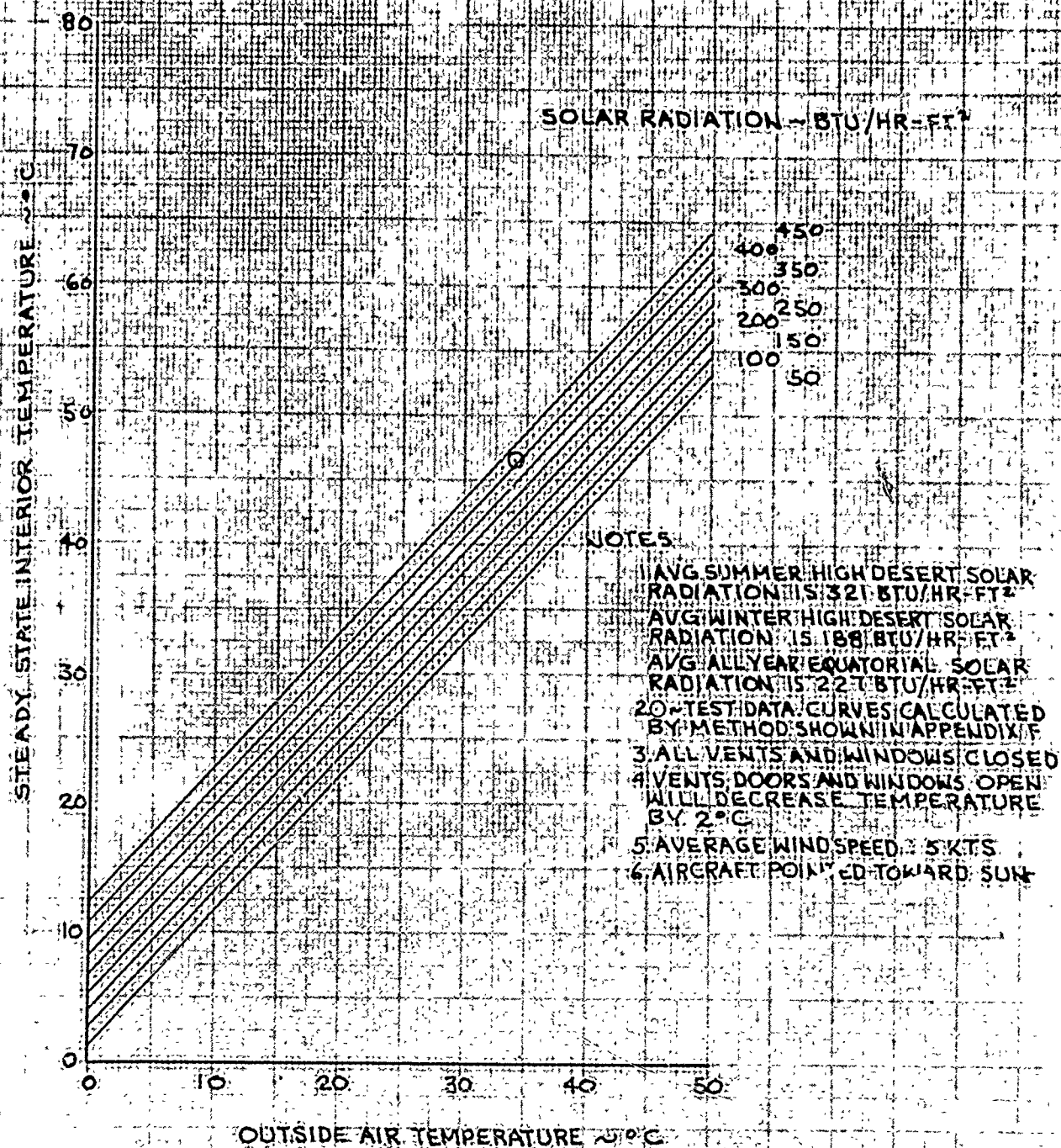




FIGURE 126  
 STATIC INTERIOR TEMPERATURE  
 CH-54B USA 9/69-18463  
 AFT CABIN



## APPENDIX H. HELICOPTER VIBRATION SOURCES

There are three primary sources of vibration in present-day gas turbine-powered helicopters: the main and tail rotors; all other rotating components; and, if the helicopter is armed, gunfire. The rotor induced vibrations are of a low frequency with the fundamental frequency equal to the rotor speed. In present-day helicopters, the main rotor speed ranges from about 3 to 8 Hz with the rotor speed generally decreasing with increasing rotor diameter. A vibration occurring at the main rotor fundamental frequency is referred to as the one-per-rotor-revolution (1/rev). The rotor also induces harmonic vibrations at frequencies which are integral multiples of the number of rotor blades multiplied by the fundamental rotational frequency. Thus, a two-bladed rotor with a fundamental frequency of 5 Hz induces vibrations at frequencies of 5 Hz (1/rev), 10 Hz (2/rev), 20 Hz (4/rev), 30 Hz (6/rev), etc., and a three-bladed rotor at frequencies of 5 Hz (1/rev), 15 Hz (3/rev), 30 Hz (6/rev), 45 Hz (9/rev), etc. Normally, main rotor induced vibrations beyond the 10th harmonic, 100 Hz for a two-bladed rotor, are not significant. Rotor induced vibrations at harmonics of the rotor fundamental frequency are the predominant helicopter low-frequency vibrations and are caused by dissymmetry of lift over the rotor disc which excite rotor blade structural modes and generally increase with airspeed. Vibrations are induced by all other rotating components in the helicopter. The frequencies range from the fundamental rotational frequency of the component up to geartooth, ball-bearing, and turbine-blade-passage frequencies which may range as high as 20 to 30 kilohertz. Gunfire induced vibrations are caused by recoil forces transmitted through the gun mount and by muzzle blast pressures. They have a fundamental frequency equal to the gun rate of fire and harmonics of this fundamental up to about the 20th harmonic. Typically, the highest vibration level will be at one of the gunfire harmonic frequencies. Fundamental gunfire frequencies range up to about 70 Hz.



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13. ABSTRACT

Vibration and temperature measurement tests were conducted on a CH-54B helicopter to define the vibration and temperature environment for the instruments, avionics, pilot station, and other component parts for representative flight conditions. Testing was performed by the United States Army Aviation Systems Test Activity, Edwards Air Force Base, California, between 22 August and 29 September 1972. The testing consisted of 16 flights totaling 18.5 productive test hours. Vibration data were recorded from 70 accelerometer locations for 55 flight conditions, and narrow band spectral analyses were performed on the vibration data. The results of the spectral analyses were summarized by use of statistical methods. Forward fuselage vibrations were primarily low frequency and were caused by the main rotor. Aft fuselage vibrations were primarily high frequency and were caused by gearbox and other rotating component vibration sources. The highest vibration levels were recorded at the auxiliary power plant at main transmission gear mesh frequencies. There were two shortcomings: amplification of main rotor-induced vibrations by avionics vibration isolation mounts, and excessively high Wet Bulb Globe Temperature index at the pilot station under certain environmental conditions.

14 KEY WORDS	LINK A		LINK B		LINK C	
	ROLE	WT	ROLE	WT	ROLE	WT
Vibration and temperature measurement tests CH-54B helicopter Vibration and temperature environment definitions Vibration data Accelerometer locations Narrow band spectral analyses Statistical methods Low-frequency forward fuselage vibrations High-frequency aft fuselage vibrations						